Conventional Synchronous Reference Frame Phase-Locked Loop Is An Adaptive Complex Filter

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Abstract—Despite the wide acceptance and use of the conventional synchronous reference frame phase-locked loop (SRF-PLL) no transfer function describing its actual input-output relationship has been developed so far. Arguably, the absence of such transfer function has hampered the application of SRF-PLL as a filter or controller inside the closed-loop control systems. In this paper, the transfer function describing the actual input-output relationship of the conventional SRF-PLL is presented. Using this transfer function, it is shown that the conventional SRF-PLL is a first-order adaptive complex bandpass filter. It is also shown that this transfer function can be useful for tuning of SRF-PLL parameters. The accuracy of this transfer function is confirmed through numerical results.

Index Terms—Synchronous reference frame phase-locked loop (SRF-PLL), modeling, complex filters.

I. INTRODUCTION

Owing to its simple structure, robustness, and effectiveness, the synchronous reference frame phase-locked loop (SRF-PLL) is probably the most popular and widely used technique for extraction of information about the grid fundamental component in three-phase systems [1]. Fig. 1 shows the block diagram description of this PLL. In this PLL, as shown, the stationary (αβ) coordinate voltages (which are obtained by applying the Clarke transformation to the three-phase voltages) are transformed to the synchronous reference frame by applying the Park transformation. The dq reference frame angular position is regulated using a feedback control loop which forces \( v_q \) to zero. Typically, a proportional-integral (PI) controller is used as the loop filter (LF). Also, to make the SRF-PLL performance insensitive to grid amplitude variations, the signal \( v_q \) is divided by an estimation of grid voltage amplitude, which can be obtained by passing \( v_d \) through a low-pass filter (LPF) [2]. The fundamental frequency positive sequence (FFPS) components are finally constructed using the extracted phase and amplitude.

To the best of the authors’ knowledge, no transfer function relating the input voltages to the output voltages of the conventional SRF-PLL has been developed so far. We believe the absence of such transfer function has hampered the application of SRF-PLL as a filter or controller inside the closed-loop control systems despite the great advantages that it can offer.

In this paper, the transfer function describing the actual input-output relationship of the conventional SRF-PLL is presented. This transfer function shows that the conventional SRF-PLL is actually a first-order complex bandpass filter (CBF). It is worth mentioning that the complex filters have an asymmetrical frequency response around zero frequency, and therefore they can make distinction between the positive and negative sequences of a same frequency [3]-[5].

II. TRANSFER FUNCTION REPRESENTATION OF SRF-PLL

In this section, the transfer function describing the actual input-output relationship of the SRF-PLL is determined. To determine this transfer function, it is assumed that: 1) the LPF used to filter out the d-axis voltage component is a first-order LPF of the form \( LF(s) = k_v / (s + k_v) \) where \( k_v \) is the LPF cutoff frequency; and 2) the proportional gain \( k_p \) of the PI controller and the cutoff frequency \( k_v \) are equal, i.e., \( k_p = k_v = k \). The second assumption is similar to that assumed in [6] to obtain the transfer function describing the input-output relationship of the Enhanced PLL (EPLL).

According to Fig. 1, the SRF-PLL output signals can be expressed in time-domain as

\[
\begin{align*}
\hat{v}_{d,1}^+(t) &= \hat{v}_{d,1}^+(t) \cos(\hat{\theta}^+_1) \\
\hat{v}_{q,1}^+(t) &= \hat{v}_{q,1}^+(t) \sin(\hat{\theta}^+_1).
\end{align*}
\]

Differentiating from both sides of (1) yields

\[
\begin{align*}
\dot{\hat{v}}_{d,1}^+(t) &= \hat{v}_{d,1}^+(t) \cos(\hat{\theta}^+_1) - \hat{\theta}^+_1 \hat{v}_{d,1}^+(t) \sin(\hat{\theta}^+_1) \\
\dot{\hat{v}}_{q,1}^+(t) &= \hat{v}_{q,1}^+(t) \sin(\hat{\theta}^+_1) + \hat{\theta}^+_1 \hat{v}_{d,1}^+(t) \cos(\hat{\theta}^+_1).
\end{align*}
\]

According to Fig. 1 and what was assumed at the beginning of this section, we can obtain \( \hat{\theta}^+_1 \) and \( \hat{v}_{d,1}^+ \) as

\[
\begin{align*}
\dot{\hat{\theta}}^+_1 &= \hat{\omega}(t) + k \frac{v_d(t)}{v_{d,1}(t)} \\
\hat{v}_{d,1}(s) &= \frac{k}{s+k} v_d(s) \Rightarrow \hat{v}_{d,1}^+(t) = k \left[ v_d(t) - \hat{v}_{d,1}^+(t) \right].
\end{align*}
\]

Substituting (3) into (2) and performing some simple mathematical manipulations, yields

\[
\begin{align*}
\hat{v}_{\alpha,1}^+(t) &= k \left[ v_d(t) \cos(\hat{\theta}^+_1) - v_q(t) \sin(\hat{\theta}^+_1) \right] \\
&- k \left[ \hat{v}_{\alpha,1}^+(t) \cos(\hat{\theta}^+_1) - \hat{\omega}(t) \hat{v}_{\alpha,1}^+(t) \sin(\hat{\theta}^+_1) \right].
\end{align*}
\]
order CBF. Fig. 2 shows the frequency response of (9) for \( jv \) where

\[
\omega = 2\pi 50 \, \text{rad/s} \quad \text{and three different values of } k.
\]

Notice that the responses to negative frequencies in these plots can be interpreted as the responses to the negative sequence vector signal. As expected, the SRF-PLL frequency response is asymmetrical around zero frequency: it provides unity gain with zero-phase shift at the fundamental frequency of positive sequence, while it provides a certain level of attenuation at the same frequency of negative sequence.

### B. Analysis With Time-Varying \( \dot{\omega} \)

It is shown in this section that the estimated frequency \( \dot{\omega} \) is in general a slowly varying function time. Therefore, the obtained transfer function for the SRF-PLL (which was based on assuming a constant value for the estimated frequency \( \dot{\omega} \)) can provide a good approximation in general case. This analysis is based on the linearized model of the SRF-PLL which can be simply obtained by assuming a quasi-locked state [7].

Fig. 3 shows the linearized model of the SRF-PLL in which \( \omega \) and \( \theta_i^+ \) are the frequency and phase of the grid voltage, respectively. According to this model, the closed loop transfer function relating the actual frequency to the estimated frequency can be obtained as

\[
\dot{\omega}(s) = \frac{k_i}{s^2 + k_p s + k_i} \omega(s).
\]

This transfer function (which is a standard second order transfer function) implies any variation in the grid frequency...
be concluded that the estimated frequency \( \hat{\omega} \). According to this fact and that mentioned above, it can be expected that the estimated frequency \( \hat{\omega} \) experiences a smooth transition when the grid frequency undergoes variations. On the other hand, in most practical cases the grid frequency \( \omega \) has a stable nature, and its sudden and large variations are not expected [8]. Therefore, it can be concluded that the estimated frequency \( \hat{\omega} \) is typically selected. Therefore, it can be concluded that the estimated frequency \( \hat{\omega} \) is in practice a slowly varying function of time. Thus, the obtained transfer function for the SRF-PLL, which obtained by assuming a fixed \( \hat{\omega} \), can provide a good approximation in general case.

III. DESIGN GUIDELINES

As shown in previous section, \( G_{\text{SRF-PLL}}(s) \) is a CBF (with center frequency \( \hat{\omega} \)) which its bandwidth is determined by the parameter \( k \). The higher the value of \( k \), the higher the bandwidth and, therefore, the lower the filtering capability (see Fig. 2). So, selection of \( k \) involves a trade-off between the filtering capability and the transient time.

Assuming the dc offset in the SRF-PLL input is negligible (as is typically the case), the fundamental frequency negative sequence (FFNS) component is the disturbance component that we should be most concerned about, due to its low frequency. Fig. 4 shows the attenuation provided by the SRF-PLL at the fundamental frequency of negative sequence as a function of \( k \). The 2% settling time of the SRF-PLL in extraction of the FFPS component (according to (9) the 2% settling time can be approximated by \( t_s \approx 4/k \)) is also shown in this figure. The figure clearly shows the trade-off between the filtering capability and transient time, and it can be used for selecting a proper value for \( k \).

Once the value of \( k \) is determined, the next step is to determine the integral gain \( k_i \). From Fig. 3, the closed-loop transfer function relating the input and estimated phases can be expressed as

\[
G_{cl}(s) = \frac{\dot{\theta}_{est}^+(s)}{\theta_{est}^+(s)} = \frac{k_p s + k_i}{s^2 + k_p s + k_i}
\]  

which is a standard second order transfer function, having a zero. Define \( k = k_p = 2\zeta \omega_n \) and \( k_i = \omega_n^2 \) where \( \zeta \) is the damping factor and \( \omega_n \) is the natural frequency. Thus, we can write

\[
k_i = \frac{k^2}{4\zeta^2}.
\]

As the value of \( k \) has already been determined, \( k_i \) can be determined by selecting a proper value for \( \zeta \). Often \( \zeta = 1/\sqrt{2} \) [7] and sometimes \( \zeta = 1 \) [8] is recommended in literature. The former value is selected in this paper which results in \( k_i = k^2/2 \).

IV. NUMERICAL RESULTS

In this section, the accuracy of obtained transfer function for the SRF-PLL is confirmed through numerical results. The selected values for control parameters are summarized in Table I.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Proportional gain, ( k_p )</td>
<td>140</td>
</tr>
<tr>
<td>LPF’s cutoff frequency, ( k_v )</td>
<td>140</td>
</tr>
<tr>
<td>Integral gain, ( k_i )</td>
<td>9800</td>
</tr>
<tr>
<td>Sampling frequency, ( f_s )</td>
<td>10 kHz</td>
</tr>
<tr>
<td>Nominal frequency, ( w_o )</td>
<td>2\pi50 rad/s</td>
</tr>
</tbody>
</table>

To evaluate the accuracy of obtained transfer function, different harmonic components of different sequences are added to the input of the SRF-PLL and their amplitudes at the output of the SRF-PLL are measured. The gain of SRF-PLL at each harmonic frequency is then obtained by dividing the measured amplitude by the input voltage amplitude at that harmonic frequency, and compared with those predicted by the transfer function. Fig. 5 shows the obtained results. It can be observed that the obtained transfer function is accurate.

V. CONCLUSION

In this paper the transfer function describing the actual input-output relationship of the SRF-PLL was developed.
Using this transfer function it was shown that the conventional SRF-PLL is a first-order CBF. Usefulness of this transfer function in tuning of the SRF-PLL’s control parameters was also shown.

REFERENCES


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