The Application of Vector Fitting to Eigenvalue-based Harmonic Stability Analysis

Mohammad Kazem Bakhshizadeh, Student Member, IEEE, Changwoo Yoon, Student Member, IEEE, Jesper Hjerrild, Claus Leth Bak, Senior Member, IEEE, Łukasz Kocewiak, Senior Member, IEEE, Frede Blaabjerg, Fellow, IEEE, and Bo Hesselbæk

Abstract— Participation factor analysis is an interesting feature of the eigenvalue-based stability analysis in a power system, which enables the developers to identify the problematic elements in a multi-vendor project like in an offshore wind power plant. However, this method needs a full state space model of the elements that is not always possible to have in a competitive world due to confidentiality. In this paper, by using an identification method, the state space models for power converters are extracted from the provided data by the suppliers. Some uncertainties in the identification process are also discussed and solutions are proposed, and in the end the results are verified by time domain simulations for linear and nonlinear cases with different complexities, no matter which domain (phase or dq) is used.

Index Terms— Eigenvalue analysis; Harmonic Stability; Matrix Fitting; Participation Factor Analysis; Vector Fitting

I. INTRODUCTION

THE drastic increasing trend of global energy consumption and the demand for cleaner and more sustainable energy are bringing more new and renewable energy sources into the existing power system [1]–[3]. As a consequence of the very wide-spread renewable energy resources, the interfacing units, typically Power Electronics (PE) based power devices, are connected anywhere in the existing power system and unexpected interaction problems are caused by these newly installed PE units [4]–[7]. These interaction problems can be categorized by their frequency range into two categories. One is low-frequency small signal instability around the fundamental frequency [8]–[10] or even lower frequency, such as the sub-synchronous resonance frequency [11]–[13]. The other one is the instability with the relatively higher frequencies ranged from a few hundred Hertz to a few kilo Hertz [7], [14], [15]. Even though the physical reason of these instabilities may be different from each other, all these interaction problems can be understood by the conditions that creates unstable poles in the system transfer-function [16], [17].

There are typically two ways to assess small signal stability. One is the Impedance Based Stability Analysis (IBSA) [17] and the other one is the eigenvalue-based analysis using the State-Space (SS) model [16]. The IBSA evaluates the system’s stability using the ratio of the impedance of the two sub systems (lumped impedances) that are connected to the node under study. While the eigenvalue-based method models the entire system as SS matrices, the IBSA is a simpler method but gives only local information about the stability of the system. The IBSA is confined only to an interconnection point and it needs to be remodeled repeatedly in order to assess somewhere else [18], [19]. In contrast SS models are harder to get but using them one can study the system globally. The SS model allows the participation factor analysis or the sensitivity analysis [20], [21] which is very necessary when imposing a responsibility of the interaction problem to the participants in the power network. Phenomenally, the interaction problem is a compounded issue with the linked impedances and the participant can be an offender or a victim at the same time. In that sense, it is necessary to have a quantitative method that measures the effect on the poles of the entire system (eigenvalues) from varying the state variables in each subsystem [20]. The entire SS model can be found using a systematic and modular method called Component Connection Method (CCM) [22], [23]. Also, by the help of CCM, the problematic state variables in each subsystem can be managed and visible easily [21].

However, this method is only possible on the assumption that we have proper SS models of all subsystems. The problem is with the confidentiality of the commercial products where the detailed SS model cannot be obtained and can only be reconstructed indirectly such as by Vector Fitting (VF) [24]–[26]. In [27] the application of the VF in eigenvalue-based stability analysis has been introduced, in which based on measurements from a node in the network, an SS model is proposed using the VF. However, since this model is based on a local measurement, the model is local and not global. In other words, it cannot show the dynamics of the entire system if there are some symmetries in the system, which leads to the appearance of some hidden dynamics [28], and as a result this
method must be repeated at different nodes. It also needs a stable system to do measurements, because if the system is unstable, then no measurement can be done and this method is not applicable. Finally, since the entire network is modelled as a black box seen from the measurement point, no further studies such as the participation factor analysis can be done to find the most problematic component in a system. It must be noted that the method proposed in this paper can be considered as an extension to [27] when more information is available.

In this paper, system stability analysis based on SS and CCM by using the indirect VF is presented. Some interaction case examples are adopted to show the validity of this procedure. The result shows that the problematic subsystem could be identified based on the participation factor analysis even for an unstable system. Since the method models the entire system using a systematic approach, it includes all dynamics of the system. Some uncertainties in the VF are also discussed.

II. EIGENVALUE ANALYSIS

A. Stability Evaluation

If one has the overall SS representation of a system, for instance as given in (1), then the stability can be evaluated by investigating the eigenvalues of matrix A, which is called the state (or system) matrix [29]. The eigenvalues are indeed poles of the system and if their real part is positive, then the system is unstable. It must be noted that in this paper the focus is on linear/linearized SS models.

\[
\dot{x} = Ax + Bu \\
y = Cx + Du
\]  

(1)

The eigenvalues also contain some other useful information [20], for instance if the \(i\)th eigenvalue/pole, which is called hereafter the \(i\)th mode, is

\[
\lambda_i = \sigma_i + j\omega_i
\]

(2)

Then the oscillation frequency of that mode is \(\omega_i\), the time constant of that mode, very similar to a first order RC system, is \(1/\sigma_i\), and the damping is defined as

\[
\xi_i = \frac{-\sigma_i}{\sqrt{\sigma_i^2 + \omega_i^2}}
\]

(3)

In other words the transient response of the system to a perturbation includes this frequency which will decay with the specified time constant/damping. A negative damping by definition indicates an unstable case, where instead of damping, amplifying happens. Therefore, not only the stability of the system can be assessed using the sign of the real parts, but also the minimum damping of the system can be found. The latter can be considered as a measure that states how stable a system is.

B. How to find the overall SS model

One problem is how to find the SS representation of such a complicated system, which has some controllers in addition to a coupled electrical system. The Component Connection Method (CCM) is a good way to deal with very complicated systems [23]. In this method each subsystem (power converters, passive network and etc.) is modelled separately and in the end the overall SS can be found by some simple matrix operations. Modelling the system in this way is much easier and the equations are more readable. The implementation of this algorithm in a computer program is also more straightforward. In this method, first the block diagonal matrices are created by simply appending the different SS matrices individually without considering the interconnections between them.

\[
\tilde{x}_i = A_i x_i + B_i u_i \\
\tilde{y}_i = C_i x_i + D_i u_i
\]

(4)

Then, the final matrices can be obtained by

\[
u_{cmp} = L_1 y_{cmp} + L_2 u_{sys}
\]

(5)

\[y_{sys} = L_3 y_{cmp} + L_4 u_{sys}\]

(9)

where, \(L_i\) to \(L_4\), which are called the interconnection matrices, are the matrices which define the relationship between the inputs and outputs of the individual components (\(u_{app}\) and \(y_{cmp}\)) and the inputs and outputs of the total system (\(u_{sys}\) and \(y_{sys}\)). The total SS model is described by

\[
\tilde{x}_{app} = A_T x_{app} + B_T u_{sys}
\]

(10)

\[y_{sys} = C_T x_{app} + D_T u_{sys}\]

where,

\[
A_T = A_{app} + B_{app} L_1 (I - D_{app} L_1)^{-1} C_{app}
\]

(11)

\[B_T = B_{app} L_1 (I - D_{app} L_1)^{-1} D_{app} L_2 + B_{app} L_2
\]

\[C_T = L_3 (I - D_{app} L_1)^{-1} C_{app}
\]

\[D_T = L_3 (I - D_{app} L_1)^{-1} D_{app} L_2 + L_4
\]

and \(I\) is the identity matrix.

C. Improper transfer functions

A transfer function is called improper, if the order of the numerator polynomial is more than the order of the denominator polynomial. The SS model of an improper transfer function could not be described by only A, B, C and D
matrices and another matrix $E$ is needed to model the extra order.

$$
\dot{x} = Ax + Bu \\
y = Cx + Du + Eu
$$

The VF is able to find the $E$ matrix; however, in this paper the improper transfer functions are avoided by choosing a proper impedance or admittance representation. For instance, for Current-Controlled Converters (such as solar inverters) a series inductor is normally used for smoothing the output current, therefore this series inductance makes the transfer function of the output impedance improper. However, by using the admittance model for a current controlled converter this problem can be avoided. The same can be concluded for Voltage-Controlled Converters, in which a capacitive shunt is used at the output terminal. Thus, for a Voltage-Controlled Converter an impedance model should be used. As a conclusion the $E$ matrix is not necessary in the identification process by choosing the correct models based on the application and a little engineering judgement. If the magnitude of the frequency response goes up for higher frequencies, then it means the current model might be improper.

### III. THE PROPOSED METHOD FOR DEALING WITH BLACK BOX MODELS

If the SS models of converters and other elements are available, then one can use the aforementioned method and evaluate the stability. However, the structure and parameters of the power converters are not always available due to confidentiality and intellectual property rights. Instead, the terminal characteristics of the converter are delivered as a look up table, which shows the frequency response of the converter to a voltage/current perturbation at a given condition. Fig. 1 shows the admittances of 5 current controlled converters [15], which are considered in this paper. It is assumed that these are the only available information. The admittances are measured in the phase domain and since the bandwidth of the Phase Locked Loop (PLL) is set too low, therefore, the coupling in the frequency response can be neglected [30], and the system can be treated as a Single Input Single Output (SISO) system [4].

In this paper, in order to find an SS model for these numerical data, the Vector Fitting (VF) is utilized. The VF is an iterative process, which tries to find a proper approximate transfer function or SS for the given frequency response [24]–[26], [31].

$$
f(s) \approx \sum_{m=1}^{N} \left( \frac{R_m}{s - P_m} \right) + D + sE
$$

where, $f(s)$ is the numerical frequency response, $N$ is the order of the transfer function, $R_m$ is the corresponding residue of the pole $P_m$, $D$ is the feed-through (direct input to output gain) matrix and $E$ is non-zero in cases that the transfer function is improper.

The following issues should be addressed in the approximation process: 1) up to which frequency should the fitting be done? Due to the digital nature of the controller, it is suggested to evaluate the system up to the Nyquist frequency, which is half of the sampling frequency [32], [33]. 2) What is the suggested order for the fitting process? As a general rule, the minimum order that can minimize the fitting error should be used [24]. However, there are cases where such decisions cannot be made. Therefore, in this paper an investigation is carried out with different system orders in order to see what happens if over-fitted models are used. 3) What are the effects of the measurement noise in the fitting process? In this paper for the sake of simplicity and a clearer presentation, the noise is not considered, however, there are different statistical methods to minimize the noise effect in the system identification.

### IV. SIMULATION RESULTS

In this section the proposed method is explained by two test cases. The first case is formed of 5 converters and is a simple study case where all models are linear. The second case is a more comprehensive case, which includes an active inverter and an active rectifier, and the effects of the Signal Conditioning Filter (SCF), PLL and dc link voltage controller are considered. In the first case, since the model is linear and symmetrical, the study is carried out in the phase domain. However, for the second case the linearization is performed in the synchronous reference frame.

![Figure 1](image-url) The frequency characteristic of the considered converters [15] (a) the magnitude plot (b) the phase plot.
A. A Linear Case study

Fig. 2 shows the considered power system, which is based on the Cigré LV benchmark system [34]. The current control is done using a Proportional Resonant controller as shown in Fig. 2, and the parameters of the electrical system and controllers are listed in Table I. Depending on which converters are connected or disconnected, different stable and unstable cases can be seen [15], [35]. Table II shows a few different configurations and Fig. 3 is the time domain simulation considering those cases.

Fig. 4 shows the magnitude plot of the admittance of Inverter 2 and the accuracy of the identified models (magnitude of the absolute error) with 6th, 8th and 12th orders inductors. The controller internal control structure.

For elements where the transfer function is accessible, one can find the equivalent SS representation. For instance, the SS equations of the network can directly be obtained from the differential equations describing the system dynamics (notice the notations and directions in Fig. 2) as (14) and (15).

Fig. 5 shows the considered power system as a control block diagram in order to show how CCM can be utilized. The \( L_j \), \( L_2 \), \( L_3 \) and \( L_4 \) interconnection matrices of (9) and (11) are given as (16). The inputs and outputs are highlighted with red and blue signals, respectively. The elements of \( K_{\text{cmp}} \) and \( Y_{\text{cmp}} \)

![Diagram](image-url)

**Fig. 2.** The considered power system [15], which is based on Cigré LV benchmark system [34]; (a) the overall power scheme, (b) the converter internal control structure.

![Diagram](image-url)

**Fig. 3.** Time domain simulations for different cases [15] shown in Table II.
vectors are also highlighted in the Fig. 5. Any signal can be considered as the system input and output, however as an example, the grid voltage $v_{c}$ is considered as the input to the overall system and $v_{pcc}$ is considered as the output.

$$L_{1} = \begin{bmatrix} [0]_{5 \times 5} & [1]_{5 \times 1} \\ [1]_{5 \times 5} & [0]_{5 \times 1} \end{bmatrix}, \quad L_{2} = \begin{bmatrix} [1]_{5 \times 1} \\ [0]_{6 \times 1} \end{bmatrix}$$

$$L_{3} = \begin{bmatrix} [0]_{1 \times 5} & 1 \end{bmatrix}, L_{4} = [0]$$

1) Challenges in the VF

The CCM as described above can be utilized to build up the entire SS model of the system and to study the system dynamics [23]. Fig. 6 shows the pole plot of the entire system (for Case 5) for different identification orders that is zoomed in for a better view and the reader cannot see all the high frequency poles. Time domain simulations for a detailed switching model as shown in Fig. 3 indicate the stable operation of Case 5. However, there are some RHP poles in the identified system as listed in Table III.

Fig. 6. The pole plot of the entire system (as shown in Fig. 2) for Case 5.

<table>
<thead>
<tr>
<th>Unstable poles depending on the order [s⁻¹]</th>
<th>6th</th>
<th>8th</th>
<th>12th</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>-</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td></td>
<td>1.04e7</td>
<td>1.69e6</td>
<td>0.88e7</td>
</tr>
</tbody>
</table>

One may think that the unstable identified poles are caused by overfitting, because the unstable poles do not appear for the 6th order, but the problem is indeed caused by the lack of information for the frequencies beyond the trained range of the frequency. Fig. 7 shows the sum of admittances of the converters for Case 5 ($Y_{1} + Y_{2} + Y_{3}$) for the original data and the fitted data with different orders. It can be seen that at the high frequency range, beyond the trained range, there is a non-passive region, which causes those unstable poles reported in TABLE III for the 8th order model. Actually, this is the reason why passivity enforcement is necessary in the VF. Passivity enforcement is the process during the VF to make sure that the model is passive at all frequencies even beyond the trained range [36]. This can be done by enforcing the Hamiltonian matrix of the identified system to have no imaginary eigenvalues [37]. Passivity enforcement is necessary in approximating the passive elements such as transformers, because the models will afterwards be used in time domain simulations and if they are non-passive, they might make the system unstable. However, this is not a
concern in this study, because: 1) the aim of this paper is not to develop a model for time domain simulations, in fact evaluating the stability is the target here. 2) a power converter is not a passive component due to [33]: a) the time delay, computational and PWM delay which affect the high frequency region b) The current controller which affects the current control bandwidth (for example a Constant Power Load introduces a negative resistance in the control bandwidth) c) The low frequency outer loop controllers (e.g. PLL, voltage and power controller), which affect the low frequency range.

Therefore, the passivity enforcement is not applicable for power converter approximation. The proposed workaround in this paper is to limit the frequency of the identified poles of the total system. In other words the system is trained up to 10 kHz, therefore, the identified poles beyond this range must be disregarded. It can easily be done by removing the poles, which are outside the confidence circle as shown in Fig. 8.

2) Participation factor analysis

By removing the high frequency poles from the study, the Participation Factor (PF) analysis can be done by some simple matrix operations [20], [21]. For the \( i \)-th pole, the participation analysis can be done using

\[
P_{ki} = \frac{\partial \lambda_i}{\partial a_{kk}} = \Phi_{ki} \Psi_{ik}
\]

where, \( \Phi_{ki} \) is the right eigenvector of the \( i \)-th eigenvalue, \( \Psi_{ik} \) is the left eigenvector of the \( i \)-th eigenvalue, and \( P_{ki} \) indicates the contribution of the \( k \)-th state on the \( i \)-th pole.

In this section Case 2, which is unstable, is considered [15], [35]. It can be seen in Fig. 9 that the instability is due to an eigenvalue at (229±j8180) rad/s. Table IV shows the five largest contributors to this unstable pole and also indicates that despite different approximation orders they identify the contribution levels to be almost the same. It can be seen that Inverter 1 has the most contribution to the unstable pole. Since the model is a black box, no more conclusions can be made on which part of Inverter 1 is causing the instability. However, by informing the supplier about this, they can improve the stability by looking at the frequency of stability.

3) Time domain simulations

As discussed in section II.A, an eigenvalue contains information about the transient response, i.e. how fast the transient decays/grows and at which frequency. In this section,

\[\text{TABLE IV. THE PARTICIPATION FACTOR ANALYSIS FOR CASE 2 THAT IS UNSTABLE.}\]

<table>
<thead>
<tr>
<th>State Name</th>
<th>PF</th>
<th>State Name</th>
<th>PF</th>
<th>State Name</th>
<th>PF</th>
</tr>
</thead>
<tbody>
<tr>
<td>INV1.State 3</td>
<td>0.296</td>
<td>INV1.State 4</td>
<td>0.294</td>
<td>INV1.State 5</td>
<td>0.295</td>
</tr>
<tr>
<td>INV1.State 4</td>
<td>0.302</td>
<td>INV1.State 5</td>
<td>0.300</td>
<td>INV1.State 6</td>
<td>0.300</td>
</tr>
<tr>
<td>INV2.State 3</td>
<td>0.167</td>
<td>INV2.State 3</td>
<td>0.167</td>
<td>INV2.State 7</td>
<td>0.167</td>
</tr>
<tr>
<td>INV2.State 4</td>
<td>0.169</td>
<td>INV2.State 4</td>
<td>0.169</td>
<td>INV2.State 7</td>
<td>0.169</td>
</tr>
<tr>
<td>Grid.State 1</td>
<td>0.112</td>
<td>Grid.State 1</td>
<td>0.112</td>
<td>Grid.State 1</td>
<td>0.112</td>
</tr>
</tbody>
</table>
the previously presented cases are reviewed again by means of time domain simulations. Simulations are carried out in PLECS [38] using a very detailed switching model. The controller is exactly modeled by using triggered subsystems to mimic the sampled-based control loop in a real DSP. The single update PWM is used in this paper, which is the reason the sampling and switching frequencies are equal. The most critical eigenvalue, which has the lowest damping, in Case 5 is $-64 \pm 8254j$, which indicates an oscillation frequency of 8254 rad/s and a time constant of 1/64 seconds. It can be seen in Fig. 10 that the oscillation frequency in Case 5 after a perturbation is accurately anticipated. The measured time constant is also roughly correct, since the oscillation magnitude (peak to peak) is changed -61 % from $t_1=0.203$ to $t_2=0.211$ [s]. However, a -47% drop is predicted by the decaying/growing exponential function (18).

$$\frac{I_2}{I_1} = e^{(t_2-t_1)/\tau} \tag{18}$$

where, $\tau=1/\sigma$ is the time constant (for a stable pole it is negative), and $I_2$ and $I_1$ are the current magnitudes at $t=t_2$ and $t=t_1$, respectively.

Similar study is also done for the Case 2, which is unstable. The unstable eigenvalues are $229\pm j8180$ rad/s. The highlighted oscillation frequency in Fig. 11 is almost the same the imaginary part of the predicted eigenvalue. In the simulation the peak to peak magnitude is changed 962% from $t_1=0.203$ to $t_2=0.213$ [s], which indicates a good correlation with the predicted change of 887% using (18).

B. A nonlinear case

Linearized models should be used for small-signal stability analysis of nonlinear systems. Therefore, the first step in analyzing the stability using the proposed method is to find the steady state operating point that can be obtained after a load flow. In this paper the linearization is performed in a synchronously rotating frame (the dq frame), where each ac quantity can be modelled by two dc signals (d- and q-channels).

In contrast to linear systems, the linearized nonlinear models are dependent on an operating point, and as shown in [39], by changing the operating point the admittance/impedance characteristics would be different. Therefore, for each condition (e.g. different active and reactive power generation) a new set of numerical data should be used for identification. In [39] it has been shown that by some simple sensitivity studies the admittance/impedance can be found for any operating point. It should also be noted that power system elements are mostly operated very close to the nominal conditions. Therefore, assuming a constant admittance profile for studies seems reasonable. Furthermore, it should also be taken into account that providing the correct data for studies is the suppliers’ responsibility. Therefore, in this part the given characteristics are for the given operating point and finding the operating point dependent characteristics is out of scope of this paper.

Another important point is that the nonlinear behavior in the power electronic devices mostly happens in the low frequency range (i.e. less than two times the fundamental frequency) due to the fact that the outer loop controllers have a bandwidth much slower than the current controller. Therefore, if the objective is to study the interactions in the harmonic frequency range (medium to high frequency), linear models can be used in a similar way to the previous case, where PLL dynamics are neglected [4].

Outer loop control (dc link control, power control and synchronization loop) generally results in an Multi-Input Multi-Output (MIMO) control system, where the impedance characteristics cannot be considered as in a SISO system [30], [40]. In phase (sequence) domain modelling, they result in appearance of some frequency couplings, i.e. if a small signal voltage perturbation is applied at the converter terminals, then the converter will respond with different frequencies. In the case of a balanced system with a current controller in the dq frame and a simple SRF PLL, the response includes $\omega_p$ and $2\omega_1$-2$\omega_p$ where $\omega_p$ is the perturbation frequency and $\omega_1$ is the fundamental frequency. Then a 2x2 matrix must be used as the converter admittance/impedance for small signal stability analysis. In the dq domain modelling, normally impedances are defined as 2x2 dq impedances, and since the operating point is a dc signal (as long as the system is balanced) in the dq frame the aforementioned frequency couplings do not happen.

In this section to study the effects of the synchronization loop (PLL) and the dc link control, a test case as shown in Fig. 12 is considered. The Voltage Source Inverter (VSI) injects active current to the PCC while the Active Front End (AFE) feeds a dc load by absorbing active power from the PCC. This system is based on the test system considered in [41] and the parameters are listed in Table V. The power circuit and the
control structure of the VSI and the AFE are shown in Fig. 13. The SCF block acts as a low-pass filter to attenuate the high frequency content from the measurements. The dc link in the AFE is controlled by a PI controller, which absorbs more active power if there is a drop in dc link voltage. The terminal voltage limiter can also be measured in the dq domain, and finally the same methodology as in the previous case is followed here. The admittances are not SISO, hence, the Matrix Fitting (MF) should be utilized, which is the MIMO version of the VF [24]–[26], [31]. It must be noted that a slightly different method than [31] should be used because [31] assumes the transfer function matrix is symmetrical, which is not the case in dq impedances.

Two scenarios are reported in this part, one is stable and the other one is intentionally made unstable by increasing the integrator gain of the PLL of the VSI (see Table V). Fig. 14 shows the original admittance data where the difference is located at the low frequency range, since the PLL is changed. The SS model of the network can be obtained as

$$\dot{x} = A_{net}x + B_{net}u = \begin{bmatrix} \frac{1}{R_g} & -\frac{1}{L_g} \\ \frac{1}{C_L} & -\frac{1}{C_L R_g} \end{bmatrix} \begin{bmatrix} \Delta v_g \\ \Delta i_L \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u \tag{19}$$

where, \(\Delta\) is used to emphasize that small signal incremental equations are used. It should be noted that the above equations are valid for a single-phase system. For a three-phase system

### Table V. Parameters of the Nonlinear Power System.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>(V_s)</td>
<td>Grid voltage (phase voltage rms) [V]</td>
<td>120</td>
</tr>
<tr>
<td>(f_s)</td>
<td>Grid frequency [Hz]</td>
<td>60</td>
</tr>
<tr>
<td>(R_L)</td>
<td>Resistance of local passive load [(\Omega)]</td>
<td>10</td>
</tr>
<tr>
<td>(C_L)</td>
<td>Capacitance of local passive load [(\mu F)]</td>
<td>250</td>
</tr>
<tr>
<td>(L_g)</td>
<td>Grid inductance [mH]</td>
<td>0.2</td>
</tr>
<tr>
<td>(R_g)</td>
<td>Grid resistance [(\Omega)]</td>
<td>1.1</td>
</tr>
<tr>
<td>(L_{LVSI})</td>
<td>Inductance of the inverter [mH]</td>
<td>1.0</td>
</tr>
<tr>
<td>(R_{LVSI})</td>
<td>Self-resistance of (L_{LVSI}) [(\Omega)]</td>
<td>120</td>
</tr>
<tr>
<td>(V_{dc})</td>
<td>DC link voltage [V]</td>
<td>600</td>
</tr>
<tr>
<td>(i_{d,ref})</td>
<td>d channel current reference [A]</td>
<td>140</td>
</tr>
<tr>
<td>(i_{q,ref})</td>
<td>q channel current reference [A]</td>
<td>0</td>
</tr>
<tr>
<td>(k_{pVSI})</td>
<td>Proportional gain of current controller</td>
<td>0.0105</td>
</tr>
<tr>
<td>(k_{iVSI})</td>
<td>Integrator gain of current controller</td>
<td>1.1519</td>
</tr>
<tr>
<td>(k_{pAFE})</td>
<td>Proportional gain of PLL</td>
<td>0.1</td>
</tr>
<tr>
<td>(k_{iAFE})</td>
<td>Integrator gain of PLL</td>
<td>0.32</td>
</tr>
<tr>
<td>(L_{AFE})</td>
<td>Inductance of the AFE [mH]</td>
<td>0.5</td>
</tr>
<tr>
<td>(R_{AFE})</td>
<td>Dc link capacitor [(\mu F)]</td>
<td>90</td>
</tr>
<tr>
<td>(C_{d,AFE})</td>
<td>Dc link voltage [(\mu F)]</td>
<td>100</td>
</tr>
<tr>
<td>(R_c)</td>
<td>Dc load resistance [(\Omega)]</td>
<td>13.825</td>
</tr>
<tr>
<td>(V_{dc})</td>
<td>DC link voltage reference [V]</td>
<td>600</td>
</tr>
<tr>
<td>(i_{d,ref})</td>
<td>q channel current reference [A]</td>
<td>0</td>
</tr>
<tr>
<td>(k_{pAFE})</td>
<td>Proportional gain of current controller</td>
<td>0.0052</td>
</tr>
<tr>
<td>(k_{iAFE})</td>
<td>Integrator gain of current controller</td>
<td>1.152</td>
</tr>
<tr>
<td>(k_{pAFE})</td>
<td>Proportional gain of dc link voltage controller</td>
<td>0.0628</td>
</tr>
<tr>
<td>(k_{iAFE})</td>
<td>Integrator gain of dc link voltage controller</td>
<td>45.45</td>
</tr>
<tr>
<td>(k_{pAFE})</td>
<td>Proportional gain of PLL</td>
<td>0.05</td>
</tr>
<tr>
<td>(k_{iAFE})</td>
<td>Integrator gain of PLL</td>
<td>0.5</td>
</tr>
<tr>
<td>(SCF)</td>
<td>Signal Conditioning Filter</td>
<td>(-\frac{\omega_0^2}{s^2 + 2\xi\omega_0 + \omega_0^2})</td>
</tr>
<tr>
<td>(\omega_0)</td>
<td>Natural frequency of SCF [rad/s]</td>
<td>1.23e6</td>
</tr>
<tr>
<td>(\xi)</td>
<td>Damping factor of SCF [rad/s]</td>
<td>4.74e-13</td>
</tr>
<tr>
<td>(f_{sw})</td>
<td>Switching/sampling frequency [kHz]</td>
<td>20</td>
</tr>
<tr>
<td>(T_{del})</td>
<td>Time delay due to the digital control</td>
<td>1.5/f_{sw}</td>
</tr>
</tbody>
</table>

Fig. 12. The considered nonlinear power system [41] with a Voltage Source Inverter (VSI) and an Active Front End (AFE).

Fig. 13. The power circuit and control structure of (a) the Voltage Source Inverter (b) the Active Front End.
the equations can be transformed into dq domain [42] using
\[
A_{dq} = \begin{bmatrix} A_{net} & -\omega_1 I \\ \omega_1 I & A_{net} \end{bmatrix}, \quad B_{dq} = \begin{bmatrix} B_{net} \\ 0 \end{bmatrix}, \\
C_{dq} = \begin{bmatrix} C_{net} \\ 0 \end{bmatrix}, \quad D_{dq} = \begin{bmatrix} D_{net} \\ 0 \end{bmatrix}
\]
(20)

where, \( I \) is the identity matrix of the appropriate size.

Now the CCM can be applied to get the overall SS matrices of the whole system. Fig. 15 shows the identified poles of the system for the stable (in blue) and unstable (in red) cases. Fig. 16 shows the time domain results of the PLL output of the VSI.
for stable and unstable cases when a perturbation is applied. The measured frequencies in Fig. 16 are almost the same as the imaginary part of the highlighted poles, which are the poles with the minimum damping. Furthermore, the exponential curves in Fig. 16 (a) and (b), which are based on the real part of the predicted poles as mentioned in (18), show a good agreement between the time constant in the simulations with the proposed method.

1) Participation Factor Analysis

By using (17) the participation factor analysis for the unstable pole in the second case is carried out. Table VI shows the three largest contributors to this instability, where it meets the expectation, since the reason of instability was the increase in the PLL gain of the VSI.

V. CONCLUSION

In this paper, the eigenvalue-based stability analysis is used to evaluate stability of a system with multiple converters. The converters are modelled as black boxes where no information about the internal structure and parameters are available. The VF is used to find a proper SS model, however there are uncertainties in the modelling. It is shown that some models might result in a non-passive model and a method is proposed to exclude the irrelevant poles from the study. Also, the participation factor analysis is utilized to quantify how much each component is responsible for the observed instability. A nonlinear case with synchronization loops and a dc link voltage control, which is linearized in the dq domain, is also presented to show that the Matrix Fitting can successfully be used for the analysis of MIMO systems.

REFERENCES


| TABLE VI. THE PARTICIPATION FACTOR ANALYSIS FOR THE UNSTABLE CASE. |
|---------------------------------|----------------|
| **State Name** | **PF** |
| VSIState 15 | 0.44 |
| VSIState 16 | 0.35 |
| AFEState 17 | 0.19 |
Mohammad Kazem Bakhshizadeh (S’16) received the B.S. and M.S. degrees in electrical engineering from the Amirkabir University of Technology, Tehran, Iran in 2008 and 2011, respectively. He is currently an industrial PhD student at Aalborg University, Aalborg, Denmark in collaboration with DONG Energy Wind Power, Fredericia, Denmark. In 2016, he was a visiting scholar at Imperial College London, London, U.K. His research interests include power quality, modeling and control of power converters, and grid converters for renewable energy systems.

Changwoo Yoon (S’08) received the B.S. and M.S. degrees from the Department of Control and Instrumentation Engineering, Seoul National University of Technology, Korea, in 2007 and 2009, respectively. He was an engineer at the Advance Drive Technology Co., Anyang, Korea from 2009 to 2013. He received his PhD in 2017 at the Department of Energy Technology (ET) at Aalborg University (AAU) in the field of small-scale power system stability. In 2015, he was a visiting scholar at University of Manitoba, Canada. His main research interests include power electronics for distributed generation, power quality and high power dc–dc converter for renewable energy.

Jesper Hjerrild was born in 1971. He holds an MSc and PhD degrees in electrical engineering from the Technical University of Denmark, Lyngby, in 1999 and 2002, respectively. Currently, he is employed with DONG Energy. His main technical interest is electrical power systems in general, involving a variety of technical disciplines including modeling of power system including wind power and power system control, stability and harmonics. Furthermore, he also works with designing of the wind farm.

Claus Leth Bak was born in Århus, Denmark, on April 13th, 1965. He received the B.Sc. with honors in Electrical Power Engineering in 1992 and the M.Sc. in Electrical Power Engineering at the Department of Energy Technology (ET) at Aalborg University (AAU) in 1994. After his studies he worked as a professional engineer with Electric Power Transmission and Substations with specializations within the area of Power System Protection at the NV Net Transmission Company. In 1999 he was employed as an Assistant Professor at ET-AAU, where he holds a Full Professor position today. He received the PhD degree in 2015 with the thesis “EHV/HV underground cables in the transmission system”. He has supervised/co-supervised +35 PhD’s and +50 MSc theses. His main Research areas include Corona Phenomena on Overhead Lines, Power System Modeling and Transient Simulations, Underground Cable transmission, Power System Harmonics, Power System Protection and HVDC-VSC Offshore Transmission Networks. He is the author/coauthor of app. 240 publications. He is a member of Cigré JWG C4-B4.38, Cigré SC C4 and SC B5 study committees’ member and Danish Cigré National Committee. He is an IEEE senior member (M’1999, SM’2007). He received the DPS 2014 best paper award and the PEDG 2016 best paper award. He serves as Head of the Energy Technology PhD program (+ 100 PhD’s) and as Head of the Section of Electric Power Systems and High Voltage in AAU and is a member of the PhD board at the Faculty of Engineering and Science.
Łukasz Hubert Kocewiak (M’12, SM’16) holds BSc and MSc degrees in electrical engineering from Warsaw University of Technology as well as PhD degree from Aalborg University. Currently he is with DONG Energy Wind Power and is working as a senior power system engineer on development of electrical infrastructure in large offshore wind power plants. The main direction of his research is related to harmonics and nonlinear dynamics in power electronics and power systems especially focused on wind power generation units. He is the author/co-author of more than 60 publications. He is a member of various working groups within Cigré, IEEE, IEC.

Frede Blaabjerg (S’86–M’88–SM’97–F’03) was with ABB-Scandia, Randers, Denmark, from 1987 to 1988. From 1988 to 1992, he got the PhD degree in Electrical Engineering at Aalborg University in 1995. He became an Assistant Professor in 1992, an Associate Professor in 1996, and a Full Professor of power electronics and drives in 1998. From 2017 he became a Villum Investigator. His current research interests include power electronics and its applications such as in wind turbines, PV systems, reliability, harmonics and adjustable speed drives. He has published more than 450 journal papers in the fields of power electronics and its applications. He is the co-author of two monographs and editor of 6 books in power electronics and its applications. He has received 18 IEEE Prize Paper Awards, the IEEE PELS Distinguished Service Award in 2009, the EPE-PEMC Council Award in 2010, the IEEE William E. Newell Power Electronics Award 2014 and the Villum Kann Rasmussen Research Award 2014. He was the Editor-in-Chief of the IEEE TRANSACTIONS ON POWER ELECTRONICS from 2006 to 2012. He has been Distinguished Lecturer for the IEEE Power Electronics Society from 2005 to 2007 and for the IEEE Industry Applications Society from 2010 to 2011 as well as 2017 to 2018. He is nominated in 2014, 2015 and 2016 by Thomson Reuters to be between the most 250 cited researchers in Engineering in the world. In 2017 he became Honoris Causa at University Politehnica Timisoara (UPT), Romania.

Bo Hesselbæk received the M.Sc. degree in electrical engineering from Aalborg University, Aalborg, Denmark, and the MBA from the University of Southern Denmark, Odense, Denmark. The first years of his career, he was with the Danish Transmission System Operator both within transmission planning and operation. Since 2008, he has been with Vestas Wind Systems, Aarhus, Denmark, where he was Director of Vestas R&D America, until 2012, when he moved to DONG Energy Wind Power, Fredericia, Denmark, to head a department that designs the main electrical infrastructure of offshore wind farms. He holds multiple patents and publications.