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Article

Lifetime Estimation and Failure Risk Analysis in a Power Stage Used in Wind-Fuel Cell Hybrid Energy Systems

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Abstract: This paper presents a methodology based on the failure mode and effect analysis (FMEA) to analyze the failures in the power stage of wind-fuel cell hybrid energy systems. Besides, fault tree analysis (FTA) is applied to describe the probabilistic failures in the vital subcomponents. Finally, the reliability assessment of the system is carried out for a five-year operation that is guaranteed by the manufacturer. So, as the result, the reliability analysis proves that the metal oxide semiconductor field effect transistor (MOSFET) and electrolytic capacitor are the most critical components that introduce damages in the power circuit. Moreover, a comparative study on the reliability assessment by the exponential distribution and the Weibull distribution show that the B1 lifetime obtained by the Weibull distribution is closer to reality.

Keywords: failure mode and effect analysis; failure mechanism; power stage; reliability; wind-fuel cell hybrid energy systems

1. Introduction

Renewable energy systems are rapidly growing in the power sector industry, such as wind turbines, solar energy, and also fuel cells [1–4]. Renewable energy sources are proliferating even more than the expected estimations, although each has its pros and cons. For instance, wind turbines are dependent on wind means climate condition, while fuel cells demand hydrogen-rich fuel. Furthermore, one tricky issue is to keep power production stable; hybrid energy systems facilitate such disadvantages [5,6]. A hybrid wind-fuel cell system usually includes a wind turbine, proton exchange membrane fuel cells (PEMFC), ultracapacitor, an electrolyzer, and a power convertor. Wind turbine power output variations because of wind speed change could be reduced by a fuel cell stack. In this system, the wind turbine and the fuel cell supply the load simultaneously; in order to save extra energy produced by the wind turbine when wind is over speeding, it is converted to hydrogen utilizing an electrolyzer to be used in the fuel cell when needed. Minimizing voltage fluctuations in the system and generating AC voltage are, respectively, the ultracapacitors and the power converter functions [7,8]. PEMFC is a kind of fuel cell being developed by General Electric Corporation as a renewable energy system in many applications, such as transportation, stationary applications, and portable applications, as well as hybrid energy systems [9,10]. Generally, PEMFCs are divided into three main subsystems that contain: Power conditioner, stack, and balance

of plant (BoP) [11]. A power conditioner is one of the crucial subsystems, in which the DC/DC converter regulates the output from the PEMFC stack to a fixed DC voltage [12]. The power stage component is a critical part of the power conditioner subsystem in a PEMFC system which includes active and passive subcomponents. Active subcomponents consist of primary metal oxide semiconductor field effect transistors (MOSFETs) and secondary MOSFETs, which both could contain eight transistors, and their functions are to control the electrical current, voltage regulation, boost switching, and also rectification. Besides, there are passive subcomponents including: Input and output electrolyte capacitors, transformer, choke, varistor, shunt resistor, fuse, and heatsink. The functions of these components are filtering, transmission of current and voltage, and interconnection between different components. MOSFETs as active subcomponents and electrolytic capacitors as passive subcomponents are more significant due to their functions and applications. MOSFETs are used as a switch where the electrical current passes at a desired time interval. In addition, electrolyte capacitors work as a storage for the electrical energy and stabilization of the current voltage [13–15]. There are many studies of capacitors' reliability and failure analysis [16–18] and this paper focuses on the MOSFET as a critical active subcomponent in the power stage and carrying out a diverse failure mechanism analysis of it by failure mode and effect analysis (FMEA) technique.

Achieving a product that can meet customers' demands with the best design, construction, production, and operation costs is one of the main goals in all industries [19,20]. Reliability is a critical criterion of a product's performance, expressed in both deterministic and probabilistic approaches. In the deterministic expression, failure modes and mechanisms are often discussed based on observations, while in the probabilistic case, the failure issues are studied based on statistics [21]. Function investigations and analysis of each system require an individual function analysis of each component, its subsets, and their interaction. The advantages and disadvantages of a component entirely depend on the subsets it is used in. Evidently, the use of defective components with a short lifetime will reduce the efficiency and lifetime of the component and the main system. Therefore, prior to the reliability evaluation of a system, its related components, and failure modes, as well as failure mechanisms of its components and even critical subcomponents, should be adequately comprehended [22].

The literature review shows that the FMEA method is an essential step in conducting a failure mode and failure mechanisms evaluation [11,23]. The FMEA method has been used in multiple types of industry and it is based on discovering, arranging, and decreasing the failures or faults. The majority of the literature available on the PEMFC systems have performed a brief study about failure modes and failure mechanisms [24–26], also most studies were on system-level and non-electrical parts of the PEMFC system, such as electrochemical parts, BoP, and stack part [27–29]. Reliability, availability, and risk study of different parts of the PEMFC are important issues that should be assessed completely. For system recognition, there are main steps, which are significant for the identification of the systems and it is the basis for this study. FMEA focuses on prevention by facilitating process improvement and identifying and eliminating concerns as well as the development of a process or design [30].

Fault tree analysis (FTA) is used for reliability assessment of a system. The fault tree approach is a deductive process by means of which an undesirable event, called the top event, is postulated, and the possible ways for this event to occur are systematically deduced. The deduction process is performed so that the fault tree embodies all component failures (i.e., failure modes) that contribute to the occurrence of the top event. The fault tree itself is a graphical representation of the various combinations of failures that led to the occurrence of the top event [31]. The fault tree itself is a logical model, and thus represents the qualitative characterization of the system logic. There are, however, many quantitative algorithms to evaluate fault trees. For example, the concept of cut sets can also be applied to fault trees by using the Boolean algebra method. This methodology has been used in several applications as well as PEMFCs [32,33]. The focus of the FTA suggested in this paper is the failure of power stage as the top event by considering filters as input and output.

In this paper, the FMEA method is used for the power stage component as a central part of the power conditioner subsystem of a PEMFC system. FMEA as a technique in reliability analysis is used to rank the estimated risk priority with various potential failure modes for critical subcomponents and potential failure modes/mechanisms. According to the FTA of the power stage, it is demonstrated how the failure could happen. Furthermore, with the use of exponential and Weibull distributions by applying Monte Carlo simulation, the reliability is estimated and the reliability curve is presented within the 5-year guarantee period for the system analyzed.

2. Power Stage Components

In the wind-fuel cell system as a hybrid energy system application, the power conditioner subsystem of a PEMFC system carries out the primary power conversion from the input voltage to the output voltage. Usually, a power stage has three parts: Input filter, power amplifier, and output filter. MOSFETs are used as an active subcomponent and it are significant and important due to functions and applications. The power amplifier contained in this case is sixteen MOSFETs used as switches and rectifier where the electrical current is conducted at the desired time interval. Besides, two transformers are used to isolate the primary and secondary sides and to store transient energies during transients.

Furthermore, a voltage dependent resistor (VDR) or varistor is used as control/limit for excessive transient voltage. Both the input filter and the output filter contain the fuse, choke, shunt resistor, and an electrolytic capacitor. A shunt resistor functions as a type of current sensor used in the power stage [13,34]. The schematic of the PEMFC’s different levels and all of the main elements of the power stage are depicted and identified in Figure 1 and Figure 2, respectively.

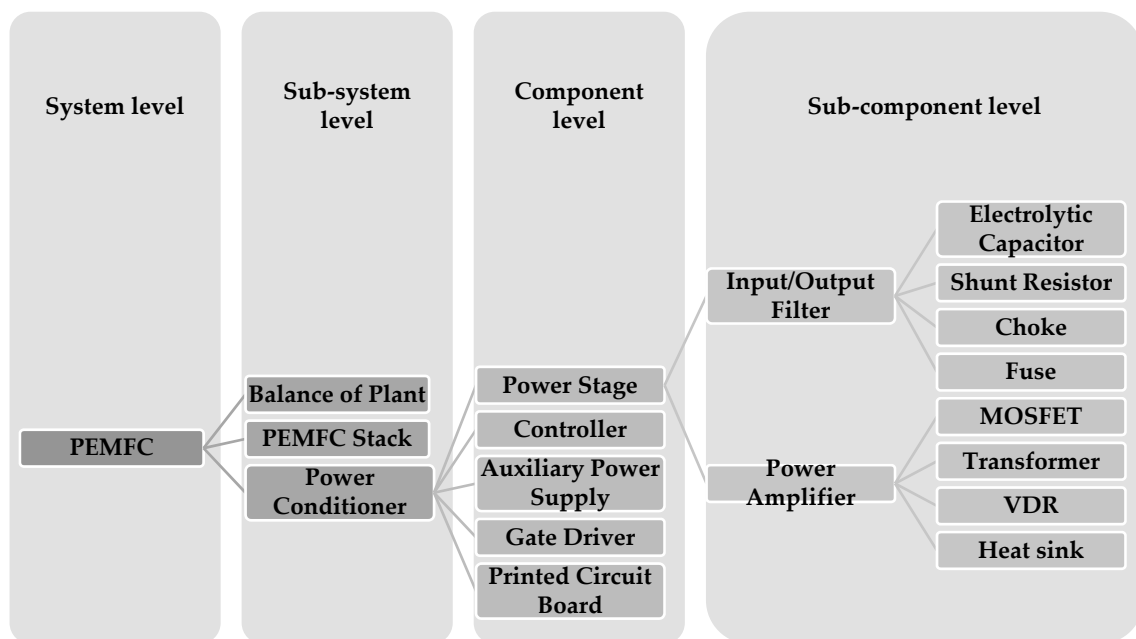


Figure 1. Simplified schematic of the proton exchange membrane fuel cell (PEMFC) categorized in different levels.

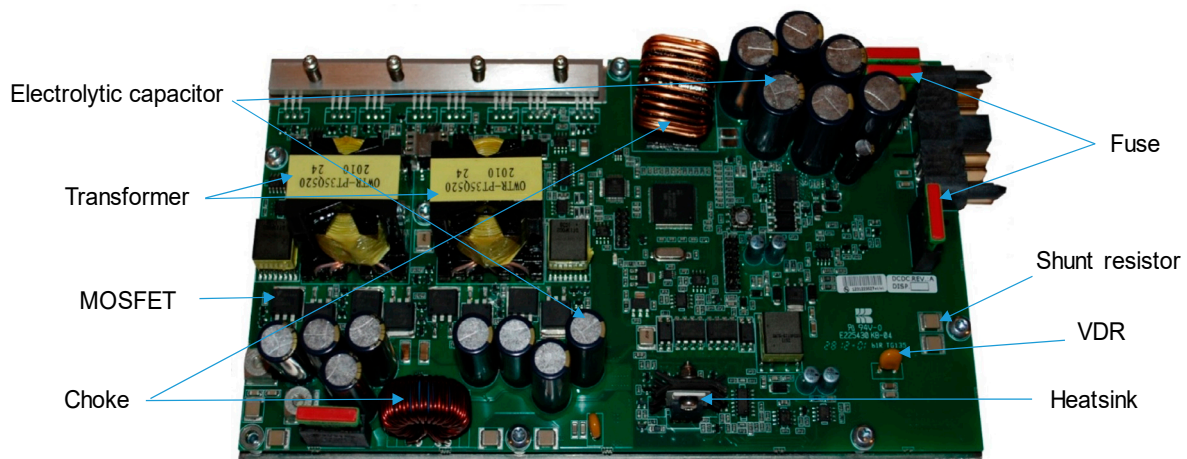


Figure 2. Critical power stage subcomponents in a power conditioner used in PEMFC.

3. Failure Mechanisms and Failure Modes Analysis

Each system has internal durability that may be varied due to particular internal or external circumstances. Failure occurs when exerted stress exceeds the capacity of a system [35]. Failure mechanisms are physical processes that cause failures or stress that, in turn, reduce the stability of the system [36]. These mechanisms are different for mechanical and electrical equipment [37]. Mechanical failure mechanisms can generally be divided into three categories: Tension creation, strength reduction, and stress increase. However, the failure mechanism in electrical equipment is more complicated than that of mechanical failure mechanism due to the complexity of electrical assemblies, which can be divided into three general categories of electrical stress (tension), inherent failure, and external failure. Each of these mechanisms will cause a functional problem and reduce the reliability [38].

First, electrical tension mechanism: Application of an exceeded voltage or current intensity to an electrical component leads to stress creation, reduced performance, or degradation. Additionally, extreme electrical currents increase the heat and local melting at sensitive points of the circuit, which often result in the catastrophic failure or hidden damages of the circuit [21,39], such as failure mechanism type of the MOSFETs and the electrolytic capacitors.

Second, inherent failure mechanism: This mechanism is related to the electronic component itself. These kinds of failure mechanisms are often related to semiconductor components/chips and the growth of active electrical layers on their surface. In general, the inherent failure mechanisms include ion contamination, gate oxide breakdown, surface charge spreading, and hot electrons [21,39]. These failures often occur due to weaknesses in the manufacturing process or incomplete print design techniques.

Third, external failure mechanism: This failure mechanism generally occurs because of external factors, such as mounting and packaging problems, and the way of connecting with other components in the unit or system environmental effects [39]. Today, due to the growth of knowledge and technology in the design and manufacturing of electronic components, external failures are more important than the inherent failure of the components. Die attachment failure, electron migration, corrosion, radiation, and internal connection failures are among common failure mechanisms of external failure in the electronic components.

Applying an exceeded voltage to the MOSFET as a top subcomponent of the power stage in a circuit is a partial and secondary fault. However, the existence of electrostatics because of high voltage discharge in this element is a partial and primary fault, leading to local melting and the oxide gate's breakdown. Both conditions, i.e., the electrostatic discharge (ESD) and the electrical over stress (EOS), are included in a subset of failures due to electrical stresses. Because of improper processing of the oxide gate or mentioned electrical stresses, differences appear in voltage and current characteristics

of the MOSFET. This defect, comprising an intrinsic failure mechanism and electrical stress, traps electrons at the common interface of the oxide gate, creating improper electrical fields and energizing electrons to enter the oxide, resulting in a threshold voltage shift and short circuit. This failure mechanism steps as an instance on the critical active subcomponent of the power stage as illustrated in Figure 3.

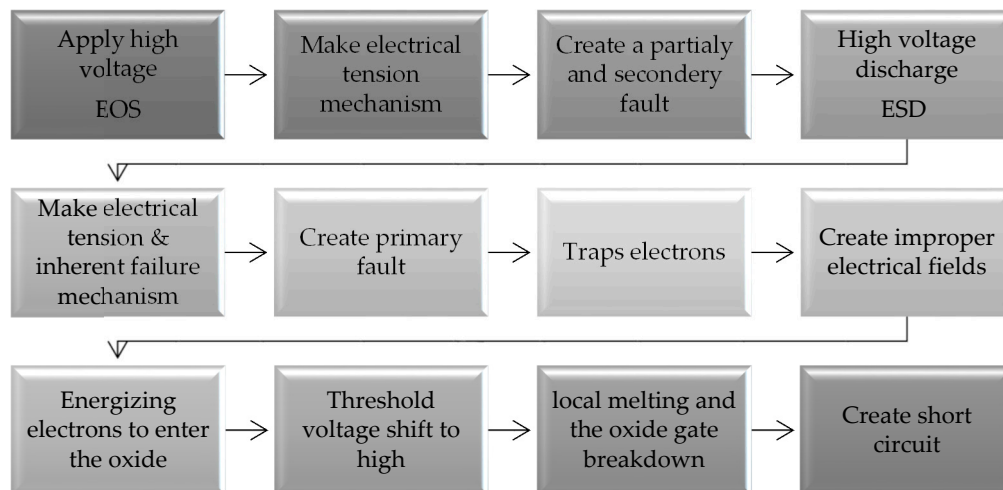


Figure 3. Failure mechanism analysis of the metal oxide semiconductor field effect transistor (MOSFET).

FMEA is an important step in the reliability assessment. The design is the primary objective of the FMEA. Another objective of the FMEA is to identify and classify the potential risk of components [40]. It can support the fault-tolerant plan, testability, security, logistic patronage, and pertaining functions for system FMEAs; the aim is to review the design and predict the damage to the system. Improvements of the test and verification of the plans are other targets of the FMEA [41]. Figure 4 shows the process of an FMEA for the power stage in the PEMFC. This methodology could be applied in the state-of-the-art of the PEMFC industry in order to overcome shortages in identifying the critical failure mechanism for each component. Occurrence (O), Detectability (D), and Severity (S) are used in the FMEA methods as three risk factors. Input parameters of three factors are scored by a four-point scale to classify different failures, depending on the case study [42]. Based on Tables 1–3, scale factors start from one to four shown in the ranking, specified for very low to high risk, respectively. Tables 1–3 show the O, D and S classification respectively [43,44]. Table 4 is the FMEA table with the top functions, failure modes, failure cause, failure mechanism, and mechanism type, as well as risk priority number (RPN) as an initial estimation of risk of subcomponents of the power stage in a PEMFC system [45,46].

By implementation of the FMEA and using the scales for severity (S), occurrence (O), and detection (D) factors and by multiplying these input factors [44], the highest risk priority percentage for each subcomponent of the power stage is recognized, which is demonstrated in the Pareto plot of RPN for each subcomponent for a power stage, as shown in Figure 5. As it can be seen, MOSFET and electrolyte capacitor are the most effective on reliability and lifetime of the power stage with around 50% risk. Furthermore, other subcomponents, like transformer and choke, are in the less priority level for risk analysis; that is why they are not considered in following sections.

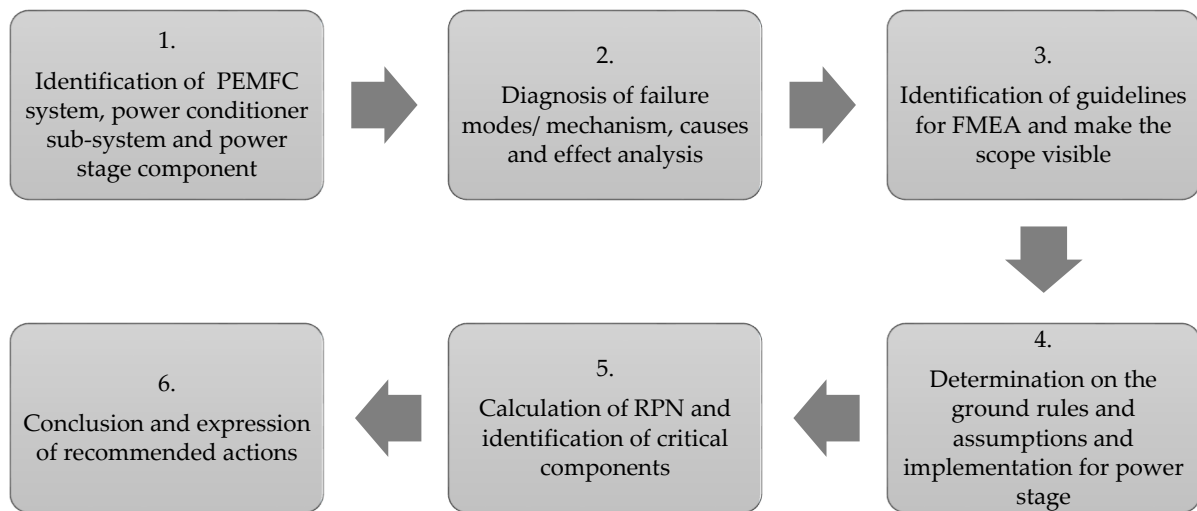


Figure 4. Failure mode and effect analysis (FMEA) process for the power stage in PEMFC.

Table 1. Occurrence (O) rating scale in FMEA analysis.

Ranking	Criteria	Description
1	Very low	Unlikely to occur at all
2	Low	Remote—once in 1 to 10 number
3	Medium	Rare—once in 10 to 100 number
4	High	Occasional—once in 100 to 1000 number

Table 2. Detection (D) rating scale.

Ranking	Criteria	Description
1	High	Detectable with a shutdown
2	Medium	Detectable according to the deviation
3	Low	Detectable by a sensor
4	Very low	Not physically detectable

Table 3. Severity (S) rating scale.

Ranking	Criteria	Description
1	Very low	Negligible changes like temperature
2	Low	Reduction in ability to work
3	Medium	Loss of ability to work
4	High	Major damage to work

Table 4. Failure modes, causes, and mechanisms of power stage components.

#	Sub-Components of Power Stage	Top Function	Top Failure Mode	Top Failure Cause	Top Failure Mechanism	Mechanism Type	S	O	D	RPN
1	Fuse	Protecting	Fail to protect	High voltage/temperature	Over voltage	Electrical tension mechanism/overstress	2	3	2	12
2	Electrolytic capacitor	Filtering and storing	Does not filter and store	High current/temperature	Leakage and Short/open circuit	Electrical tension mechanism/overstress	4	2	4	32
3	Choke	Smoothing and resist changing	Fail to smooth and resist changing	Manufacturing defect and high temperature	Short/open circuit	Inherent failure mechanism/wear out	3	3	3	27
4	Shunt resistor	Measuring of currents	Fail to measure currents	Manufacturing defect and high temperature	Overvoltage	Inherent failure mechanism/wear out	3	2	2	12
5	MOSFET	Protection and regulation	Fail to switch and regulation	High voltage/current/temperature	Gate oxide short/breakdown, EOS, ESD	Electrical tension mechanism/overstress	4	3	4	48
6	VDR	Compensating voltage	Does not compensate voltage	Manufacturing defect and high temperature	Overvoltage	Electrical tension mechanism/overstress	2	2	2	8
7	Transformer	Inducting and reinforcing	Does not reinforce	Manufacturing defect and high temperature	Leakage and short/open circuit	Inherent failure mechanism/wear out	3	3	3	27
8	Heatsink	Heat reducing	Does not heat reduce	Manufacturing defect	Thermal damage	External failure mechanism/overstress	2	1	2	4

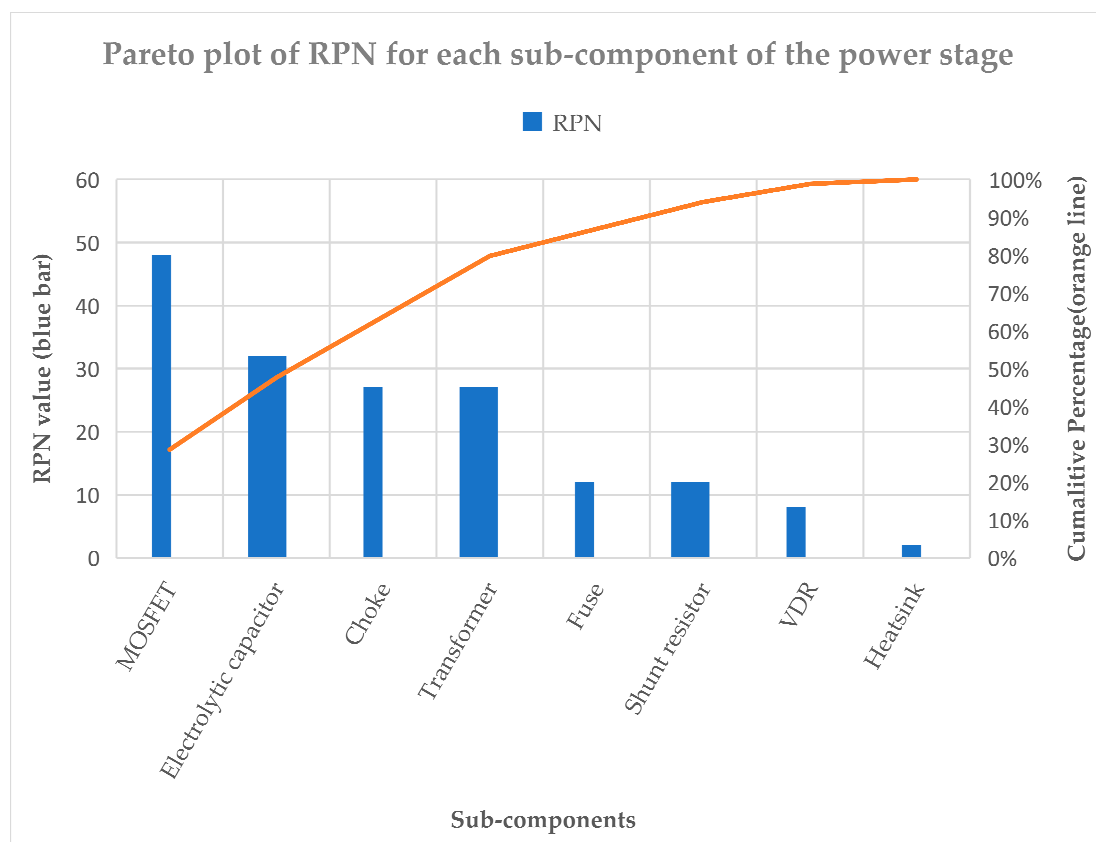


Figure 5. The Pareto plot of risk priority number (RPN) for each subcomponent of the power stage.

4. Fault Tree Analysis

This section is dedicated to introducing failures of the power stage, where the relationship among their subcomponents is delineated by means of the fault tree. The FTA is a deductive method based on the assumption of an unacceptable situation or an event contrary to the main purpose of the system. This unacceptable situation/event is called the “top event”. In the analysis of the fault tree, it is required to distinguish a component fault from a system fault that results from more than one component [33,47]. Also, the classification of failures into primary and secondary categories will be advantageous in the estimation of the fault tree. That means primary failures include occurrence under normal/tolerable (designed) system conditions, while secondary failures occur in a component and in a state that the system is not designed, and they are usually caused by inappropriate external conditions [48]. The fault tree of the power stage is shown in Figure 6.

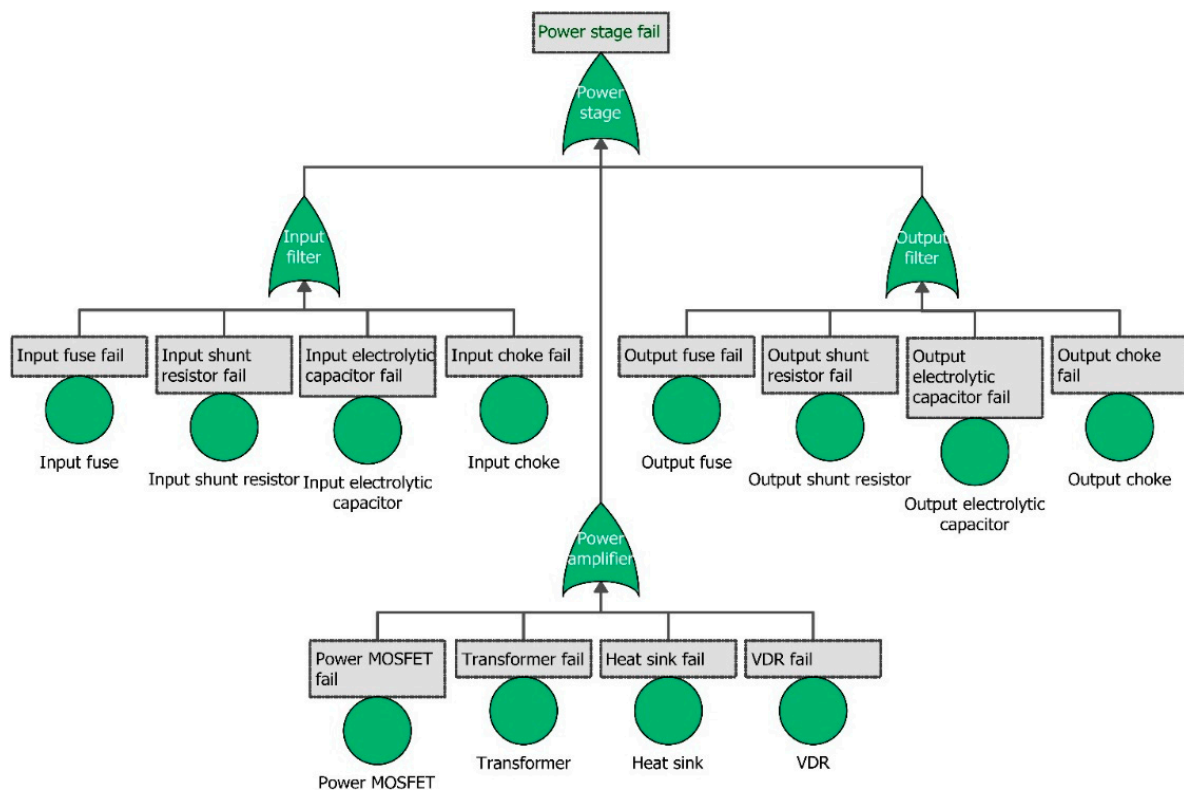


Figure 6. Fault tree of the power stage of PEMFC.

The investigation is performed through the whole reliability conditions and calculates the results for each component by using the probabilistic reliability generic data of the power stage [7,13]. Using MIL-HDBK-217F (Military Handbook: Reliability Prediction of Electronic Equipment), as well as some physics of failure-based and mission profile-based approaches [12], all data are collected for the FTA. Reliability of exponential distribution is given by Equation (1):

$$R(t) = \exp(-\lambda.t) \tag{1}$$

where, $R(t)$ is the reliability over time t , and λ is the failure rate. Moreover, reliability of Weibull distribution is given by Equation (2):

$$R(t) = \exp \left[-\left(\frac{t}{\eta}\right)^\beta \right] \tag{2}$$

where, β is the shape parameter, and the scale parameter is η . The shape parameter is also known as the Weibull slope [49,50]. It should be mentioned that by considering β equals 1 in the Weibull distribution, it would be exactly an exponential distribution, which can show the useful life part of the bathtub curve throughout the product lifecycle failure rate, Equation (3).

$$\lambda = \frac{\beta}{\eta} \cdot \left(\frac{t}{\eta}\right)^{\beta-1} \text{ if } \beta = 1 \Rightarrow \eta = \frac{1}{\lambda} \quad (3)$$

Table 5 illustrates all critical subcomponents of the power stage with their failure rates and Weibull parameters, calculated based on Equation (3).

Table 5. Failure rate and Weibull parameters.

System	Components	Failure Rate (λ)	Weibull Parameters	
			Shape Parameter (β)	Scaling Parameter (η)
Power stage	Fuse	0.02×10^{-6}	1	5.00×10^7
	Electrolytic capacitor	0.11×10^{-6}	1	8.33×10^6
	Choke	0.16×10^{-9}	1	5.95×10^9
	Shunt resistor	0.43×10^{-9}	1	2.31×10^9
	MOSFET	0.58×10^{-6}	1	1.91×10^6
	VDR	0.43×10^{-9}	1	2.31×10^9
	Transformer	0.15×10^{-6}	1	6.51×10^6
	Heatsink	0.06×10^{-6}	1	1.66×10^7

5. Results and Discussion of Reliability Analysis

The reliability curve in Figure 7 shows the system reliability along with time when the reliability is the probability of the system not failed by time. The reliability is calculated by implementing Monte Carlo simulation with point results every 100 h with start time 1 h and end time five years for 1000 number of simulations of the system using the ReliaSoft BlockSim software package. The reliability curve of the power stage, along with the operating years, is illustrated in Figure 6. It is noted that the B1 lifetime is estimated at 21,300 h (887.5 days) in the case of a shape parameter one ($\beta = 1$) for all of components shown in Table 2, which is illustrated with the blue color. However, reliability curve with the red color shows B1 at 40,900 h (1704 days) because it has different shape parameters estimated just for MOSFET and electrolytic capacitor; their shape parameter values are taken from [7], 2.59 and 1.93, respectively. Hence, scaling parameters are estimated 1.61×10^6 for the MOSFET and 2.18×10^6 for the electrolytic capacitor. In fact, this figure clearly illustrates more realization in comparison with not considering Weibull distribution for reliability analysis. In other words, the obtained reliability curve of the system from the Weibull data is very close to the reality experienced in the system.

Consequently, failure analysis shows that two subcomponents of the power stage, which contains MOSFET as an active component and electrolytic capacitor as a passive component, have the most effect on the changes of the reliability as well as the critical failure and hidden damages to the circuit of the system as discussed and demonstrated before in the Pareto plot (Figure 5) from risk analysis of each subcomponent of the power stage based on the FMEA technique. By inserting the Weibull parameter (blue curve) for these two components in the reliability analysis, the results are more reasonable rather than exponential distribution (red one).

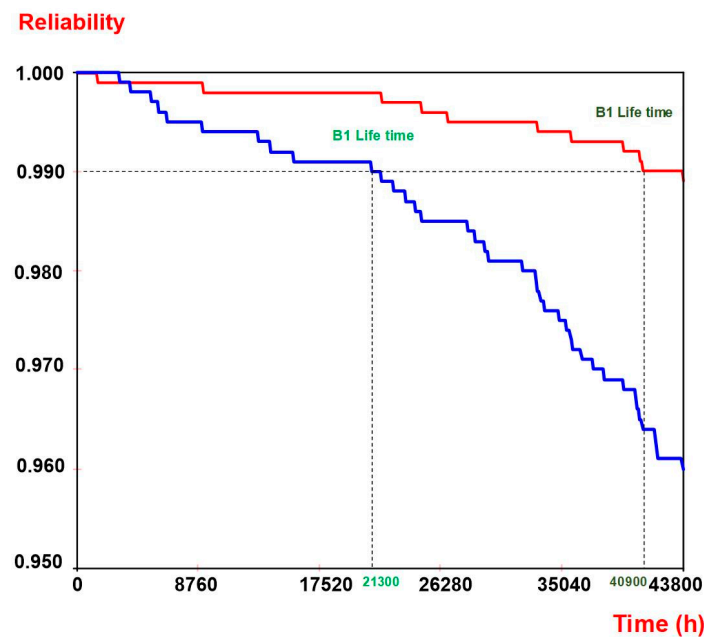


Figure 7. Reliability curve of power stage along with the operating hours (blue, Weibull distribution; red, exponential distribution).

The results of the proposed methodology are comparable and complementary with the results of other methodologies. For example, considering the critical power electronic components, the annual accumulated damage is estimated, due to the real mission profile of the fuel cell system. Then, the Monte Carlo analysis is applied to obtain the Weibull distribution of the power semiconductors lifetime. The presented reliability estimation and findings using FMEA and FTA by assuming Weibull distributions have their pros and cons. For instance, it is more detailed, focusing on subcomponents, components, and system; on the other hand it is more understandable, simple, easy, and faster.

6. Conclusions

This paper has presented a failure mechanism analysis of the power stage components in a hybrid wind-fuel cell system by using the FMEA and the FTA. The FMEA identified and analyzed the failure mechanism of power stage components for selected critical subcomponents, which their failures may have significant effects on the system reliability. Some of the failure modes of an active subcomponent such as MOSFET are switching losses, conduction losses, improper pieces selection, failure to operate as designed, voltage and current fluctuations, fractured, overloading, shock failure, and contact damage. Moreover, some of the failure modes of passive subcomponent like electrolyte capacitors are: Non-amplification, improper pieces selection, failure to function as intended for any piece, voltage, and current fluctuations, breakage, electric current, improper assembly, inadequate support (structural), fractured, loosened, open-circuited, overloading, oxidized, shock failure, short-circuited, contact damage, swells, thinning, distortion, and vibration. Furthermore, the FTA is constructed by considering the results of the FMEA with three significant parts: Input filter, power amplifier, and output filter. The reliability curve of the power stage can be estimated in five years, which is consistent with the defined guarantee period. It is concluded that the B1 lifetime of the power stage is 2.4 years for the same shape parameter (assumed exponential distribution) and 4.7 years for different shape parameters (assumed Weibull distribution), which is closer to real experience. It is recommended to use Weibull distribution for reliability analysis rather than exponential distribution as it leads to more realistic results. Since the Weibull parameters are not usually available for all components or difficult to obtain by reliability tests, FMEA is recommended to distinguish the high-risk components and consequently to find their Weibull parameters for reliability analysis.

Author Contributions: The main idea for the paper was proposed by S.R. S.R. wrote the first draft of the paper, except Section 2, which was drafted by S.B. S.R. and S.B. developed the methodology. S.R. and S.B. post-processed the results. A.S.B., J.D.S., and F.B., supervised the findings of this work and reviewed methodology. All authors contributed for articulating the research work in its current form as a full research manuscript.

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