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Huang, Liang; Wu, Chao; Zhou, Dao; Chen, Liang; Pagnani, Daniela; Blaabjerg, Frede

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Tran The Hoang,
University of Auckland, New Zealand

*CORRESPONDENCE
Liang Huang,
✉ lihu@energy.aau.dk

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Challenges and potential solutions of grid-forming converters applied to wind power generation system—An overview

Liang Huang^{1*}, Chao Wu², Dao Zhou¹, Liang Chen¹,
Daniela Pagnani^{1,3} and Frede Blaabjerg¹

¹AAU Energy, Aalborg University, Aalborg, Denmark, ²Department of Electrical Engineering, Shanghai Jiaotong University, Shanghai, China, ³Electrical System Design and Grid Integration, Ørsted, Copenhagen, Denmark

As the capacity of wind power generation increases, grid-forming (GFM) wind turbine generators are deemed as promising solutions to support the system frequency for future low inertia power grids. So far, the GFM converter with a nearly ideal dc voltage source has been studied thoroughly. However, when the GFM converter is applied to wind power applications, there are some realistic problems and challenges, such as coordinating wind turbine control and GFM control, limited energy to support the grid, variable wind speed, etc. These problems still need more discussion. In this paper, an overview of challenges and potential solutions of GFM converters applied to wind power generation systems are provided, where different energy reserving schemes, GFM control schemes, and overcurrent protection schemes are compared and discussed. Finally, a few perspectives on future trends are shared according to the authors' knowledge.

KEYWORDS

wind power generation, back-to-back converters, grid-forming control, dc voltage control scheme, energy reserving scheme, overcurrent protection scheme

1 Introduction

In the past decades, due to the foreseen exhaustion of conventional fossil-based energies and their climate impact, many global efforts have been devoted to developing renewable energy sources (Blaabjerg et al., 2017). Among different energy sources, wind power grows rapidly due to its high energy density and easy obtainment (Brown, 2015). For example, wind power has already provided 50% of the total electricity consumption in Denmark (Hvelplund et al., 2017). Besides, the output characteristics of the wind generators (e.g., dynamic responses and steady-state error of output voltages and currents, terminal impedance/admittance characteristics, and power quality) highly depend on the control scheme of converters (Peyghami et al., 2019), (Van et al., 2021). Thus, the control scheme of wind generators will play an important role in the future power system (Rocabert et al., 2012; Olivares et al., 2014; Fraile, 2021).

Currently, the grid-following (GFL) control scheme with the phase-locked loop (PLL) has been widely used in the wind power generation system. However, as the penetration of wind energy increases, the system inertia and the grid strength will reduce dramatically. Thus, conventional GFL converters may suffer from frequency and voltage instability problems (UK National Grid, 2017). Although some improved GFL control methods, e.g., tuning PLL bandwidth (Wen et al., 2016), H-infinity tuning method (Egea-Alvarez et al., 2015), and impedance reshaping methods (Alawasa et al., 2014; Fang et al., 2018; Huang et al., 2022a), can enhance the voltage stability, the frequency stability issue is still hard to deal with. Besides, the

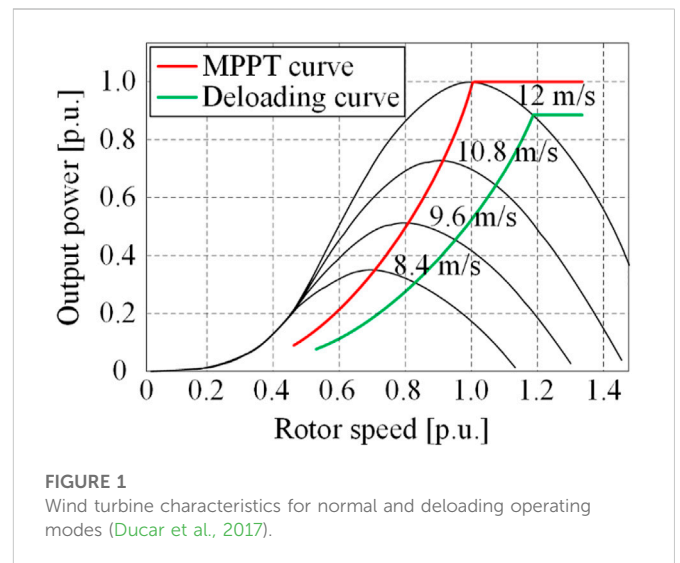
island operation is a big challenge for GFL converters since they rely on the externally generated voltage. With the GFL control, the converters will shut down when there is a large disturbance or outage on the grid and wait for a signal that the disturbance has settled before restart.

To address the above issues, a new concept called “grid-forming” (GFM) converter has been proposed in recent years. Different from GFL converters, GFM converters can operate in the island case and provide frequency support to the grid, so they attract lots of research attention (Denis et al., 2017; Matevosyan et al., 2019; Wang et al., 2020a; Lasseter et al., 2020; Lin, 2020; Ndreko et al., 2020; Rosso et al., 2021; Li et al., 2022). So far, various GFM control schemes, such as droop control (Brabandere et al., 2007), (Guerrero et al., 2005), and virtual synchronous generator (VSG) control (Beck and Hesse, 2007; D’Arco and Suul, 2013; Bevrani et al., 2014; Liu et al., 2016), have been proposed in existing literature (Brabandere et al., 2007; Guerrero et al., 2005; Beck and Hesse, 2007; D’Arco and Suul, 2013; Bevrani et al., 2014; Liu et al., 2016; Zhong and Weiss, 2011; Zhang et al., 2010; Zhang et al., 2016; Groß et al., 2019). Besides, some improved control schemes, such as virtual impedance (He and Li, 2011; Rodriguez et al., 2013; Vasquez et al., 2013), tuning inertia and damping (Alipoor et al., 2015), are also developed to enhance the small-signal stability and transient stability of GFM converters (He and Li, 2011; Rodriguez et al., 2013; Vasquez et al., 2013; Alipoor et al., 2015; Wang et al., 2020b; Du et al., 2020; Liao et al., 2020; Wu and Wang, 2020; Huang et al., 2021a; Arasteh et al., 2022; Huang et al., 2022c). Moreover, the single-loop and multiple-loop GFM controls are two widely used schemes (Du et al., 2020). The single-loop scheme is relatively simple, but it relies on the passive L-C filters to filter out the harmonics. When the L-C filter is small, its filter performance is limited. Differently, the multiple-loop scheme has an equivalent active resistance introduced by the inner current control loop, which is beneficial to reduce the harmonics and improve the power quality of the GFM inverters.

When the GFM control technology is applied to wind power generation systems, the energy reserving scheme, the dc-link voltage control scheme, and the cooperative control of the machine-side and grid-side should be taken into account. For the type-3 wind generators, the dc-link voltage is usually controlled by the grid-side converter (GSC), so that the GFM control can be performed on the rotor-side converter (RSC). Differently, for the type-4 wind generators, the dc-link voltage can be controlled by either the GSC or the machine-side converter (MSC) (Huang et al., 2021b). Moreover, if there is an additional battery energy storage system (BESS) on the dc-link, the dc-link voltage is able to be controlled by the BESS (Fang et al., 2019). Thus, different dc-link voltage control methods are worth being compared (Nguyen et al., 2022). Besides, to provide frequency support to the grid, the wind generator should reserve some additional energy, so that the deloading operation of the generator may be necessary (Kumar et al., 2020). In this paper, several energy reserving schemes, dc-link voltage control schemes, and overcurrent protection schemes for wind generators are reviewed, where type-3 and type-4 wind generators are the study focus.

Overall, the main contribution of this paper can be summarized as follows:

- 1) A comprehensive review and comparison among different GFM control schemes for type-3 and type-4 wind generators are presented in this paper, which provides a good reference for scholars and engineers in the wind power generation field.



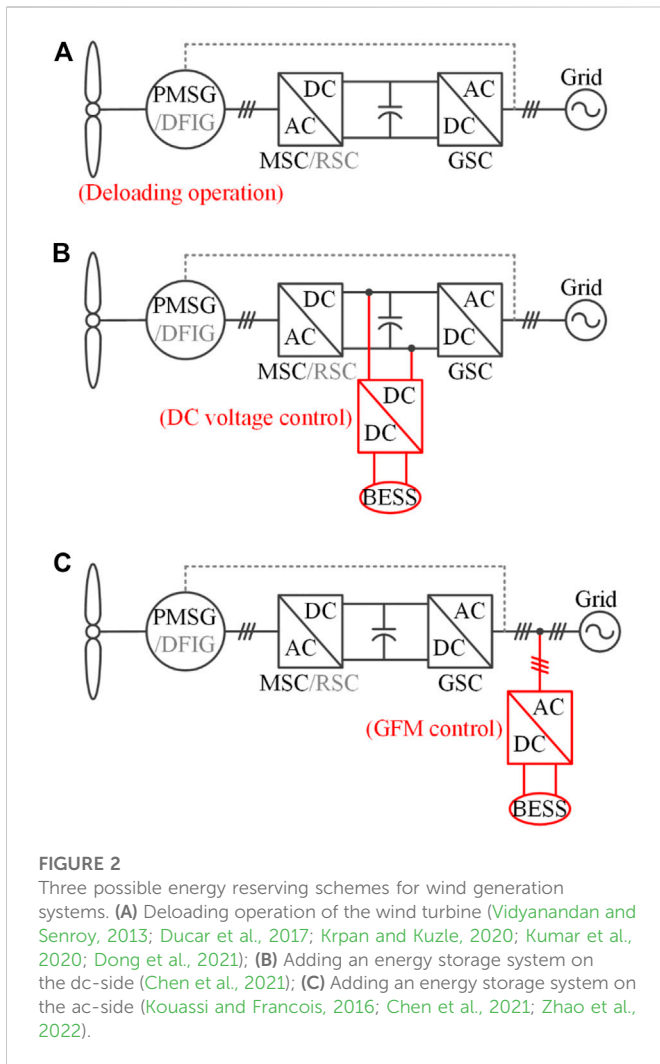
- 2) In this paper, the authors not only review different energy reserving schemes, GFM control schemes, and overcurrent protection schemes, but also share personal perspectives about the potential solutions according to the authors’ research experience.
- 3) The main challenges of applying GFM control technology to wind turbine applications are summarized, and several possible future research directions are proposed in this paper.

The rest of this paper is organized as follows: Firstly, in order to meet the basic requirement of having backup energy, three energy reserving schemes for wind generators are discussed in Section 2. Then, from the control perspective, several possible GFM control schemes of wind generators are compared in Section 3, where type-3 and type-4 wind generators are included. In Section 4, different overcurrent protection strategies used for abnormal grid conditions are discussed. In Section 5, a few perspectives on current challenges and future trends are summarized. Finally, this paper is concluded in Section 6.

2 Energy reserving schemes of wind generators

First of all, having backup energy is a basic requirement for GFM-based wind generators. So, several energy reserving schemes are discussed in this section. For the typical wind generation system without BESS, some wind energy (e.g., 10%–20%) should be reserved, so that this backup energy can be used to support the grid frequency when the load increases. In this case, the generator does not follow the maximum power point tracking (MPPT) curve anymore. Instead, the generator follows a new deloading curve that is lower than the MPPT curve, as shown in Figure 1.

Moreover, if there is an additional BESS to store the energy, the deloading operation is not necessary. The generator can follow the MPPT curve to generate the maximum power, because the wind energy can be stored in the BESS. Under this circumstance, the backup energy in the BESS can be used to support the grid frequency when the load increases.



Based on the above analysis, three possible energy reserving schemes are shown in Figure 2, which are suitable for either type-3 or type-4 wind generators. As shown in Figure 2A, if there is no additional BESS in the wind generator, the wind turbine (WT) needs to operate in the deloading mode to reserve some wind energy (Vidyanandan and Senroy, 2013; Ducar et al., 2017; Krpan and Kuzle, 2020; Kumar et al., 2020; Dong et al., 2021). This is a possible way for the wind generator to achieve the GFM function, but it is not the best way from an economic point of view, because some potential wind energy is wasted. Alternatively, if an additional BESS is added to the wind generator, the deloading operation is not necessary. Namely, the wind generator can still operate in MPPT mode. The BESS can be added on either the dc-side or the ac-side. As shown in Figure 2B, when the BESS is added on the dc-side, the GSC can be controlled as a GFM converter (Chen et al., 2021). Meanwhile, the MPPT control can be performed on the machine-side. However, the energy support ability of this scheme may be limited by the capacity of the battery. Besides, the lifetime of the battery and the maintenance cost also need to be considered, especially for the offshore wind farm. Moreover, as shown in Figure 2C, when the BESS is added on the ac-side, the BESS can be controlled as a GFM converter (Kouassi and Francois, 2016; Chen et al., 2021; Zhao et al., 2022). Relatively, there are fewer physical restrictions for this scheme

because the BESS can be placed far from the wind generators. Besides, the existing wind generators with GFL control can still be used without any modification. Therefore, this scheme is easier to be implemented compared with the previous two schemes. However, the island operation or black start of the GFL-based wind generator is a challenge. A possible way is to make use of the BESS for black start (Pagnani et al., 2022). Namely, during the black-out, the BESS with GFM control in Figure 2C is used to establish the local grid voltage. After the local grid voltage is established, the GFL-based wind generators can restart for normal operation. However, this solution requires a large capacity of the BESS. In addition, another possible way is a combination of the schemes in Figures 2A, C. For example, the scheme in Figure 2C can be used for the normal grid-connected condition, while the scheme in Figure 2A can be used for the islanded condition.

3 Grid-forming control schemes of wind generators

When the basic requirement of having the energy backup is satisfied, the specific GFM control scheme will be the key point to achieve GFM function on wind generators. Nowadays, type-3 and type-4 wind generators have been widely used in the wind generation field (Kushwaha and Singh, 2013). The type-4 wind generator is usually equipped with a permanent-magnet synchronous generator (PMSG) and a full-scale power converter. Although other types of generators, such as squirrel-cage induction generator (SCIG) and wound-rotor synchronous generator (WRSG), can also be used for the type-4 wind generation system, the PMSG-based wind generator is more popular (Nguyen et al., 2022). So, the PMSG-based type-4 wind generator is chosen as an example for analysis in this paper. Moreover, the type-3 wind generator is equipped with a doubly-fed induction generator (DFIG) and a partial-scale power converter. Since a partial-scale (e.g., 33%) power converter is much cheaper than a full-scale power converter, the cost of the type-3 wind generator is usually lower than that of the type-4. However, the gearbox is necessary for the type-3 wind generator, which may increase the maintenance cost. Differently, the type-4 wind generator with a direct-driver PMSG can eliminate the gearbox. Besides, since the PMSG does not need additional exciting current, the efficiency of the PMSG is generally higher than that of the DFIG. Therefore, either type-3 or type-4 wind generators have their own advantages and limitations. This section will review and compare different GFM control schemes for type-3 and type-4 wind generators.

3.1 Generalized GFM control structure

Although there are many alternative control schemes to achieve the GFM function, they follow the same power-synchronization control (PSC) law as the traditional synchronous generator (SG). Thus, a generalized GFM control structure is summarized in (Rosso et al., 2021) to highlight its main features. As shown in Figure 3, the generalized GFM control structure consists of inner voltage/current control loops and outer power control loops, where the active power is related to the phase angle and the reactive power is related to the voltage magnitude. Besides, a voltage reference $E\angle\theta$ is generated by the active power and reactive power controller at the outer loop, which can

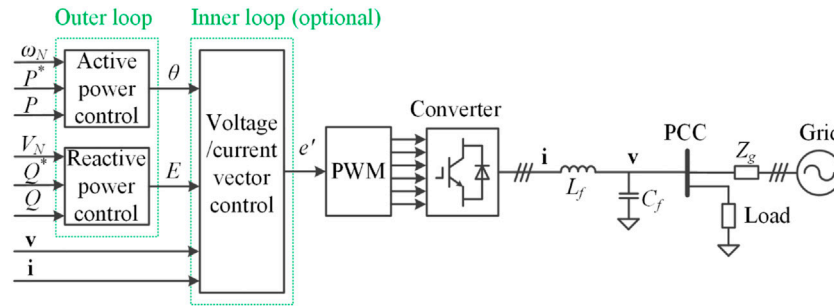


FIGURE 3
Generalized control structure of a GFM converter (Rosso et al., 2021).

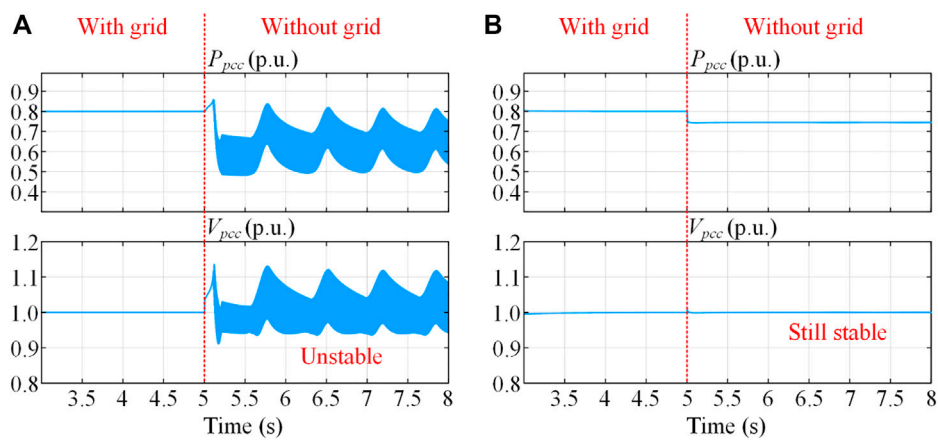


FIGURE 4
Simulation results of a grid-connected converter with different control schemes. (A) With grid-following control; (B) With grid-forming control.

be achieved by the droop control, VSG control, proportional-integral (PI)-based synchronous power control, virtual oscillator control, etc. Notably, the droop or VSG control has a steady-state error, while the PI-base control is able to eliminate the steady-state error. In addition, it is worth mentioning that this control scheme may not be suitable for low-voltage applications with a higher ratio of resistance and inductance. However, this paper mainly focuses on high-voltage applications rather than low-voltage applications.

Moreover, the inner voltage and current controllers in Figure 3 are optional. When the inner control loop is eliminated, the modulation voltage e' is the same as $E\angle\theta$. However, when the inner control loop is included, the output voltage v tracks the voltage reference $E\angle\theta$. Thus, the modulation voltage e' can be generated automatically based on the closed-loop control. Generally, including the inner control loops may increase the control complexity, but it provides additional benefits, such as accurate current control, flexible virtual impedance implementation, and improved filter performance. Besides, including the inner control loops is also beneficial for applying the current limitation to protect the converter against grid faults, which will be discussed in Section 4.

In order to demonstrate the advantages of the GFM converter over the GFL converter, simulation results of a grid-connected converter

with the typical GFL control and GFM control are shown in Figure 4. Initially, when the converter is connected to the grid, both the GFL and GFM converters work well. However, when the grid is disconnected at the instant of 5 s, the GFL converter becomes unstable, while the GFM converter is still stable. Therefore, the GFM control is very important for the stable operation of converter-interfaced generators.

3.2 GFM control schemes of type-4 wind generators

For the back-to-back converter in type-4 wind generators, the dc-link voltage can be controlled by either the GSC or the MSC. Besides, if there is an additional BESS on the dc-link, the dc-link voltage is able to be controlled by the BESS. Therefore, three categories of dc-link voltage control schemes are shown in Figures 5–7, respectively.

The grid-side dc-link voltage control scheme has been introduced in (Li et al., 2017; Xi et al., 2017; He et al., 2018; Sang et al., 2019; Li et al., 2021), which is shown in Figure 5. The control scheme of the MSC is basically the same as the conventional power control method. However, the control scheme of the GSC is different from the conventional dc-link voltage control scheme based on the PLL.

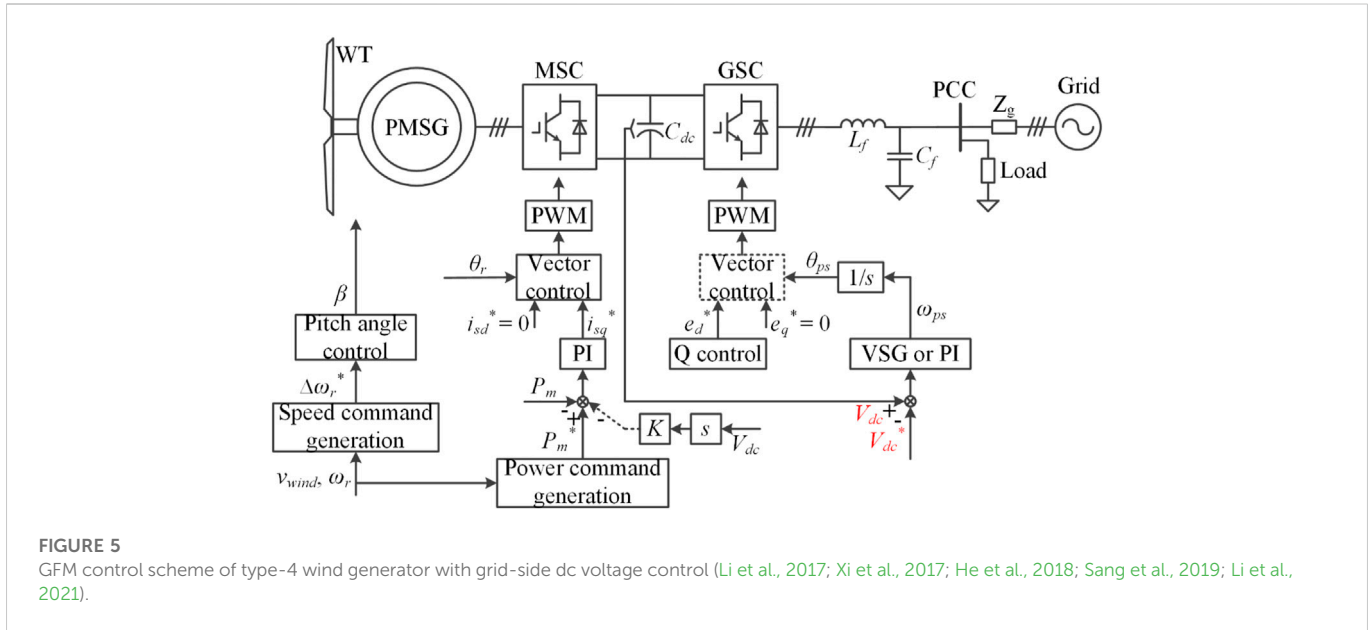


FIGURE 5 GFM control scheme of type-4 wind generator with grid-side dc voltage control (Li et al., 2017; Xi et al., 2017; He et al., 2018; Sang et al., 2019; Li et al., 2021).

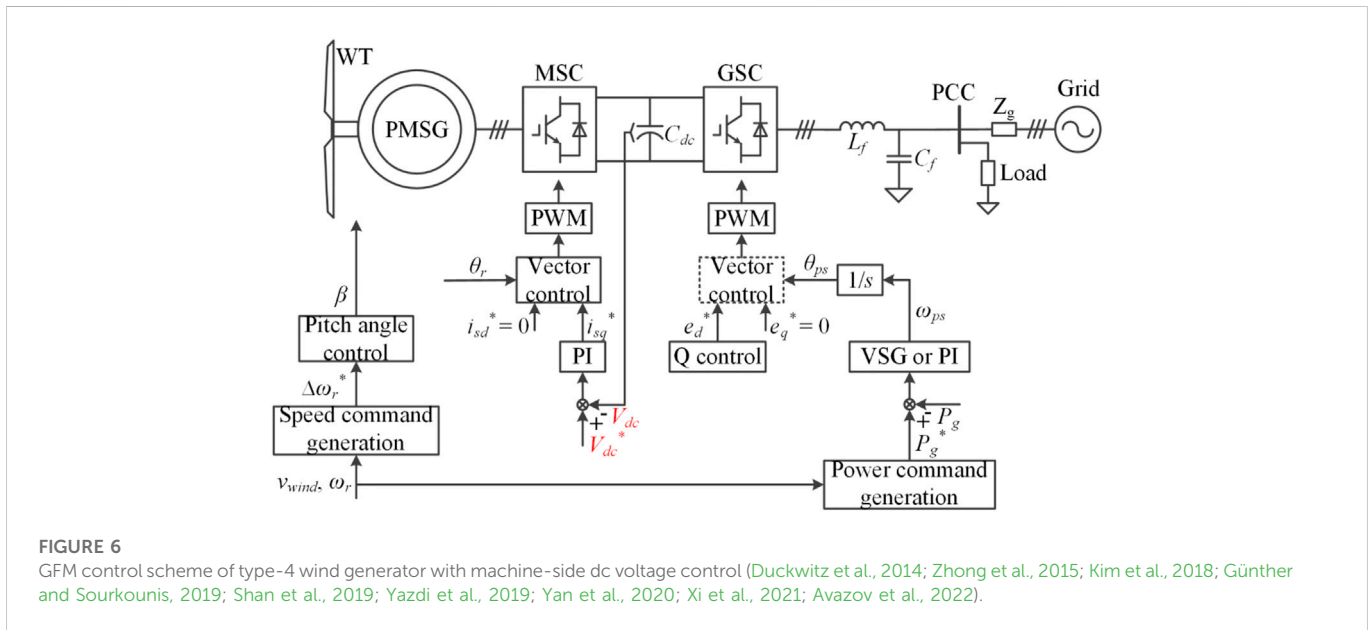


FIGURE 6 GFM control scheme of type-4 wind generator with machine-side dc voltage control (Duckwitz et al., 2014; Zhong et al., 2015; Kim et al., 2018; Günther and Sourkounis, 2019; Shan et al., 2019; Yazdi et al., 2019; Yan et al., 2020; Xi et al., 2021; Avazov et al., 2022).

Specifically, the dc-link voltage can be controlled by adjusting the output power by changing the phase angle of the output voltage reference. Besides, the magnitude of the output voltage reference is generated by a reactive power controller. Thus, alternative ways, such as droop control, VSG control, and PI control, can be used to control the dc-link voltage. Notably, when the VSG control is used, a steady-state error exists, so that the dc-link voltage cannot be controlled as same as the reference value. Differently, when the PI control is used, there is no steady-state error, so the dc-link voltage can be controlled as same as the reference value. Moreover, the inner loop of the voltage and current vector control is optional. In (Xi et al., 2017; He et al., 2018; Sang et al., 2019; Li et al., 2021), the inner loop is not included, while the inner loop is included in (Li et al., 2017). In addition, for the machine-side control scheme, a feedforward term from the dc-link

voltage to the power reference can be added. Thus, the MSC can provide some transient energy to support the dc-link voltage (Sang et al., 2019).

The main advantage of the grid-side dc-link voltage control scheme is that the typical machine-side control scheme can be inherited, which is a proven and mature method (Nguyen et al., 2022). However, the island operation is a challenge for this method because the dc-link voltage control relies on the grid voltage.

The machine-side dc-link voltage control scheme has been introduced in (Duckwitz et al., 2014; Zhong et al., 2015; Kim et al., 2018; Günther and Sourkounis, 2019; Shan et al., 2019; Yazdi et al., 2019; Yan et al., 2020; Xi et al., 2021; Avazov et al., 2022), which is shown in Figure 6. The dc-link voltage is controlled by adjusting the machine-side input power by regulating the torque. Thus, the general

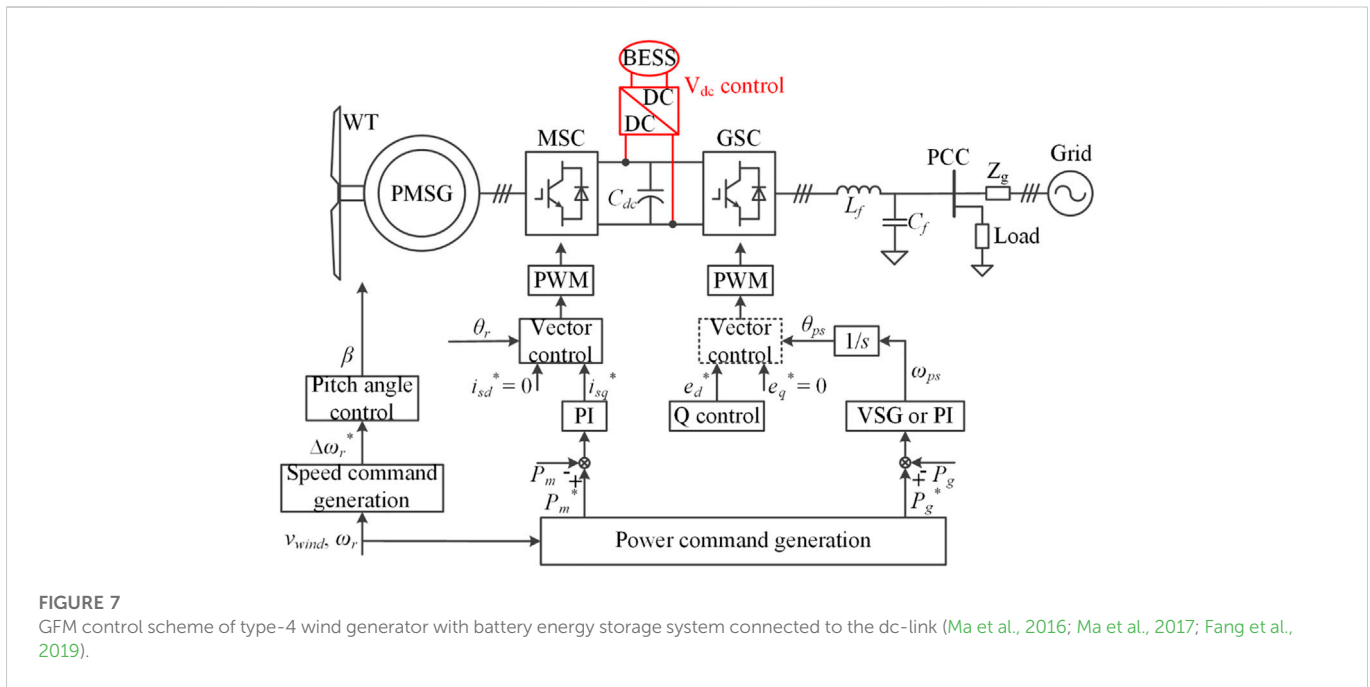


FIGURE 7
 GFM control scheme of type-4 wind generator with battery energy storage system connected to the dc-link (Ma et al., 2016; Ma et al., 2017; Fang et al., 2019).

GFM control scheme can be used for the GSC to achieve the GFM function, where the VSG or PI control is chosen as an example in Figure 6. Since the power is not controlled by the MSC, the power reference is sent to the GSC rather than the MSC for power control. Besides, the inner loop of the voltage and current vector control is optional. In (Duckwitz et al., 2014; Zhong et al., 2015; Kim et al., 2018; Günther and Sourkounis, 2019; Shan et al., 2019; Xi et al., 2021; Avazov et al., 2022), the inner loop is not included, while the inner loop is included in (Yazdi et al., 2019)- (Yan et al., 2020).

The main advantage of the machine-side dc-link voltage control scheme is that the dc-link voltage is provided by the MSC, which does not rely on the grid voltage anymore. Thus, the island operation or black start of the wind generator can be easily achieved (Shan et al., 2019), (Kim et al., 2018). Besides, the overall behavior of the PMSG plus the MSC is like a dc voltage source rather than a dc current source (Huang et al., 2021b), which is beneficial for the GSC to provide energy support to the grid.

Moreover, as shown in Figure 7, if an additional BESS is connected to the dc-link of the back-to-back converter, the dc-link voltage can be controlled by the BESS (Ma et al., 2016; Ma et al., 2017; Fang et al., 2019). Obviously, this scheme needs additional hardware extension, but it provides another degree of freedom for control. Namely, the power control can be achieved on both the MSC and the GSC, which is beneficial for optimizing the power flow through the back-to-back converter and stabilizing the dc-link voltage. Besides, the conventional power control method on the MSC can be inherited, which is a mature method. Moreover, alternative GFM control schemes can be used for the GSC, where the VSG or PI control is chosen as an example shown in Figure 7.

From the technical point of view, the GFM control scheme with the BESS is better than the previous two methods in Figures 5, 6, because the typical machine-side control scheme can be inherited without any modification and the island operation can be easily achieved by using the BESS. However, there are some obvious drawbacks for this scheme. Firstly, adding the BESS increases the cost of the wind generation system. Secondly, the installation of the battery needs more physical space, which

may be a problem if the space is limited in the nacelle of wind generators. Thirdly, the lifetime of the battery is usually not so long as that of the power electronic devices, which may increase the additional maintenance cost. Therefore, from the practical application perspective, the GFM control scheme shown in Figure 7 may not be a highly competitive scheme for type-4 wind generators.

In order to compare advantages and disadvantages of GFM type-4 wind generators with grid-side dc voltage control and machine-side dc voltage control, simulation results of GFM type-4 wind generators are presented in Figure 8. As shown in Figure 8A, with the grid-side dc voltage control, the dc-link voltage cannot be controlled to be a constant when the grid is disconnected, because the input power (depending on the wind speed) and the output power (determined by the load in island cases) are not equal anymore. Thus, the dc-link voltage will continue to increase or decrease. Finally, the wind generation system will become unstable. Differently, as shown in Figure 8B, with the machine-side dc voltage control, the dc-link voltage can be controlled to be the rated value no matter whether the grid is connected or not. This is because the input power is always adjusted according to the dc-link voltage, which can keep the input power equal to the output power in the steady state.

Overall, the advantages and disadvantages of the aforementioned three dc-link voltage control schemes of type-4 wind generators are compared in Table 1. It can be seen from Table 1 that each method has its own advantages and limitations. Thus, further studies are necessary to address these limitations. From the authors' viewpoint, the machine-side dc-link voltage control scheme may have more potential, because the control of the wind generator does not rely on the grid.

3.3 GFM control schemes of type-3 wind generators

For the type-3 wind generators, the GFM function is usually achieved on the machine-side, while the dc-link voltage is often

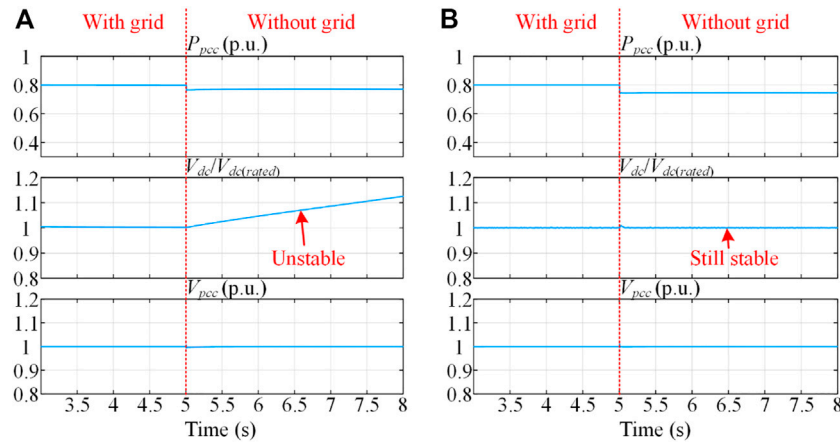


FIGURE 8 Simulation results of GFM type-4 wind generators with different dc-link voltage control schemes. **(A)** With grid-side dc voltage control; **(B)** With machine-side dc voltage control.

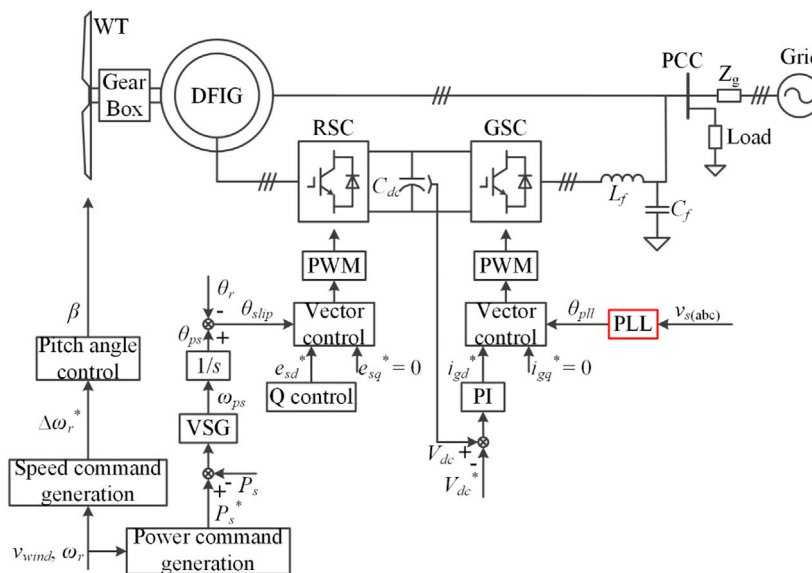


FIGURE 9 GFM control scheme of type-3 wind generator with PLL-based dc voltage control (Huang et al., 2017; Jiao and Nian, 2020; Shah and Gevorgian, 2020; Oraa et al., 2022).

TABLE 1 Comparison of three dc-link voltage control schemes of type-4 wind generators.

Schemes	Advantages	Disadvantages
Grid-side dc-link voltage control scheme Li et al. (2017); Xi et al. (2017); He et al. (2018); Sang et al. (2019); Li et al. (2021)	The conventional power control scheme of the MSC can still be used, which is a mature method.	The black start and island operation are challenges for this scheme.
Machine-side dc-link voltage control scheme (Duckwitz et al. (2014); Zhong et al. (2015); Kim et al. (2018); Günther and Sourkounis, (2019); Shan et al. (2019); Yazdi et al. (2019); Yan et al. (2020); Xi et al. (2021); Avazov et al. (2022)	The control of the wind generator does not rely on the grid, so the island operation is easy to achieve.	The control scheme of the MSC needs to be redesigned.
External dc voltage control scheme with BESS Ma et al. (2016); Ma et al. (2017); Fang et al. (2019)	The conventional power control scheme of the MSC can still be used. The island operation is easy to achieve.	This scheme needs additional hardware extension, which will increase the cost.

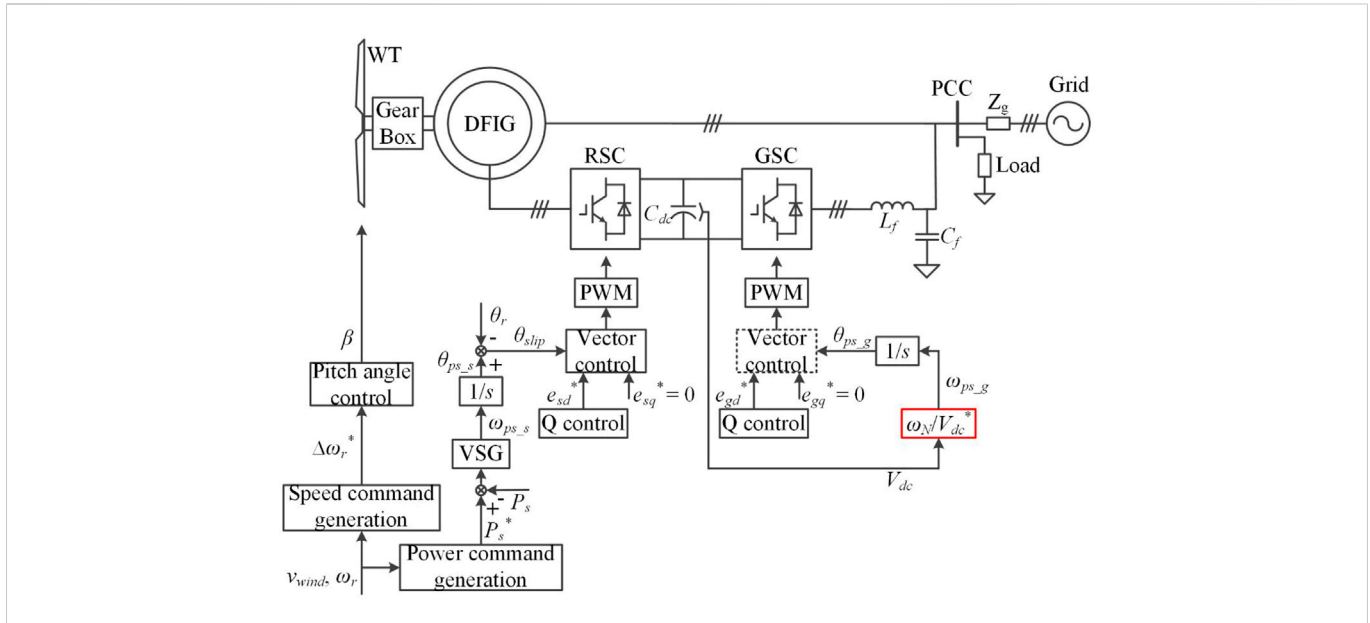


FIGURE 10
GFM control scheme of type-3 wind generator with PSC-based dc voltage control (Shao et al., 2019).

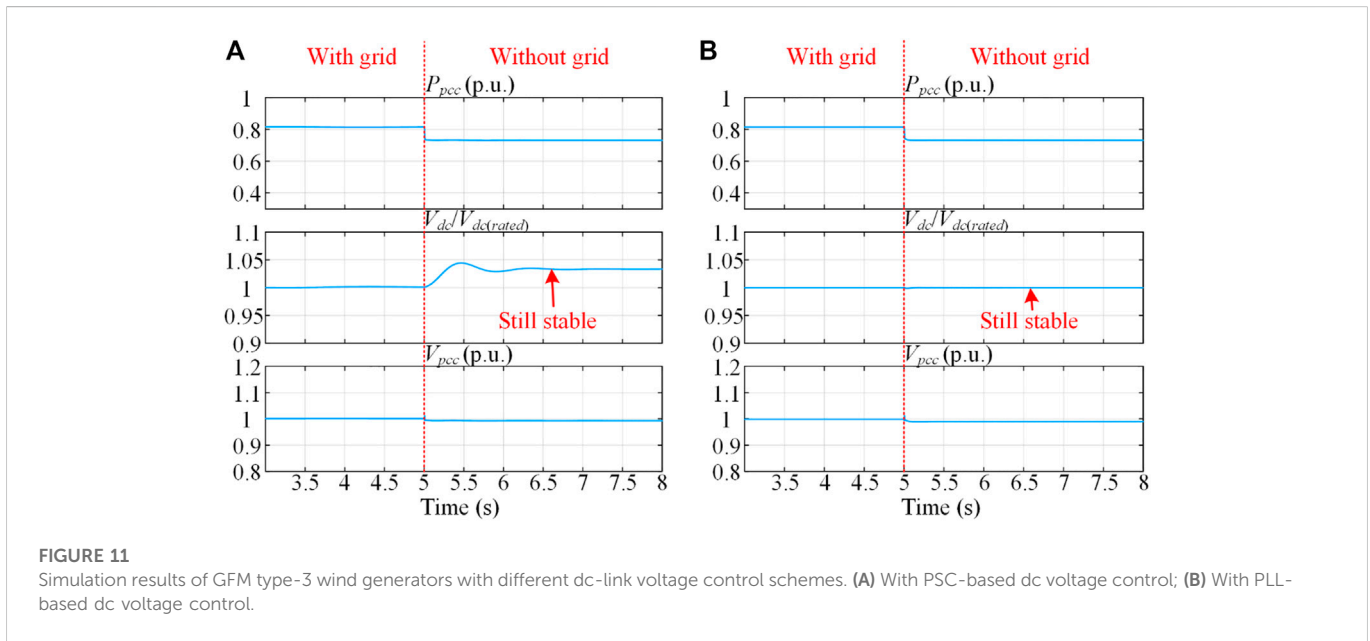


FIGURE 11
Simulation results of GFM type-3 wind generators with different dc-link voltage control schemes. (A) With PSC-based dc voltage control; (B) With PLL-based dc voltage control.

controlled by the GSC. In general, two types of control methods can be used for the GSC, which are the typical GFL control with a PLL and the PSC. However, no matter which method is used, the grid voltage is essential to establish the dc-link voltage, so the black start is a challenge for the type-3 wind generators. To achieve the black-start function, an additional auxiliary dc voltage source may be necessary. In this section, three possible dc-link voltage control schemes for type-3 wind generators are reviewed and discussed.

The GFM control scheme of type-3 wind generator with the PLL-based dc voltage control has been introduced in (Huang et al., 2017; Jiao and Nian, 2020; Shah and Gevorgian, 2020; Oraa et al., 2022), which is shown in Figure 9. The general GFM control scheme in Figure 3 can be used for the RSC to achieve the GFM function, while the conventional GFL control

method with a PLL is used for the GSC to control the dc-link voltage. The main advantage of this scheme is that the typical GFL control method on the GSC is a mature method (Oraa et al., 2022), (Shah and Gevorgian, 2020).

Moreover, the GFM control scheme of type-3 wind generator with the PSC-based dc voltage control has been introduced in (Shao et al., 2019), which is shown in Figure 10. The general GFM control scheme in Figure 3 can be used for the RSC, while the power synchronization (or called “inertial synchronization”) control is used for the GSC to control the dc-link voltage. Thus, both the RSC and the GSC have the GFM functions. In order to compare advantages and disadvantages of GFM type-3 wind generators with PLL-based dc voltage control and PSC-based dc voltage control, simulation results of GFM type-3 wind generators are presented in Figure 11.

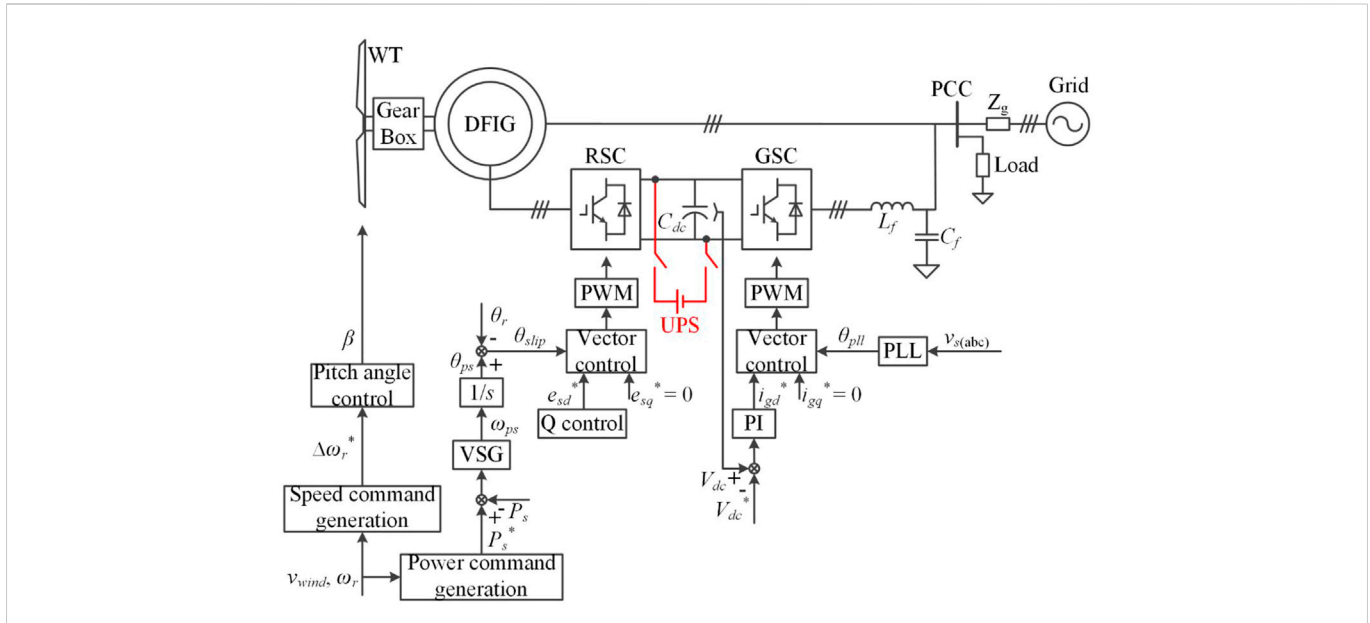


FIGURE 12 GFM control scheme of type-3 wind generator with an auxiliary UPS on the dc-link (Zhu et al., 2018), (Rodríguez-Amenedo et al., 2021).

As shown in Figure 11, GFM type-3 wind generators with PSC-based or PLL-based dc-link voltage control schemes can operate stably after the grid is disconnected, but the dynamic and steady-state characteristics of these two methods are different. It can be seen from Figure 11A that the dc voltage dynamic response by using PSC-based dc voltage control is relatively slow, and the steady-state dc voltage is not equal to the rated value. Differently, it can be seen from Figure 11B that the dc voltage dynamic response by using PLL-based dc voltage control is relatively fast, and the steady-state dc voltage can be controlled as same as the rated value. Therefore, from the authors' viewpoint, the PLL-based dc voltage control scheme may have more potential.

Although type-3 wind generators with the above two GFM control schemes can operate in the island case, the black start is still a big challenge. To achieve the black start, another scheme with an auxiliary uninterrupted power supply (UPS) on the dc-link has been proposed in (Zhu et al., 2018) and (Rodríguez-Amenedo et al., 2021), as shown in Figure 12. The overall control scheme of this method is basically the same as the control scheme in Figure 9. However, since an auxiliary UPS is added to the dc-link, the wind generator has the black start capability. Namely, the UPS is connected to the dc-link during the start-up process to energize the dc bus. Thus, the RSC operates initially to establish the stator-side voltage. Then, the GSC can be used to control the dc-link voltage. After the start-up process is finished, the UPS is disconnected. Obviously, having the black start capability is a major advantage of this scheme. However, since the additional auxiliary UPS is added, the cost of this scheme is higher than the previous two schemes without the UPS. Besides, additional maintenance cost for the UPS is also inevitable.

Overall, the advantages and disadvantages of the above three GFM control methods of type-3 wind generators are compared in Table 2. The RSC controls of these three methods are basically the same. However, the main difference is whether to have a PLL or an auxiliary UPS. Relatively, the PLL-based control scheme is a mature method. However, the PSC-based control scheme is a newly developed method,

which has not been widely used. So, this scheme still needs more exploration. Besides, the black start is a big challenge for the type-3 wind generator. Adding an auxiliary UPS or battery on the dc-link may be necessary to achieve the black start function.

4 Overcurrent protection schemes of GFM converters under abnormal grid conditions

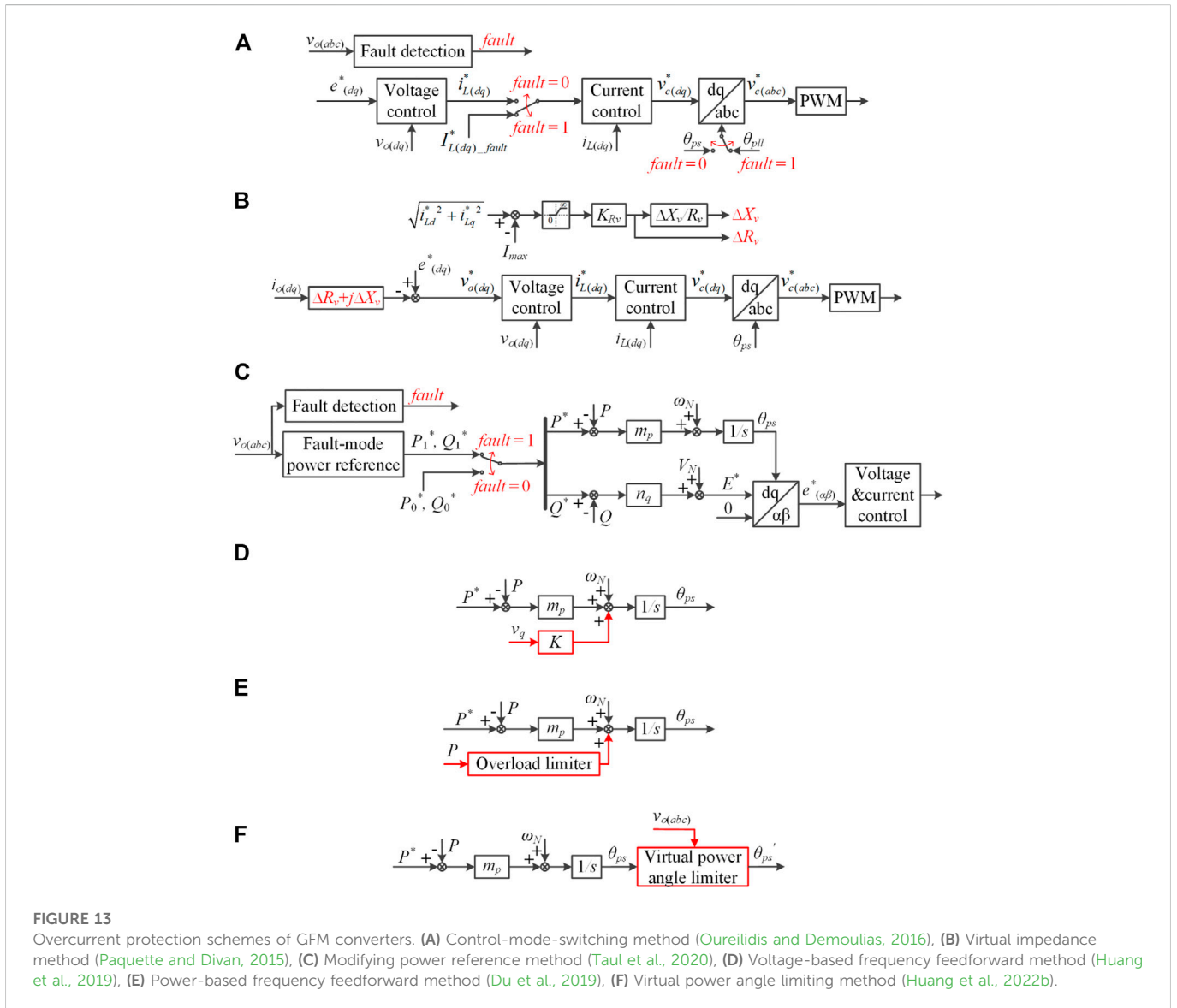
Although the aforementioned GFM control schemes can work under normal grid conditions, they still have some problems under abnormal grid conditions. Specifically, since power-electronics-based converters are only able to bear a few percent of overcurrent (typically 20%), the converters have the risk of overcurrent under grid fault or overload conditions, which may damage the power converters. In order to protect the GFM converters against extreme grid faults, such as short circuits, heavy load connection, and line-tripping/reclosing, additional overcurrent protection is necessary (Xin et al., 2016; Awal and Husain, 2021; Rokrok et al., 2022). In this section, several overcurrent protection schemes are discussed.

As shown in Figure 13, six overcurrent protection strategies are reviewed, which are the control-mode-switching method (Oureilidis and Demoulias, 2016), virtual impedance method (Paquette and Divan, 2015), modifying power reference method (Taul et al., 2020), voltage-based frequency feedforward method (Huang et al., 2019), power-based frequency feedforward method (Du et al., 2019), and virtual power angle limiting method (Huang et al., 2022b). The key performances of these overcurrent protection methods are compared in Table 3.

The control-mode-switching method is shown in Figure 13A. The idea of this method is to switch the control mode from the GFM mode to the GFL mode when the grid fault happens. When the fault is cleared, the control mode is switched back to the GFM mode. By using this method, the current can be limited to a designed fixed value

TABLE 2 Comparison of three dc-link voltage control schemes of type-3 wind generators.

Schemes	Advantages	Disadvantages
GFM control on RSC and PLL-based dc voltage control on GSC Huang et al. (2017); Jiao and Nian, (2020); Shah and Gevorgian, (2020); Oraa et al. (2022)	The conventional PLL-based dc voltage control scheme is a mature method. The dynamic characteristics of the dc-link voltage are relatively fast.	The PLL is still used on the GSC, which may cause some potential stability problems. Besides, the black start is a challenge.
GFM control on RSC and PSC-based dc voltage control on GSC Shao et al. (2019)	Not only the RSC has GFM functions, but also the GSC has the GFM functions, so the PLL is not necessary for this control scheme.	The dynamic characteristics of the dc voltage are slow, and there are steady-state errors on the dc voltage. Besides, black start is a challenge.
GFM control on RSC and adding an auxiliary UPS on the dc-link Zhu et al. (2018), Rodríguez-Amenedo et al. (2021)	This scheme has the black start capability due to the auxiliary UPS on the dc-link.	The cost of this scheme is higher than the conventional schemes because it needs hardware extension.



during the fault. However, grid fault detection is necessary for this method, which increases the complexity. Besides, during the recovery process, the wind-up issue of the integrator may worsen the transient performance.

The virtual impedance method is shown in Figure 13B. The idea of this method is adding a large virtual impedance between the converter and the grid, so that the output current can be limited. By using this

method, grid fault detection is not necessary. However, the performance of this method is sensitive to the grid impedance (Taul et al., 2020). Besides, the steady-state current cannot be limited to a designed fixed value during the fault, which varies under different grid conditions.

The modifying power reference method is shown in Figure 13C. The idea of this method is to reduce the power reference when a grid

TABLE 3 Comparison of different overcurrent protection schemes of GFM converters (Huang et al., 2022b).

Schemes	No need of grid fault detection	Smooth transient transition	Not sensitive to SCR	Effective in grid voltage sag case	Effective in frequency drop case
Control-mode-switching method Oureilidis and Demoulias, (2016)	✗	✗	✓	✓	✓
Virtual impedance method Paquette and Divan, (2015)	✓	✗	✗	✓	✓
Modifying power reference method Taul et al. (2020)	✗	✓	✓	✓	✗
Voltage-based frequency feedforward method Huang et al. (2019)	✓	✓	✓	✓	✗
Power-based frequency feedforward method Du et al. (2019)	✓	✓	✓	✗	✓
Virtual power angle limiting method Huang et al. (2022b)	✓	✓	✓	✓	✓

fault happens. This method is effective in the grid voltage sag case. However, it is not effective in the grid frequency drop case. Besides, grid fault detection is necessary for this method.

The voltage-based frequency feedforward method is shown in Figure 13D. This method makes use of the q-component voltage to add a frequency feedforward term to the P-f droop controller, which is effective in the grid voltage sag case. Besides, it is not necessary to switch the control structure by using this method. However, it is not effective in the grid frequency drop case.

The power-based frequency feedforward method is shown in Figure 13E. Based on the value of the active power, a frequency feedforward term is added to the P-f droop controller. This method is effective in the grid frequency drop case, but it is not effective in the grid voltage sag case.

The virtual power angle limiting method is shown in Figure 13F. A stable equilibrium point always exists in either grid voltage sag cases or grid frequency drop cases, so the stability of GFM converters under large grid disturbances can be guaranteed by using this method. Besides, it is not necessary to switch the control structure or parameter, and the additional grid fault detection is also not necessary. Therefore, from the authors' point of view, this method is a promising solution to protect GFM converters against overcurrent.

5 Future trends

Although some possible solutions for reserving the wind energy, controlling the dc-link voltage, and implementing overcurrent protection have been proposed so far, there are still some challenges and open issues regarding applying GFM control technology in the wind generators, which will be discussed briefly in this section.

5.1 Determining capacity of dc-link capacitor in type-4 wind generators

For the type-4 wind generators, the PMSG is connected to the grid through a back-to-back converter. Since the dynamic response of the

PMSG is generally slower than that of the converter, the dc-link capacitor plays the role of the energy buffer to provide short-term energy to the grid. Thus, the dc-link voltage is hard to be maintained constantly if the dc-link capacitor is not large enough. Therefore, to achieve the GFM function, the capacity of the dc-link capacitor needs to be increased (Lund et al., 2020). However, further evaluation is required to determine the appropriate size of the capacitor.

5.2 Reducing the mechanical stress on the turbine in type-3 and type-4 wind generators

It is reported in (Shah and Gevorgian, 2020) that the mechanical stress of type-3 wind generators with GFM control is higher than that of the conventional GFL control, due to a slower speed of the active power control. Similar phenomena are observed in type-4 wind generators with the machine-side dc-link voltage control. In (Avazov et al., 2022), the cause of this mechanical stress on the wind generator for type-4 is investigated and it is found that they appear in the form of torsional vibrations and their trigger may be a rapid variation of the electromagnetic torque, which in turn can be caused by grid frequency variations. The addition of damping in the system (internal and/or external) is one of the applied solutions for future work (Roscoe et al., 2019). Considering that higher mechanical stress may reduce the lifetime of the turbine, an improved control method to reduce the mechanical stress on the turbine is worth studying further.

5.3 Coordinating wind turbine control and GFM control

For the conventional GFL-based wind generators, the operation of the WT mainly depends on the wind speed (i.e., following the MPPT curve), which is relatively simple. Differently, for the GFM-based wind generators, both the wind speed and the power demand of the grid should be considered to modify the operating point of the WT (Ma et al., 2016), which becomes more complicated. Therefore, coordinating the WT control and the GFM control still needs more studies.

5.3 Seamless transition between GFL control mode and GFM control mode

Considering that a sufficient energy supply is essential for GFM converters, it is more reasonable for wind generators to operate in the GFM mode when the wind speed is high, while they run in the conventional GFL mode when the wind speed is low. Thus, the seamless transition between the GFL control mode and the GFM control mode is necessary (Tayyebi et al., 2020). Therefore, an effective method to switch between the GFL and GFM modes smoothly is worth being developed in the future.

5.4 Analyzing the impact of dc current limitation on GFM-based wind generators

So far, the impact of the ac current limitation on the GFM inverter has been studied a lot. In fact, the dc current limitation is also important for the back-to-back converter to make sure the converter operates within the rated current range (Tayyebi et al., 2020). It is questionable whether the GFM function can still be achieved when the dc current is limited, which needs further exploration.

5.5 Analyzing transient stability of GFM-based wind generators

Currently, although the small-signal stability of GFM-based converters/wind generators has been widely analyzed, the transient characteristics still need more studies, which belongs to a large-signal problem, including grid voltage dip, phase jump, etc (Pan et al., 2020; Chen et al., 2022; Huang et al., 2022c; Liu et al., 2022; Luo et al., 2023). However, it is very difficult to analyze the stability of a high-order (i.e., higher than second-order) nonlinear system. Hence, analyzing the transient stability of GFM-based converters/wind generators by using a reduced-order model is a possible way, which needs further investigation.

5.6 Optimizing the proportion of GFL-based and GFM-based wind generators

As known, conventional GFL-based wind generators can output the maximum power by following the MPPT curve. However, it is not possible to use 100% GFL-based generators in a power system. Differently, it is possible to use 100% GFM-based generators in a power system, but the output power of the GFM-based generators is not as high as that of the GFL-based generators because some energy should be reserved to support the grid. Hence, the power system with mixed GFL-based generators and GFM-based generators may have complementary benefits. Thus, optimizing the proportion of the GFL-based and the GFM-based wind generators is an interesting research topic.

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6 Conclusion

This paper provides an overview of possible solutions for applying the GFM control technology in the type-3 and type-4 wind generators. The main difference between a GFM-based wind generator and a GFM inverter is whether having a strong dc-link voltage source on the dc-side. Due to the fact that there is no dc voltage source in the wind generator, the dc-link voltage needs additional control, and the generated energy from the WT needs to be reserved. Therefore, several dc-link voltage control schemes and energy reserving schemes are discussed. Compared with the grid-side dc-link voltage control scheme, the machine-side dc-link voltage control scheme for type-4 wind generators may have more potential because it does not rely on the grid voltage. Compared with the PSC-based dc voltage control scheme, the PLL-based dc voltage control scheme for type-3 wind generators may have more potential because it has fast dynamic characteristics and zero steady-state error on the dc-link voltage. Besides, the deloading operation is an effective way to reserve wind energy for both type-3 and type-4 wind generators, but part of wind energy is wasted during deloading operation. Although adding an additional BESS may have more benefits, it may cause other problems, such as a higher cost, reliability issues of the battery, etc. Furthermore, when considering abnormal grid conditions with large voltage and frequency disturbances, an effective overcurrent protection scheme is necessary for GFM converters. A recently proposed virtual power angle limiting method does not have obvious drawbacks compared with other methods, which seems to be a promising solution. Finally, perspectives on future trends are shared according to the authors' knowledge.

Author contributions

Writing—original draft preparation, LH; writing—review and editing, CW, DZ, LC, DP, and FB. All authors have read and agreed to the published version of the manuscript.

Conflict of interest

DP was employed by the company Ørsted.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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