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Energy efficient aeration in a single low pressure Hollow Sheet Membrane Filtration Module T. R. Bentzen¹, N. Ratkovich¹, M. R. Rasmussen¹ and N. Heinen²

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Introduction & Objectives

- · Fouling is the main bottleneck of the widespread of MBR systems.
- Process hydrodynamics can decrease and/or control fouling.
- by adding air and having a 2-phase flow.
- Hollow Sheet (HS) MBR (Alfa Laval) (Fig. I)
- Operates with low TMP (~0.03 bar) across the entire membrane surface (MS). · Permeate is drained from entire MS.
- · Advantages of low TMP are:
- MS is less prone to fouling (longer service life)
- Activated sludge (AS) passing across MS does NOT accumulate/stick to MS.
- · AS flows upwards between the membrane sheets while permeate passes through the MS.
- To ensures that AS circulates properly:
 - Air bubbles are used to create a two-phase cross-flow velocity
 - Bubbles generate scouring effect to remove particles that are attached to MS.





Figure 6. Contour plot of CFD velocities between

filtration sheets at an air flow rate of 55 m³·h⁻¹.

Methodology

Velocity measurements

- Single filtration module which has 86 HS polyvinyl membranes (total MS of 154 m²) (Fig. 2).
- Experiments were conducted at the Danish Hydraulic Institute (DHI) (Fig. 3). Experimental velocity measurements were obtained from micro-propellers (MP) between
- two HS membranes (Fig. 4).
- Air is introduced in reactor through 7 perforated pipes with 7 holes (4 mm) in each pipe.
- Air flow rate in the experiment was 55 and 83 $m^3 \cdot h^{-1}$ and CFD model was 37, 55 and 83 m^{3.}h⁻¹.

CFD model (Fig. 5)

- Ansys CFX v13
- Mixture 2-phase model
- k- ϵ turbulence model





Figure 4. locations of the MP



Figure 5. Real and virtual representation MBR module.

20.003 5.6e-003 1.0e-003 1.8e-004 3.2e-005 64.00

Results and discussion

Velocity measurements

CFD velocity profiles for one HS membrane (Fig. 6).

Air flow rate	Experimental	CFD	Error
(m³·h ⁻¹)	(m⋅s⁻¹)	(m⋅s⁻¹)	(%)
37*	-	$\textbf{0.198} \pm \textbf{0.054}$	-
55	0.218 ± 0.051	$\textbf{0.242} \pm \textbf{0.065}$	10.9
83	$\textbf{0.309} \pm \textbf{0.067}$	$\textbf{0.292} \pm \textbf{0.072}$	5.7

- *Experimental measurements were not carried out at this air flow rate Air is well distributed within module and no pronounced dead zones
- were found (Fig. 7).
- A fairly good agreement between the experimental measurements and the CFD simulation regarding the magnitude of the velocity was achieved (error less than 11 %).
- CFD model enabled to provide insight on the velocity profiles and air distribution.

Wall shear stress

· It was inferred from CFD simulation that values of the shear stress were accurate (Fig. 8).

Air flow rate	CFD	
(m³·h ⁻¹)	(Pa)	
37	0.196 ± 0.02	
55	0.384 ± 0.02	
83	0.464 ± 0.03	

· Shear stresses on MS are evenly distributed.

Figure 8. Shear stress profiles for the HS system for an air flow rate of 37 $m^{3} \cdot h^{-1}$. Above diffuser holes (left) and between diffuser holes (right).

Conclusions

- A proper validation of the CFD model was made in terms of velocity measurements using MP with water.
- Wall shear stress was inferred from CFD simulations.
- An error less than 11 % was found between experimental measurements and CFD simulations in terms of velocity profiles.
- Shear stress is homogeneously distributes over the HS MS
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Figure 7. Air volume fraction and velocity vectors for a HS

membrane filtration module