

-The Wave Star- Power Take-Off System Modelling



The Wave Energy Research Group WERG is situated at the Department of Civil Engineering, Aalborg University. It originates from the Hydraulics and Coastal Engineering Laboratory, which presents extensive experience within the field.

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Figure 1:

View of the Nissum Bredning plant in Storm protection mode. Platform support through pier. 20/20 sym. floater config. Rated 5.5 kW. Onboard DSP, Hydraulic and Control Rooms. 19000 hours operative, 15 storms without damage.

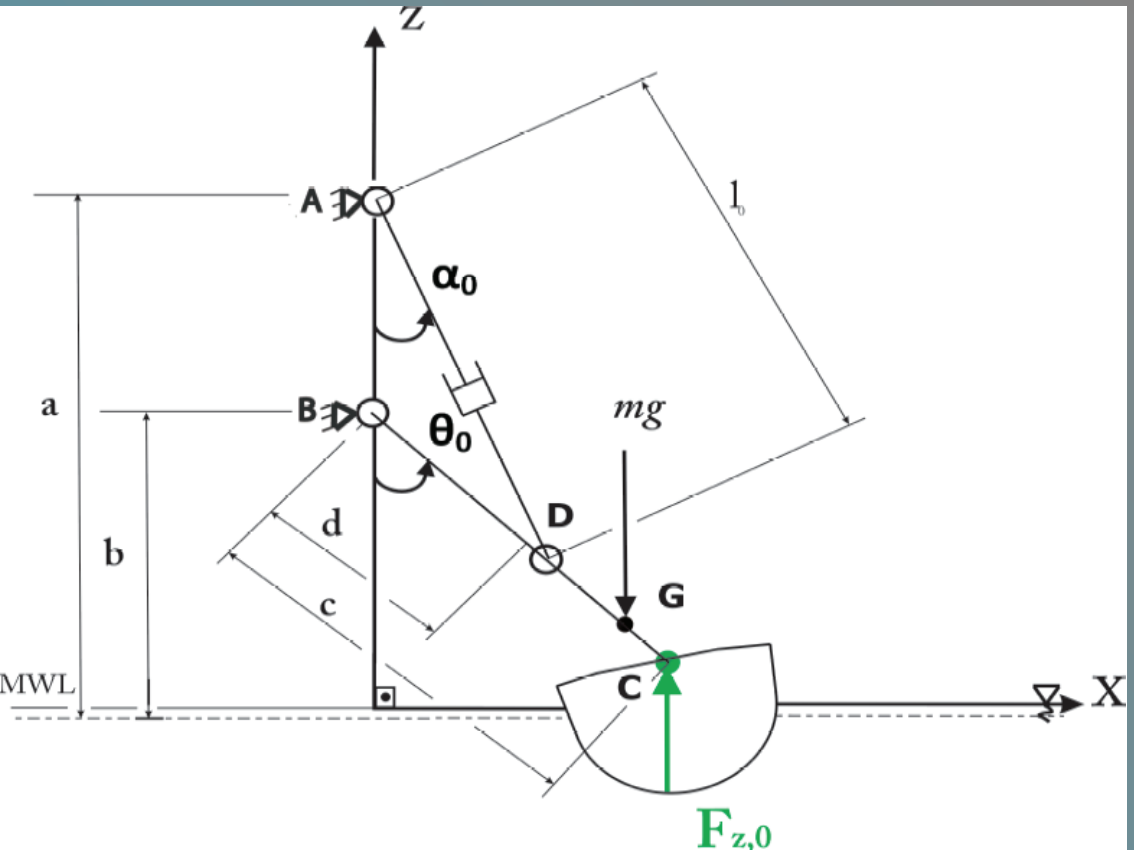


Figure 2:

Single Floater plane cut view through Mean Water Level. System control force $f_c = 0$. Upward applying Hydrodynamic wave force $F_{z,0}$ induces a Moment around bearing B. Result: Floater & piston excursion ($f_{z,u} > 0$ for Energy extraction).

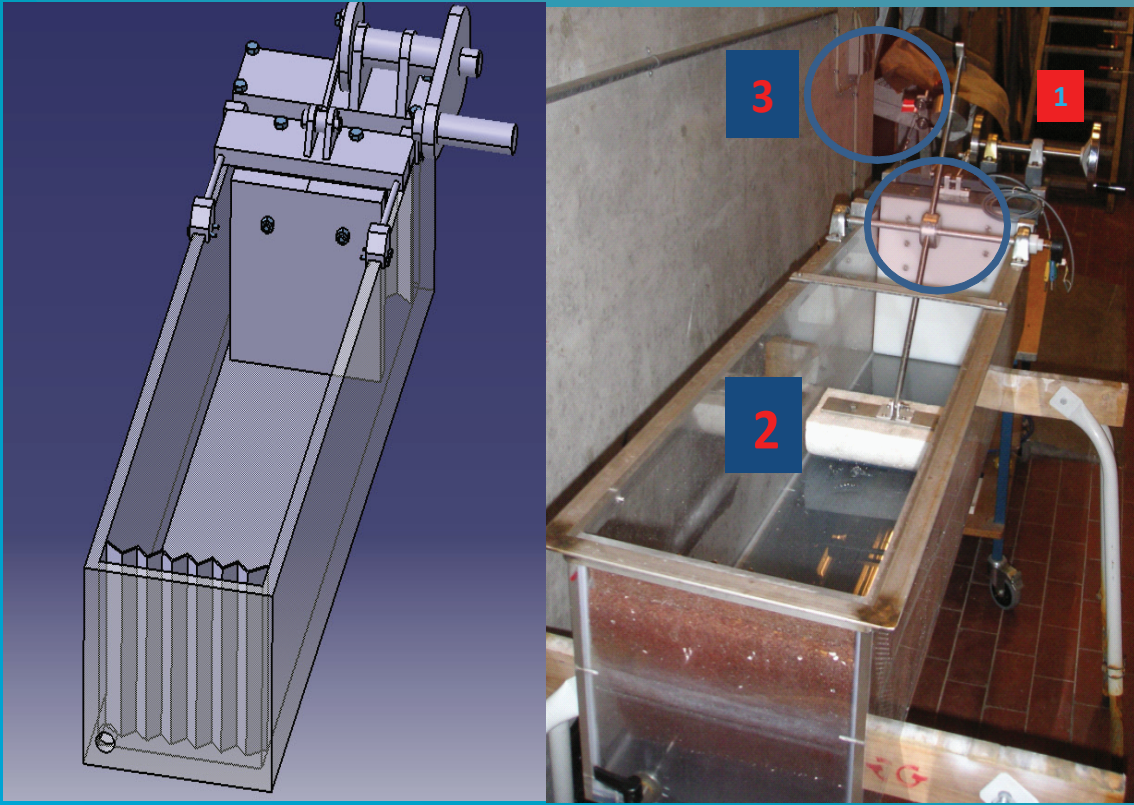


Figure 3:

Left: CAD model of a paddled Wave generator. Right: AAU's Basic lab prototype (250x300x1045mm) - Below, a semicil. float (140x300). Above, Magnetic Reelight "PTO" on strut. Experiments carried on a DC-motored unit (Scale 1:50).

Wave Energy is an arising renewable energy form. The Wave Star Energy A/S device has shown remarkable efforts through various testing in the department laboratories of AAU at 1:40 scale during 2000-2008. Furthermore, it has been tested and grid connected via hydraulic Power Take-Off on a 1:10 scale at the Helligsø pier in the Nissum Bredning fjord since 2006 until now. Further ongoing projects for the 1:2 scale in Denmark are being developed.

This thesis initially focuses on the Hydrodynamic modeling and the Control System study of the WSE Power Take-Off (PTO). It is completed through the experimental testing of a single floaters motion with an electromechanical drive.

Formulation <ul style="list-style-type: none">- Nissum Bredning floaterSemispher: R = 0.5 m		1) STATICS: Force balance xz plane 2) DYNAMICS: Single Floater response, SDOF, Linear PTO Damping 2 nd order delay system																												
Hydrodynamics <ul style="list-style-type: none">- Regular Waves- Excitation frequency $\omega_w = 0.9$ rad/s- Wave Height: $H_s = 2$ m- Wave period: $0.5s < T \leq 21$ s (78 unequally spaced ω)- Draft: 0.5 m- Depth: 2 m Model in background 256 quad elements mesh		<table><tr><th>Domain</th><th>Subject</th><th>Stat.</th></tr><tr><td rowspan="10">Time (Linear Time Variance) Frequency (LTV)</td><td>• Linear Potential theory</td><td>✓</td></tr><tr><td>• Coefficients</td><td>✓</td></tr><tr><td>• Equation of motion</td><td>✓</td></tr><tr><td>- Prony method</td><td>✓</td></tr><tr><td>• Magnitude G, Phase Φ {Impedance}</td><td>✓</td></tr><tr><td>- $G(j\omega) < 0.5$</td><td>✓</td></tr><tr><td>- ω</td><td>✓</td></tr><tr><td>- $-90^\circ < \Phi < 90^\circ$</td><td>✓</td></tr><tr><td>- Phase min. sys</td><td>✓</td></tr><tr><td>• Variable Damping</td><td>✓</td></tr><tr><td>• Power absorption ratio</td><td>✓</td></tr></table>			Domain	Subject	Stat.	Time (Linear Time Variance) Frequency (LTV)	• Linear Potential theory	✓	• Coefficients	✓	• Equation of motion	✓	- Prony method	✓	• Magnitude G , Phase Φ {Impedance}	✓	- $ G(j\omega) < 0.5$	✓	- ω	✓	- $-90^\circ < \Phi < 90^\circ$	✓	- Phase min. sys	✓	• Variable Damping	✓	• Power absorption ratio	✓
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Exp. Testing (~ Scale 1:40)		Design single motored floater																												



Figure 4:

Conclusions	Status
• Satisfactory overlapping of Floater response: $z(t)$, $v(t)$. (delay of 0.35 s neglectable)	✓
• Computational efficiency in time: Prony approximation	✓
• Matched Characteristic behaviour of a MSD in frequency	✓
• Control systems: Basic predictive Scheme FDM, System Markow parameters	✓
• Partial Analysis of Power absorption ratio (Power spectra)	½ ✓
Issues	Status
• Irregular Waves	Ø
• Optimum Damping	Ø
• Control Strategies	Ø
• Stability	Ø
• State Feedback (Latching) e.g. Kalman filter	Ø

$$P_a(\omega) = \frac{R_m \left| \hat{F}_c(\omega) \right|^2}{2(R_m + R_r)^2} \frac{1}{1 + \left(\frac{\omega_0}{2\delta} \right)^2 \left(\frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right)^2}$$

Wave Star Energy (WSE) is a group of currently 13 employed engineers & technician, supported by Danfoss A/S. Covering the projects demand for installation, machine design, electronics & general simulation purposes, it is a steadily growing unit.

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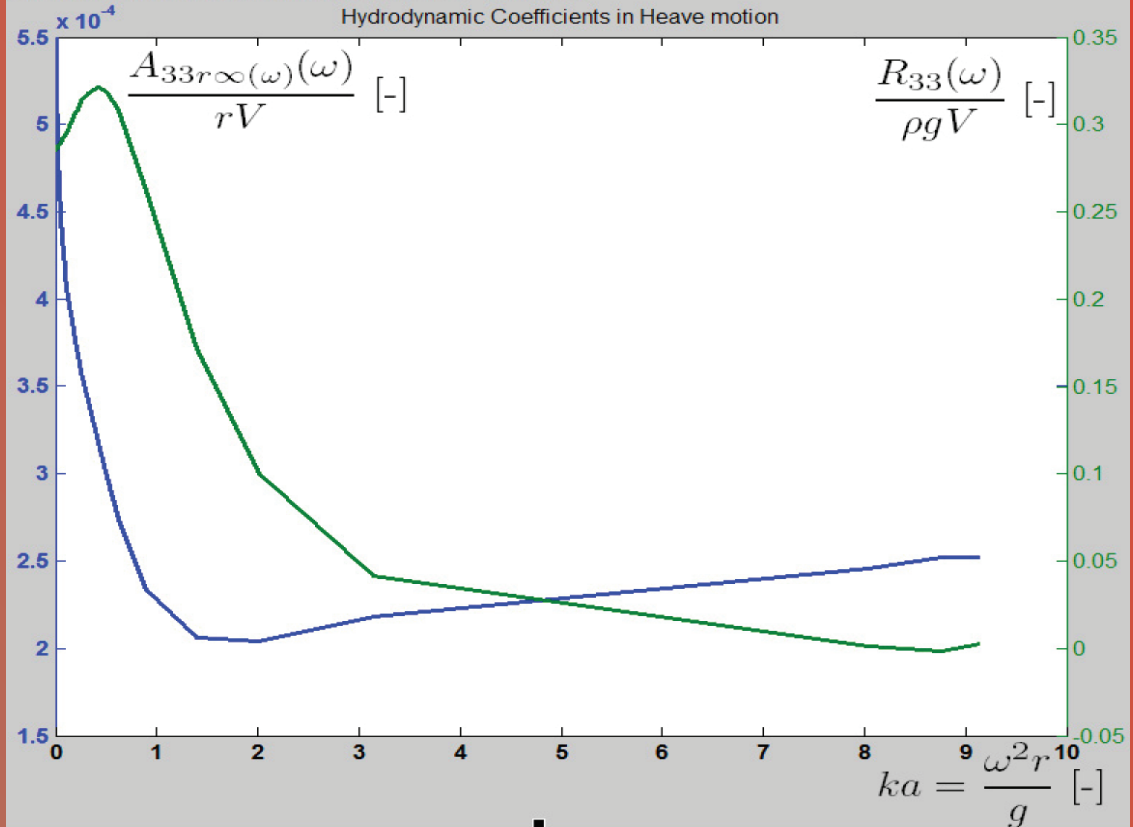


Figure 5:

Nondimensionalized Added Mass $A(\omega)/(\rho V)$ (blue) and Radiation Damping $R(\omega)/\rho g \omega$ (green) in heave motion (33) over the normalized wave number $\omega r/g$. Memory function $k_e(t)$ fitted over Prony method with 8 exponentials.

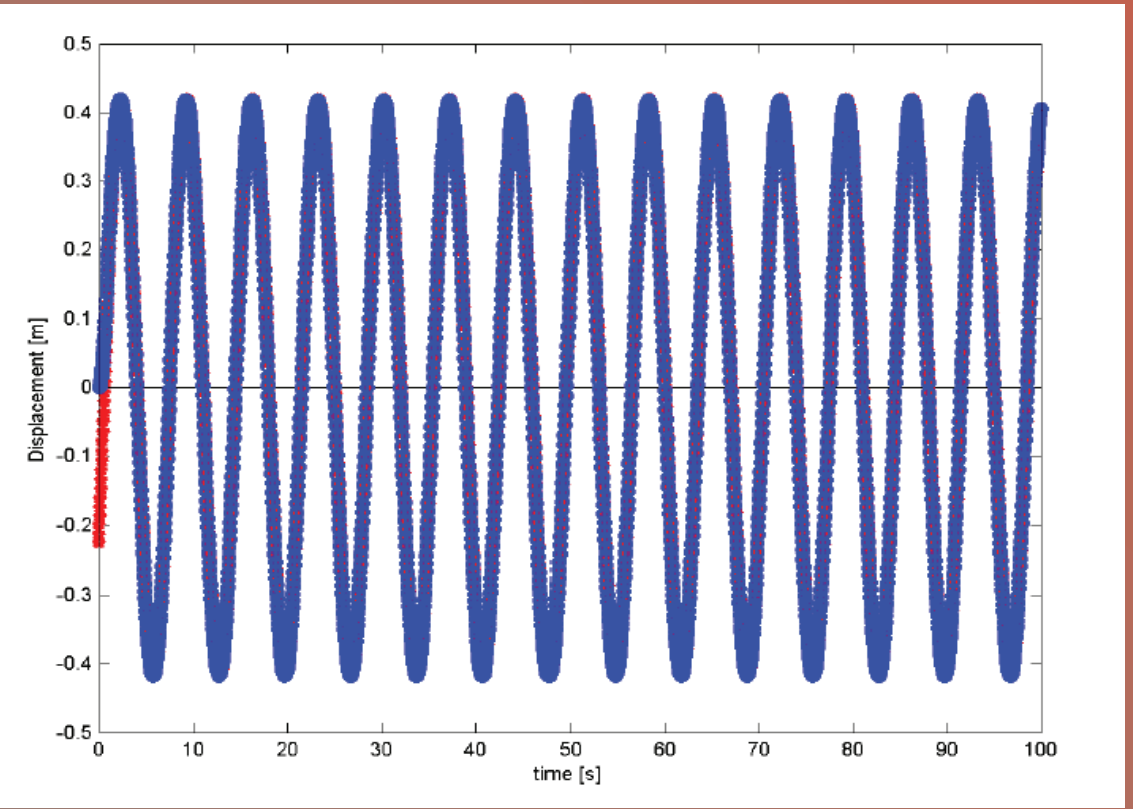


Figure 6:

Forced oscillation over 100 s: Displacement in m over time [s] for ω_w . Comparison of frequency domain derived values (blue $z(t) := |G(j\omega_w)| f_w$) and time calculated ones (red- $z(t):=ode45$). Hydrodynamic force amplitude 8 kN.

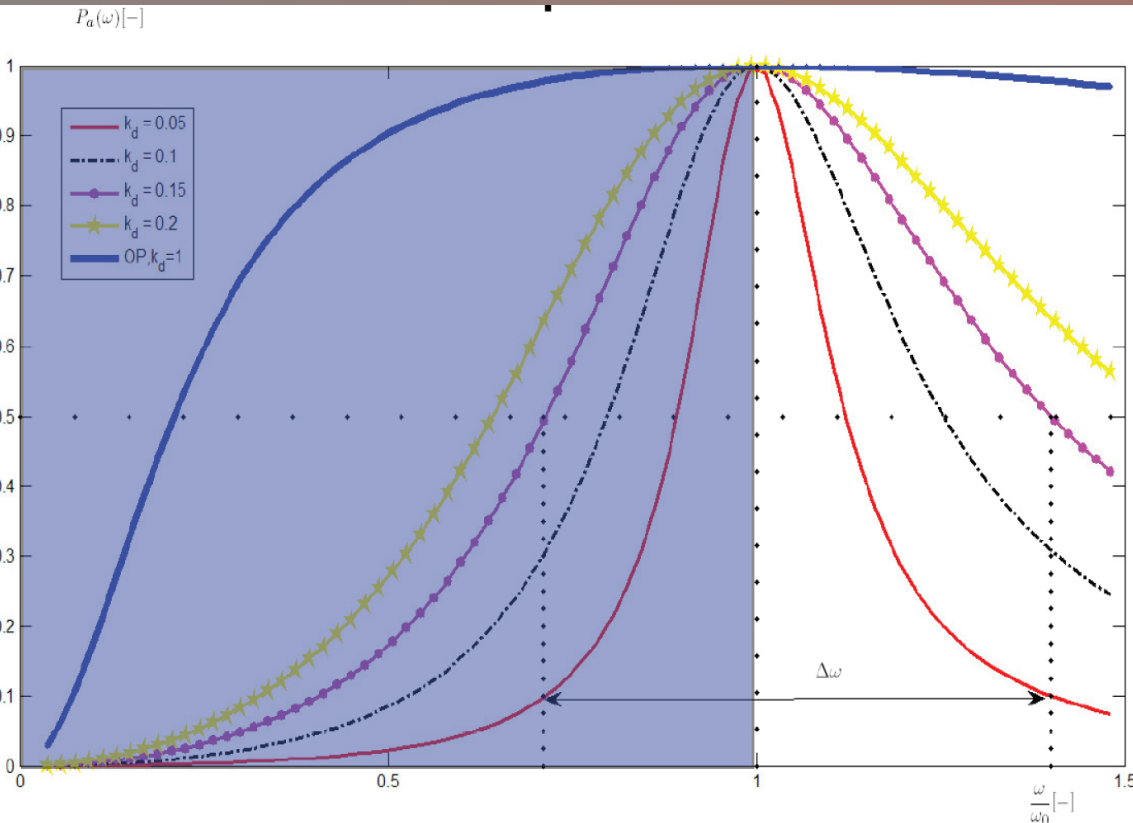


Figure 7:

Normalized Power absorption curve $P_a [-]$ over variable linearized (Factor k_d)*damping ratios δ/ω_0 . Blue background (left Eqn.): Simulated ω -range ($\omega_0 = 8.5$ rad/s). Limited operative range due to $\omega_{max} = 12$ rad/s. Right: Linear interpol. frequencies over ω_{max} for the LTV system.

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