

Evaluation of the Load-Displacement Relationships for Large-Diameter Piles in Sand

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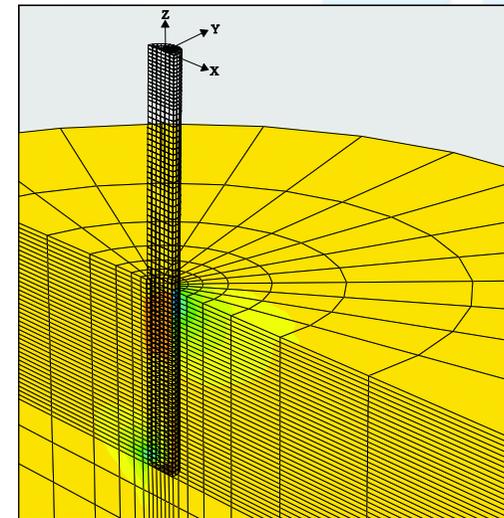
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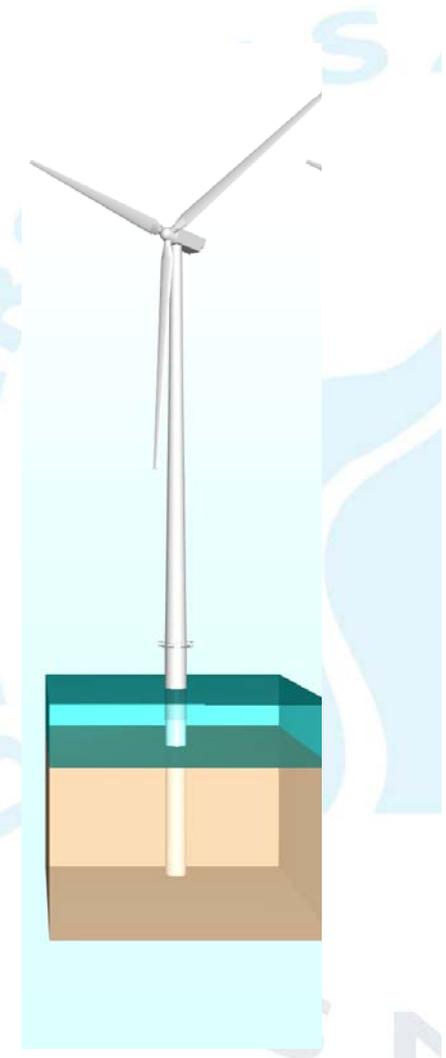
Outline

- Introduction
- Objective
- Current design basis
- Laboratory tests
- Numerical simulations
- Conclusions and future research



Introduction

- Global warming \Rightarrow Interest in renewable energy sources
- Offshore wind energy
- Large-diameter pipe pile – “monopile”



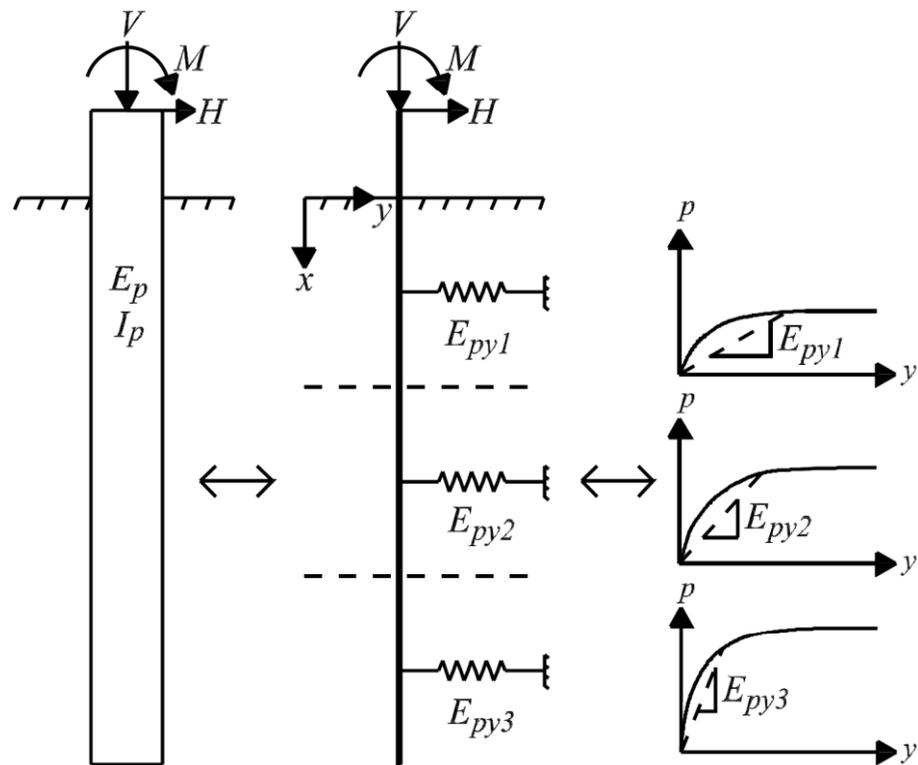
Objective

For **laterally loaded piles in sand with diameters up to 6m**, for example monopiles used as foundations of offshore wind turbines, there is **no approved design procedure**. The $p - y$ curve method, given in offshore design regulations, is usually employed for the design of monopiles. However, this method **was developed for slender piles** with diameters much less than 6m and it is based on a limited number of tests.

The aim of the present work is to extend the $p - y$ curve method to large-diameter non-slender piles by considering the effects of the pile diameter on the soil response!

Current design basis

- Winkler model approach
- Beam on an elastic foundation
- Series of uncoupled springs
- Soil response given by means of p - y curves



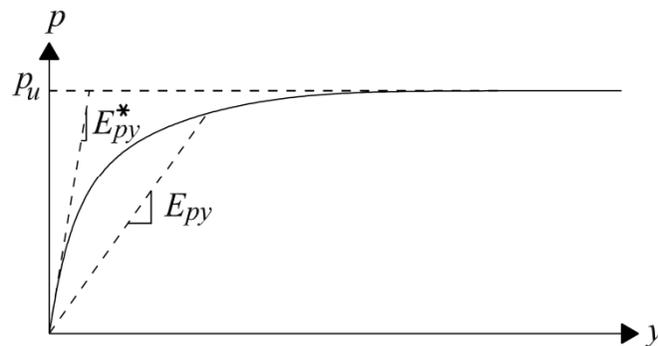
Current p - y curve formulation (API and DNV)

Full-scale tests at Mustang Island:

- $D = 610$ mm, $L/D = 34.4$
- 2 static and 5 cyclic tests

$$p(y) = Ap_u \tanh\left(\frac{E_{py}^*}{Ap_u} y\right)$$

$$E_{py}^* = kx$$



Monopiles for modern wind turbine foundations:

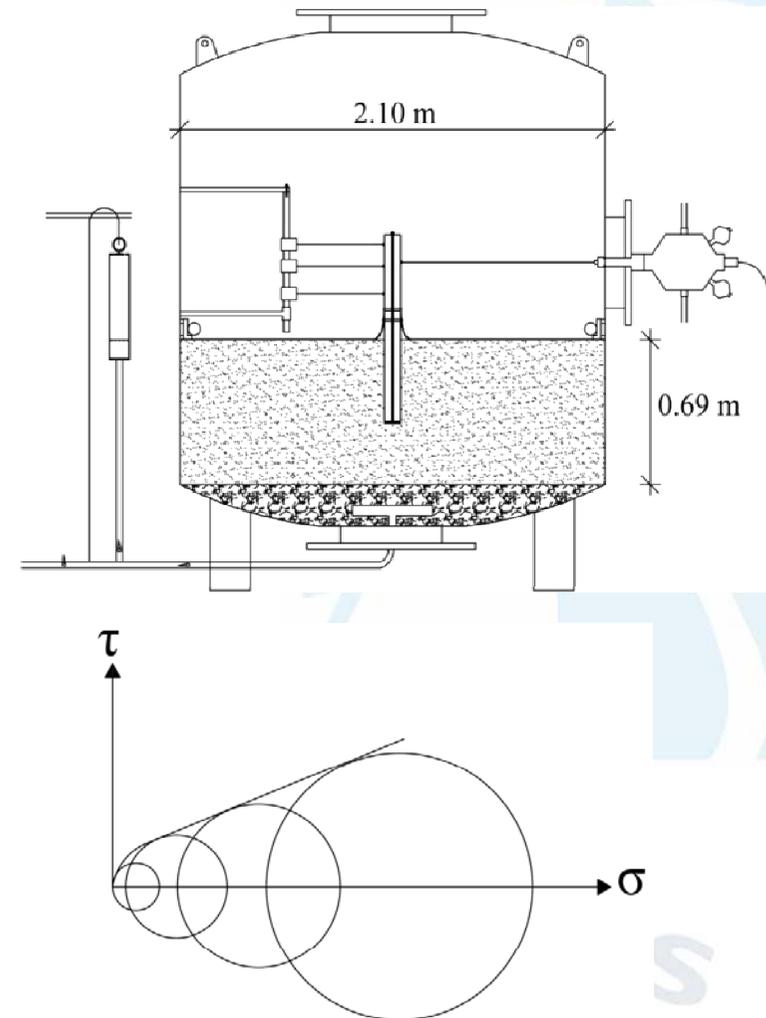
- $D = 4$ - 6 m, $L/D \approx 5$
- Strict requirements regarding pile-head rotation and total stiffness of the structure

Verification of p - y curves for large-diameter piles is needed

Laboratory tests

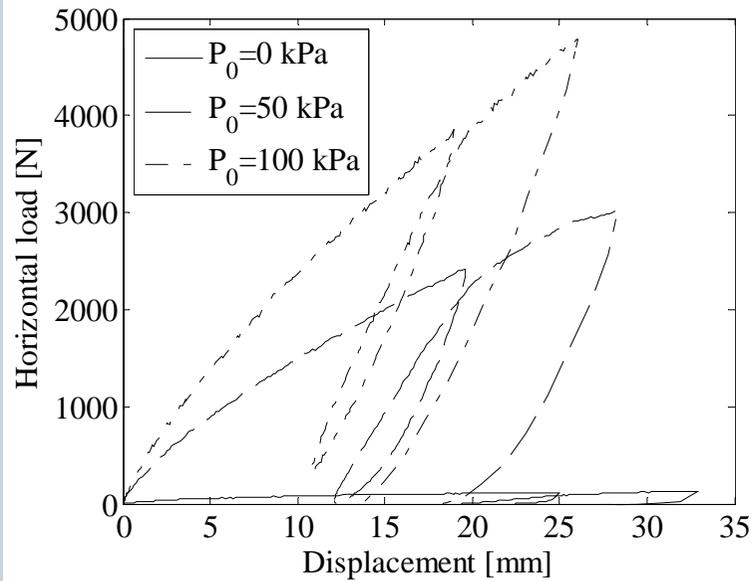
- Effect of diameter
- Verification of numerical model
- Pressure tank (new test method)
- Piles instrumented with strain gauges

	D [mm]	L [mm]	[kPa]
Test 1	80	400	0
Test 2	80	400	100
Test 3	80	400	50
Test 4	60	300	0
Test 5	60	300	50
Test 6	60	300	100

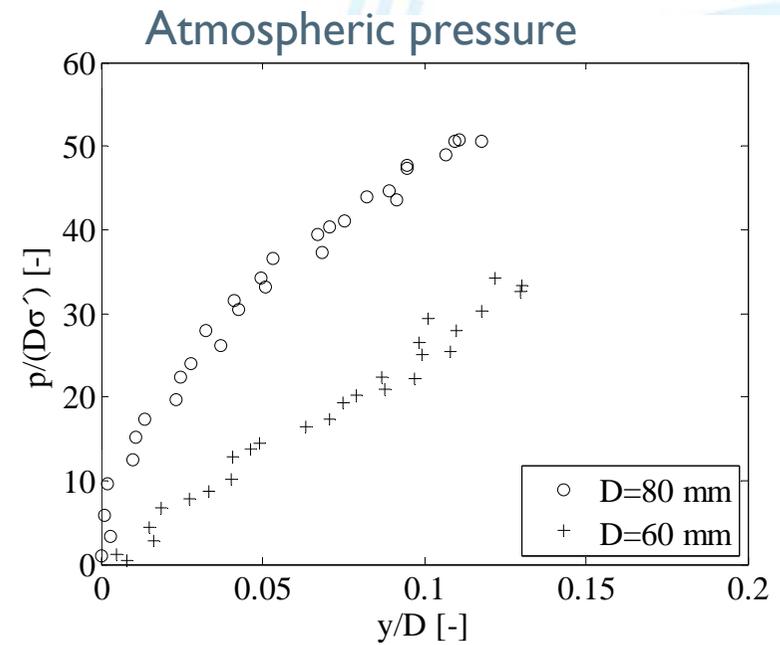


Results from laboratory tests

Effect of overburden pressure

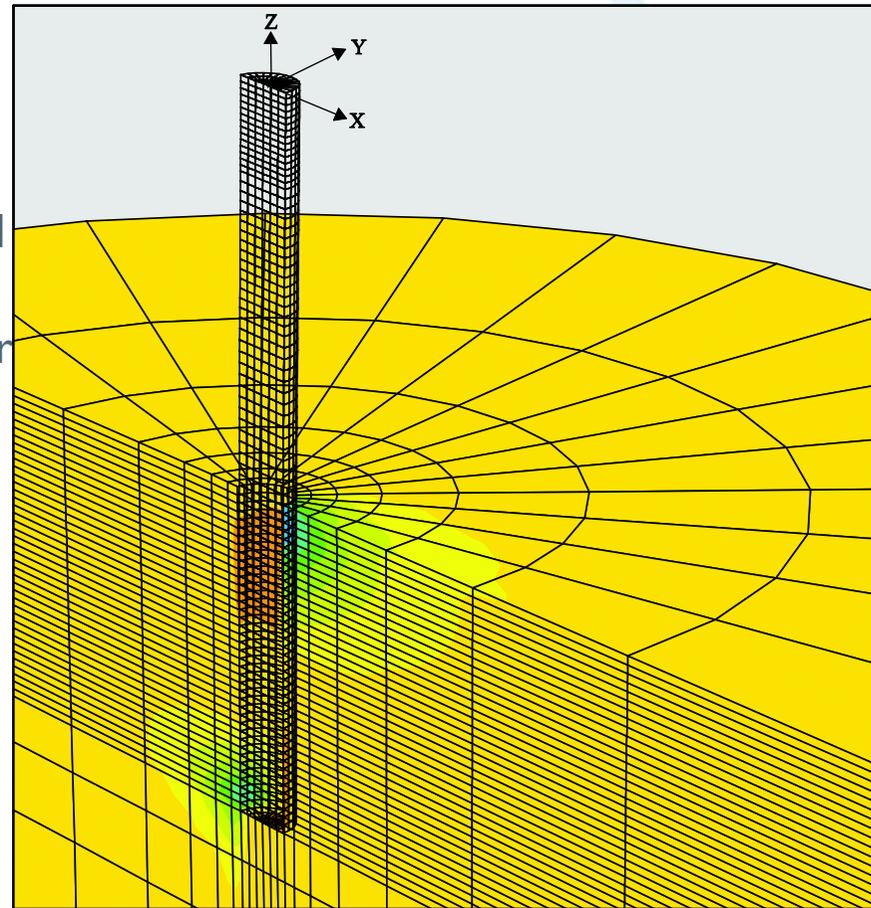


Increase in E_{py}^* for increasing D



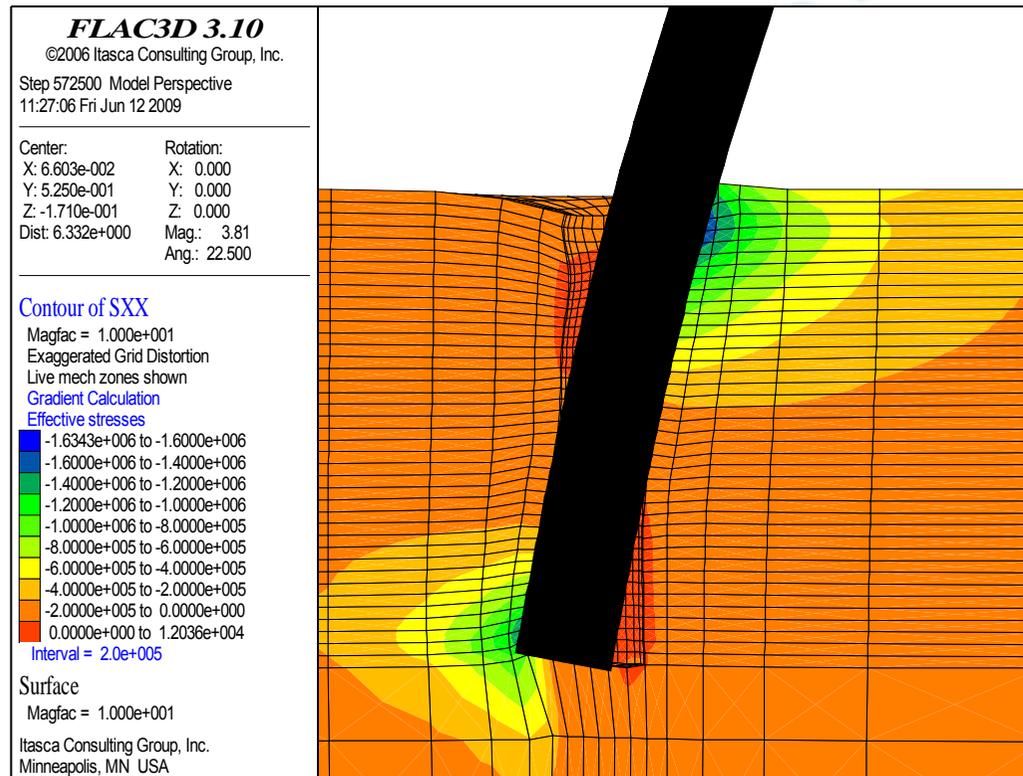
Numerical simulations in *FLAC^{3D}*

- Commercial program
- Finite difference method
- Dynamic solver
- Mohr-Coulomb material model
- Symmetric model
- Pile modelled as a solid cylinder with equivalented EI



Soil-pile interaction

- Linear Coulomb shear-strength criterion
- Tension cut-off



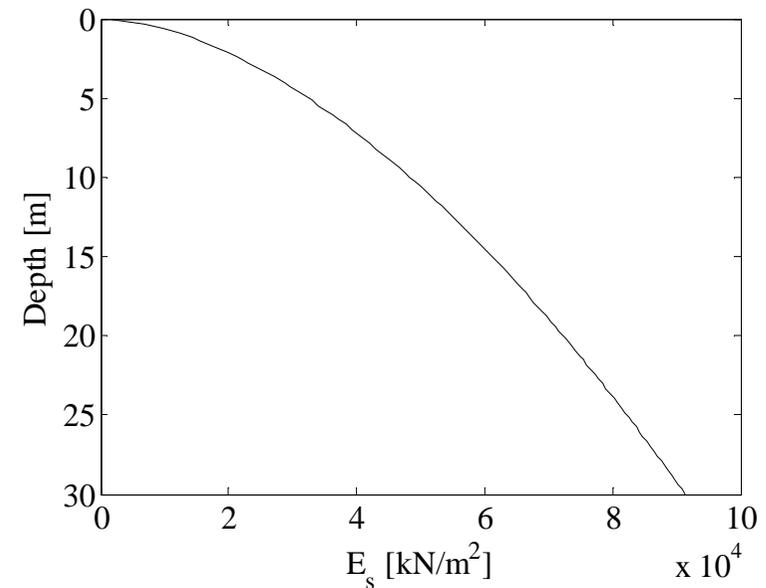
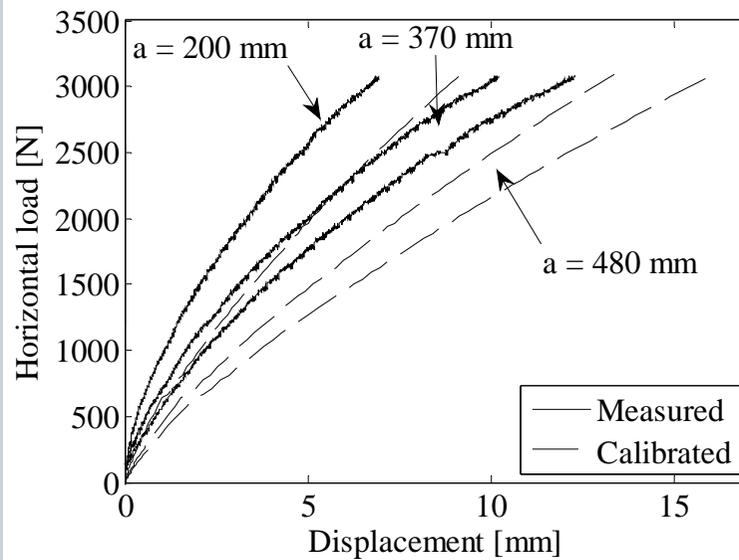
Simulation of large-scale monopiles

Comparison with laboratory tests:

- Soil parameters determined by CPT

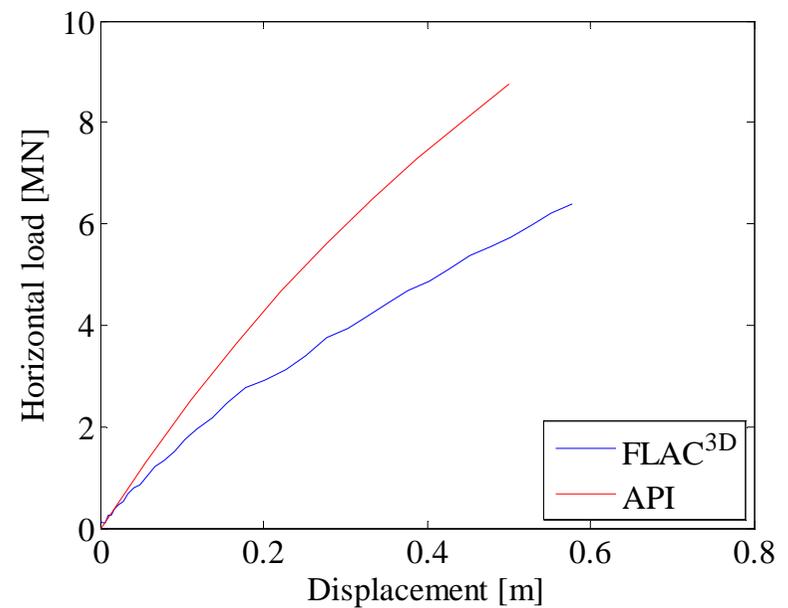
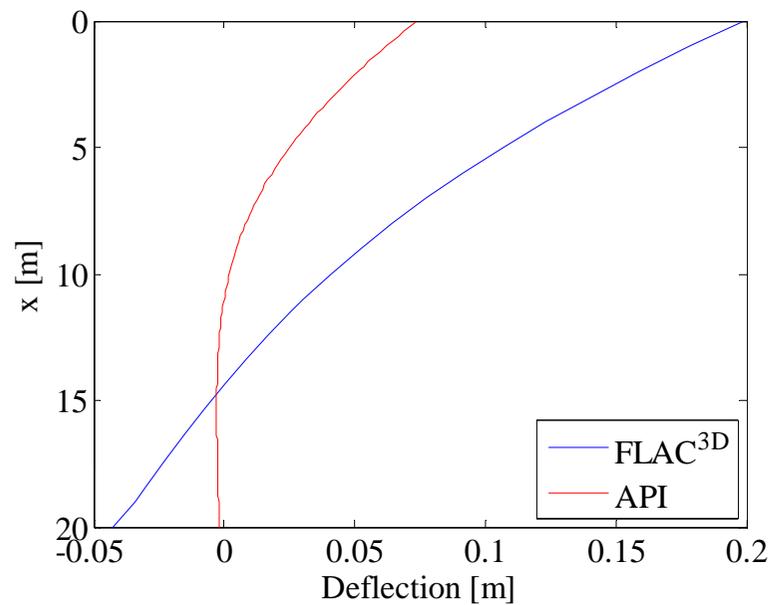
Large scale piles:

- $D = 2-7$ m, $L = 20$ m, $t = 50$ mm
- $f = 40^\circ$, $\gamma = 10^\circ$, $c = 0.1$ kPa
- Varying E_s



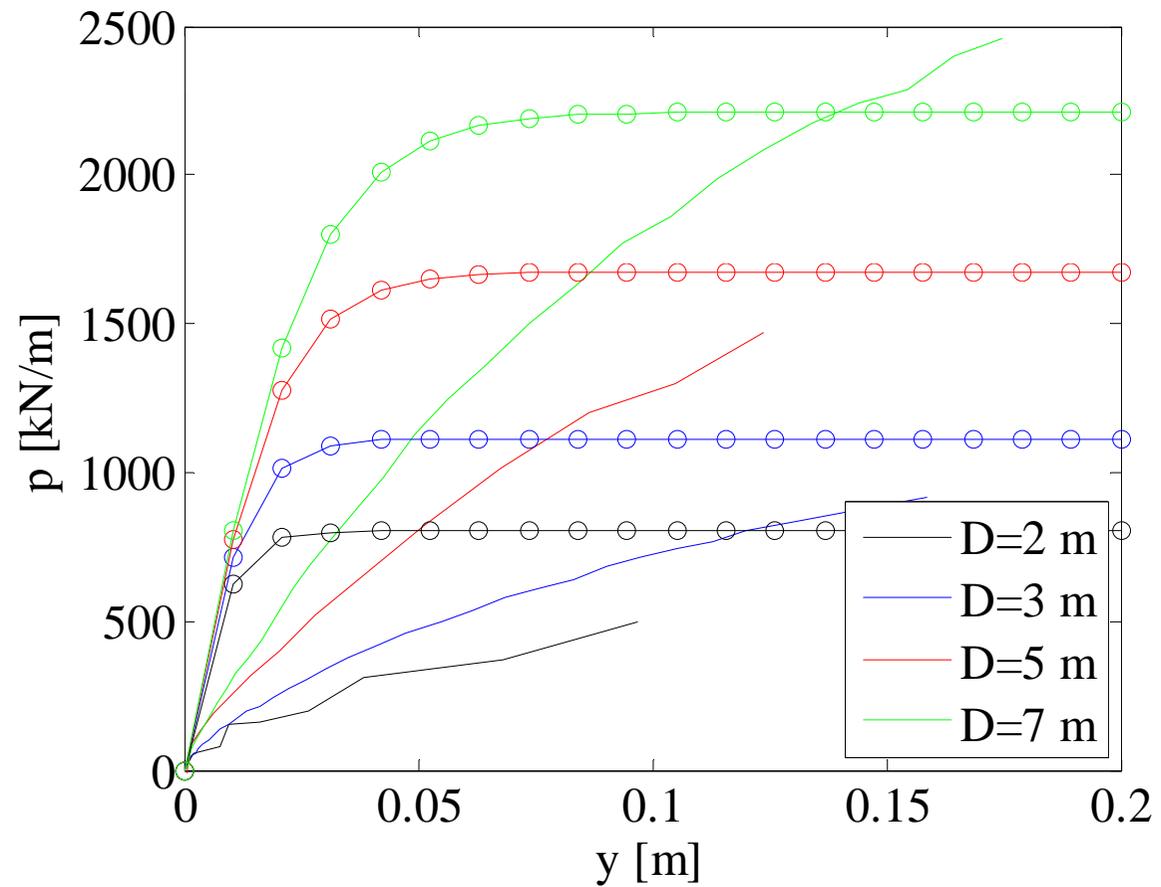
Comparison of numerical simulations with the Winkler model approach

$D = 3 \text{ m}$



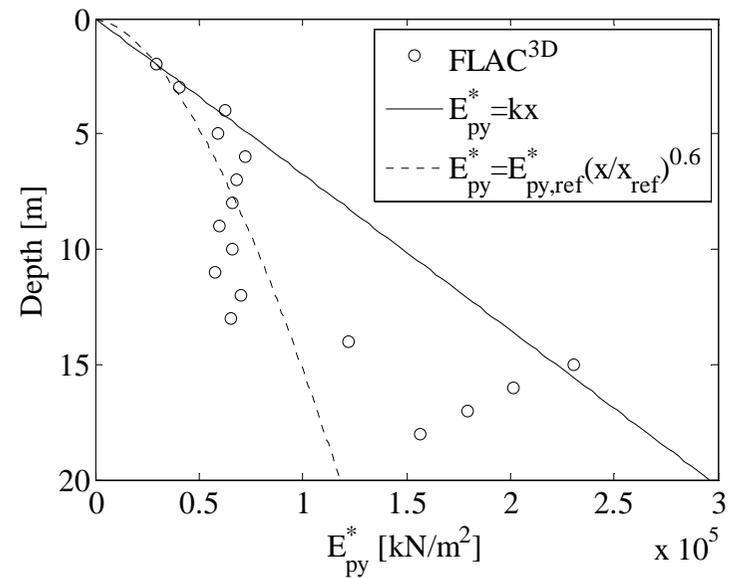
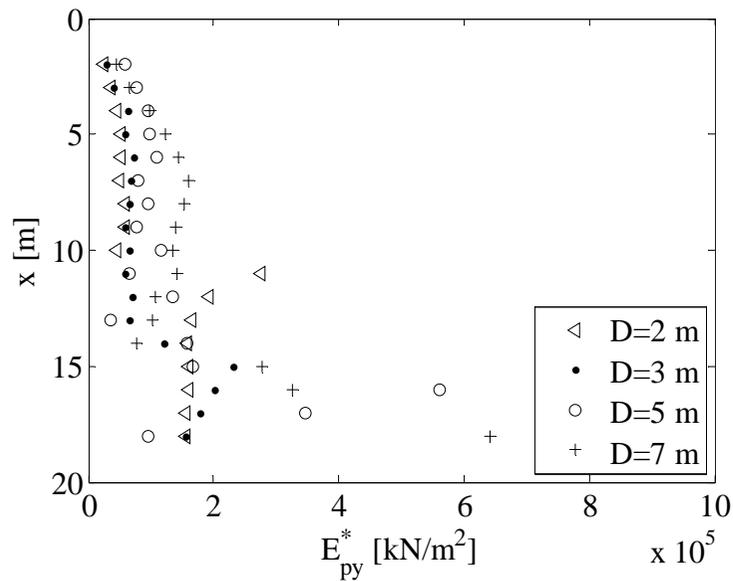
Validation of p - y curves

Depth, $x=2$ m



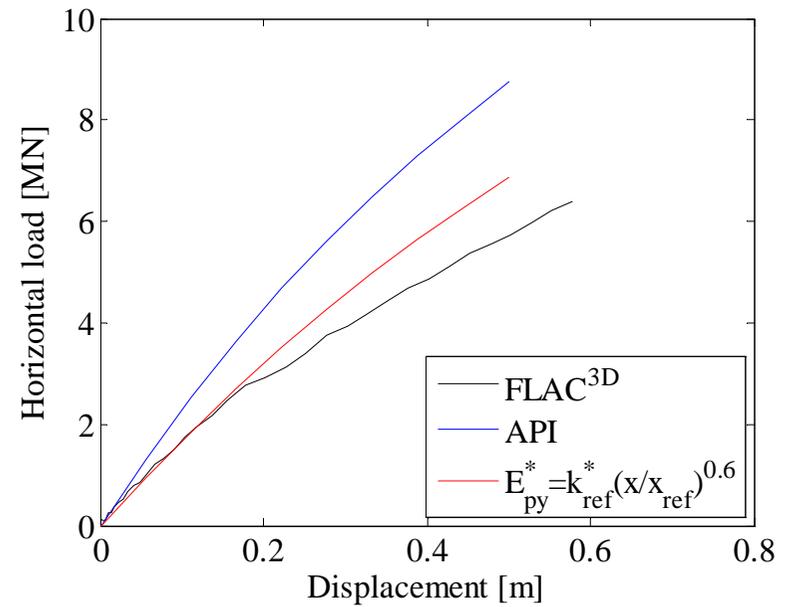
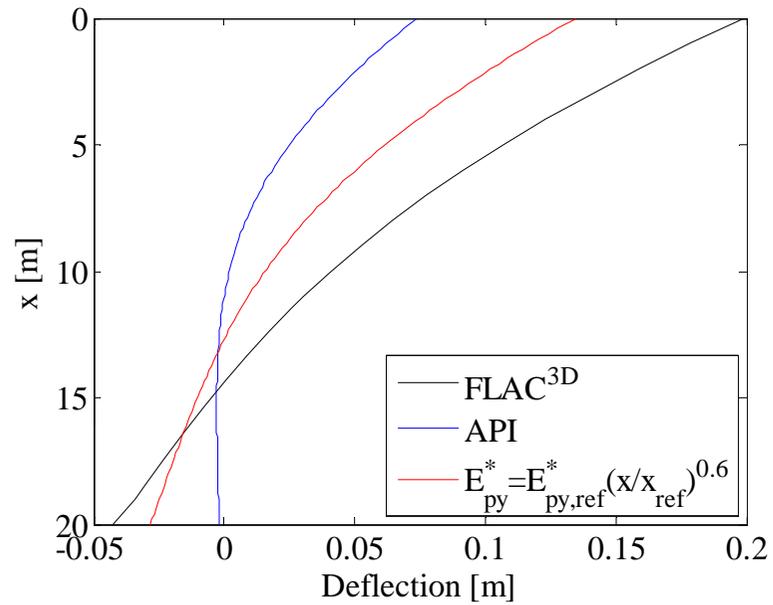
Initial stiffness

- E_{py}^* increase with increasing D
- Non-linear variation of $E_{py}^* \neq kx$
- Lesny and Wiemann (2006)



Improved p-y curves

$$E_{py}^* = \left(\frac{x}{x_{ref}} \right)^{0.6} \cdot k_{ref}$$



Conclusions

Increase in E_{py}^* for increasing D

- Numerical analyses and laboratory tests

Non-linear variation of E_{py}^* with depth

- Power function, numerical analyses

Updated p - y curves for large-diameter piles is needed

Future research

- Cyclic loading has to be considered
- Assessment of a wider range of soil and pile properties
- Full-scale measurements are needed

Thank you for your attention!

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