

Anholt

Konsolideringsforsøg (Datarapport 1)

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Anholt
Konsolideringsforsøg
Datarapport

Udarbejdet Grete Thorsen

Kontrolleret Lars Bo Ibsen

Godkendt

Anholt
Konsolideringsforsøg
Marint ler, Eem og Jura

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1. Indledning

Denne datarapport indeholder resultater af konsolideringsforsøg med tre prøver af interglacialt ler fra Eem mellemistid, en lerprøve fra Mellem Jura og en lerprøve fra Nedre Jura. Prøverne er udtaget fra kerner fra en geologisk undersøgelsesboring. Boringen er udført i foråret 1990 som led i et forskningsprojekt, GEOKAT-projektet. Geokatprojektet var et forskningsrådsstøttet projekt ved Geologisk Institut, Aarhus Universitet. Den gennemborede lagserie er beskrevet i Dansk Geologisk Forening, Årsskrift for 1990-91 (Nielsen, 1992).

2. Formål

Det væsentligste formål med forsøgene har været at undersøge om det var muligt at bestemme forkonsolideringsspenningen for aflejringerne til vurdering af den geologiske historie.

3. Forsøgsmateriale

Prøverne til konsolideringsforsøgene er udtaget fra kerneprøver, hvilket betyder, at de kan have haft mulighed for at svelle i forbindelse med prøveoptagningen. Efter optagning har prøverne været opbevaret i plastikrør, men de har ikke været opbevaret lufttæt, og der er derfor foregået nogen udtørring af prøverne.

Ved klassifikationsforsøg er bestemt følgende før forsøg:

Prøve P1	Eem	$w = 19,8\%$	$\gamma = 19.8 \text{ kN/m}^3$	$e = 0.61$	$S_w \sim 88\%$
Prøve P2	Eem	$w = 22.5\%$	$\gamma = 19.5 \text{ kN/m}^3$	$e = 0.68$	$S_w \sim 91\%$
Prøve k12	Eem	$w = 17.8\%$	$\gamma = 21.3 \text{ kN/m}^3$	$e = 0.48$	$S_w \sim 96\%$
Prøve k26	mellem Jura	$w = 12,3\%$	$\gamma = 19.0 \text{ kN/m}^3$	$e = 0.47$	$S_w \sim 75\%$
Prøve k98	nedre Jura	$w = 16,8\%$	$\gamma = 21.2 \text{ kN/m}^3$	$e = 0.46$	$S_w \sim 99\%$

Prøverne er antaget fuldt vandmættet ved afslutning af konsolideringsforsøget.

For Eem prøverne er skønnet en relativ korndensitet på $d_s = 2.72$, for prøve k26 og k98 er den relative korndensitet skønnet til henholdsvis $d_s = 2.69$ og $d_s = 2.7$

For prøve k12 er bestemt vandindholdet ved flydegrænsen $w_L = 32.1\%$ og vandindholdet ved plasticitetsgrænsen $w_p = 15.4\%$, hvilket giver et plasticitetsindeks $I_p = 16.7\%$

4. Forsøgsprogram

Forsøgene er udført i det danske konsolideringsapparat med prøvestørrelse $H \times D = 35 \times 70 \text{ mm}$ for prøve P1 og $H \times D = 30 \times 60 \text{ mm}$ for de øvrige prøver. Apparaterne havde en lille filtersten i det nederste trykhoved og som drænevej er anvendt $H_d = 0,7 \times D$.

Forsøgene er udført ved trinvis belastning. Ved forsøgene med prøve P1 og P2 er de enkelte belastningstrin afbrudt, når det kunne konstateres, at konsolideringsprocessen var afsluttet og maksimalbelastning er aftaget på én gang. Ved de øvrige forsøg er varigheden af de enkelte belastningstrin søgt afpasset, så krybningsdekadehældningen kunne bestemmes på de enkelte belastningstrin og så svelling var minimal på aflastningstrinene.

5. Tolkning af forsøg

Ved tolkning af tidskurverne er anvendt en adskillelse af konsolideringstøjning og krybningstøjning som angivet af Moust Jacobsen (Jacobsen, 1992). Krybekurverne er beregnet ud fra følgende udtryk $\epsilon_{kryb} = Q_s \times \log((t_A + t)/t_A)$, hvor Q_s er den maksimale værdi for ϵ_s .

For tidskurver ved spændinger op til den maksimale værdi af krybningstøjningsindekset, Q_s , er nået er denne værdi anvendt. For tidskurver ved højere spændinger er den aktuelle værdi for krybningsstøjningsindekset, ϵ_s , anvendt i stedet for Q_s .

Tiden, t_A , er fundet som den tid, der giver en krybekurve, der falder sammen med den sidste del af tidskurven, hvorved konsolideringstøjningen, ϵ_c , bliver konstant med tiden. Samtlige tidskurver med angivet adskillelse af konsolideringskurve og krybekurve fremgår af bilagene.

Tiden, t_A , er kraftigt faldende op til forkonsolideringsspændingen er nået, hvorefter den er næsten konstant eller meget svagt faldende. Da der er tale om bortdræning af vand både under konsolideringsprocessen og ved krybning, vil størrelsen af t_A , når materialet er i normalkonsolideret tilstand, sandsynligvis ligesom konsolideringstiden være afhængig af den aktuelle drænvej.

Ved tolkning af konsolideringsforsøgene er foretaget bestemmelse af forkonsolideringsspænding, σ'_{pc} , tøjningsindeks, Q , krybningstøjningsindeks, ϵ_s , det maksimale krybningstøjningsindeks, Q_s , svarende til normalkonsolideret tilstand, samt konsolideringskoefficient ved 10^0C , $c_{k10} = k_{10} \times K / \gamma_w$. Konsolideringskoefficienten er beregnet ud fra følgende udtryk, $c_{k10} = (\pi/4) \times (H_d)^2 / t_c$, hvor t_c er den tid, hvor tidskurvets rette linie i v_t – afbildning skærer værdien for konsolideringstøjningen, ϵ_c . Som drænvej er anvendt $H_d = 0,7 \times D$.

Resultaterne fremgår af bilag 2.1 – 6.1. På grund af de ret korte tidskurver ved forsøgene med prøve 1 og 2 er der noget usikkerhed i bestemmelse af krybningstøjningsindeks..

For hvert belastningstrin er bestemt konsolideringsmodulen, $K = \Delta\sigma' / \Delta\epsilon_c$, som stort set svarer til tangentmodulen ved belastningstrinnets middelspænding. Resultaterne fremgår af bilag 2.2 – 6.2.

Forkonsolideringsspændingen, σ'_{pc} , er bestemt ud fra:

- variationen af tiden t_A på de enkelte belastningstrin (bilag 2.1 – 6.1)

samt følgende kriterier (dgf-Bulletin 15, 2001):

- knæk i ϵ_s - σ' kurven, hvor ϵ_s når den maksimale værdi, Q_s
- knæk eller spring i K - σ'_{middel} kurven
- afbøjning fra en ret linie i σ' - ϵ_c kurve

Der er fundet rimelig god overensstemmelse mellem de forskellige kriterier.

For prøverne k26 og k98 er de i afsnit 6 anførte værdier for Q og σ'_{pc} minimumsværdier, idet forkonsolideringsspændingen sandsynligvis ikke er nået i forsøget.

Ved at antage fuld vandmætning ved forsøgets slutning er udregnet et begyndelsesvandindhold ved hvert enkelt belastningstrin, værdierne fremgår af bilag 2.2 - 6.2.

6. Forsøgsresultater

Arbejdskurverne for de enkelte konsolideringsforsøg fremgår af bilag 2-6

Beregne og målte værdier samt tolkede parametre er angivet i nedenstående skema:

Prøve no.	Alder	w %	σ'_{pc} MPa	σ'_0 MPa	K MPa	Q %	Qs %	α Qs/Q	OCR σ'_{pc}/σ'_0	I_p %
P1	Eem	22,6	>3	~0,78	~50	9,5?	~0,5	~0,05	~4	
P2	Eem	24,9	>4	~0,78	~60	13?	~0,5	~0,04	~5	
k12	Eem	18,5	>2	~0,8	?	~8	~0,23	~0,03	~2,5	16,7
k26	M-jura	17,5	(~8)	~1,6	~100	(~6)	0,11	~0,02	>5	
k98	N-jura	16,8	(>3)	~3	~150	(~5?)	~0,07	~0,01	>1	

σ'_0 er den beregnede effektive spænding in situ, OCR = forkonsolideringsgrad = σ'_{pc}/σ'_0 . De angivne vandindhold er de beregnede vandindhold for $S_w \sim 100\%$.

7. Kommentarer til forsøgsresultater

7.1 Sammenligning med Terzaghi-kurve og Casagrande-konstruktion

På en Terzaghi-kurve, $\varepsilon = Q \times \log ((\sigma'_\kappa + \sigma')/\sigma'_\kappa)$, findes kurvens maksimale krumning ved

$$\sigma' = 0.62 \times \sigma'_\kappa,$$

Anvendelse af Casagrande konstruktion:

Tangenten til kurven i det punkt med størst krumning får hældningen $0.38 \times Q$. Ved en vinkel på 30° mellem tangent og vandret linie gennem tangentpunktet får vinkelhalveringslinien hældningen $0.18 \times Q$. Skæringspunktet mellem vinkelhalveringslinien og kurvens asymptote, $\varepsilon = Q \times \log (\sigma'/\sigma'_\kappa)$, findes ved $\sigma' = 2 \times \sigma'_\kappa$.

På bilag 7 er vist arbejdskurverne for de udførte konsolideringsforsøg med tilpassede Terzaghi-kurver: $\varepsilon = \Delta\varepsilon_0 + Q \times \log ((\sigma'_\kappa + \sigma')/\sigma'_\kappa)$. Terzaghi-kurverne er tilpasset efter følgende princip: Tøjningsindekset Q = den ved forsøget bestemte værdi for Q , σ'_κ så lille som mulig og $\Delta\varepsilon_0$ er den værdi på arbejdskurvens ε - skala, der svarer til $\varepsilon = 0$ på Terzaghi-kurven. I nedenstående skema er de herved fundne værdier for σ'_{pc} og Q sammenholdt med de værdier, der er fundet ud fra forsøgene. For prøve k26 og k98 er forkonsolideringsspenningen sandsynligvis ikke nået i forsøget.

I skemaet er angivet værdier for $\Delta\varepsilon_0$, hvor positive værdier svarer til, at prøverne har udvidet sig inden forsøgsstart, mens negative værdier tyder på et poreundertryk ved forsøgsstart.

Prøve no.	Alder	σ'_0 (kPa)	σ'_{pc} (kPa)	Q (%)	σ'_{pc} (kPa)	Q (%)	$\Delta\varepsilon_0$ (%)	$\Delta\varepsilon_0$ (%)
			Forsøg	Forsøg	Terzaghi	Terzaghi		
1	Eem	~780	>2500	9,5?	4000	15	+0,5	
2	Eem	~780	>4000	13?	4000	15		-0,5
k12	Eem	~800	~5000	~8	4000	11	+4,6	
k26	M-jura	~1620	(~8000)	(~6)	(6000)	(9)		-0,45
k98	N-jura	~3040	(>3000)	(~5)	(6000)	(8)		-0,7

7.2 Sammenligning med skønsformel for tøjningsindeks Q baseret på vandindhold

I DS415:84 er anført følgende skønsformel for normalkonsoliderede, gytjeholdige (dyndede) aflejringer: $Q = 60 \times (w - 25) / (w + 40) \%$, når w indsættes i %. For post- og senglaciale aflejringer fra Skagen 3 boringen (Thorsen, 2006a) er udtrykket $Q = 60 \times w / (w + 90) \%$, fundet som en mulig tilnærmelse.

Fig. 1 viser de ud fra arbejdskurverne fundne værdier for tøjningsindeks, Q , sammenholdt med kurven $Q = 60 \times w / (w + 90) \%$. Som vandindhold er anvendt de begyndelsesværdier, der er beregnet ud fra antagelse om fuld vandmætning ved forsøgets slutning.

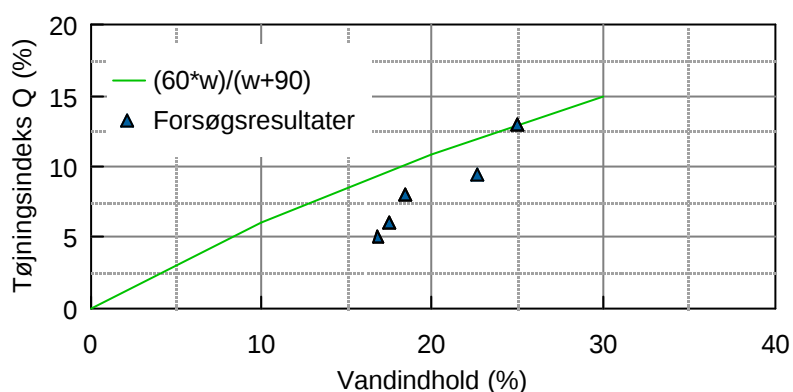


Fig. 1 Tøjningsindeks fra forsøg som funktion af vandindhold

Fig. 2 viser de fundne værdier for tøjningsindeks, Q , der er fundet ved tilpassede Terzaghi-kurver.

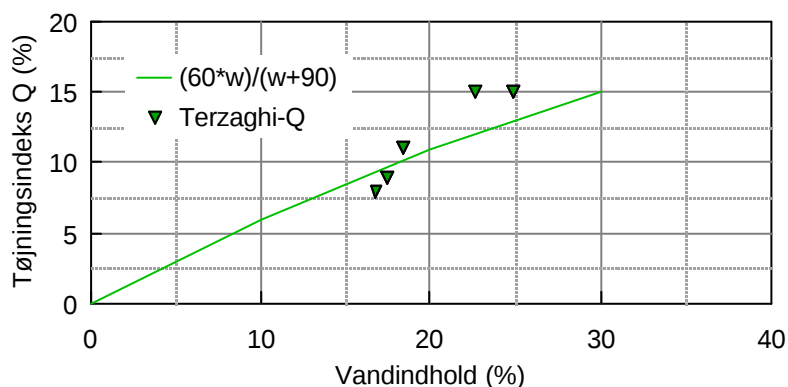


Fig. 2 Tøjningsindeks fra Terzaghi-kurve som funktion af vandindhold

7.3 Sammenligning med andre forsøg med Eem-ler

På fig. 3 er arbejdskurverne for prøve P1, P2 og k12 vist sammen med to arbejdskurver fra forsøg udført på naturfugtige prøver af Eem-ler, Skagen 3, prøve K98 (Thorsen, 2006a) og Nørre Lyngby, prøve A1-P7 (Thorsen, 2006b).

Fig. 4 viser de samme arbejdskurver, men kurverne er forskudt, så ε – skalaen svarer til de tilpassede Terzaghi-kurver. Desuden er indtegnet de dertil svarende asymptoter. I signaturforklaringen for arbejdskurverne er angivet værdien for korrektionen, $-\Delta\varepsilon_0$, og ved asymptoterne er angivet de anvendte værdier for tøjningsindeks, Q , og forbelastningsspænding, σ'_{pc} .

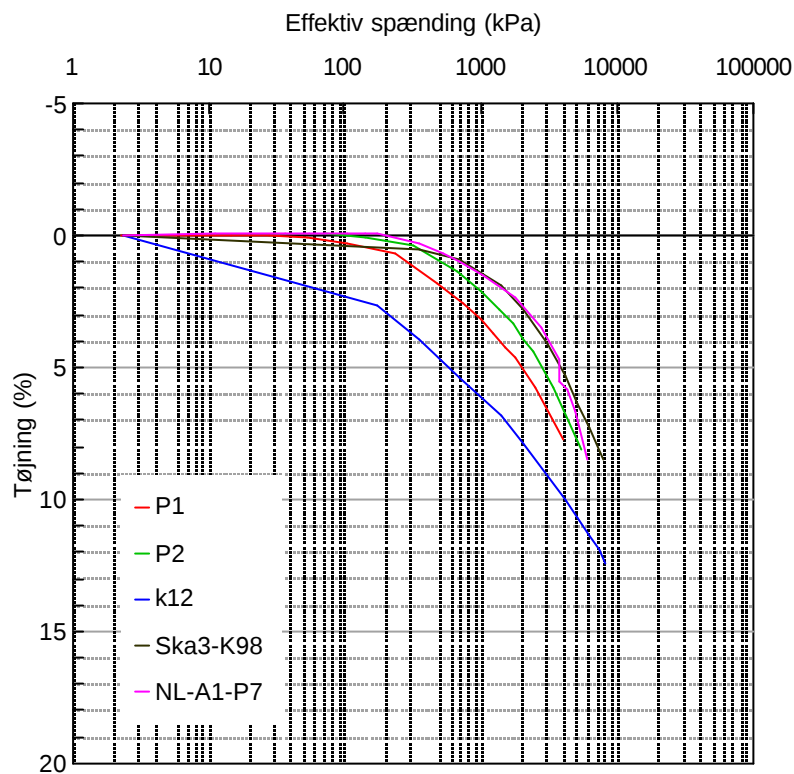


Fig. 3 Arbejdskurver fra P1, P2 og k12 sammenholdt med arbejdskurver fra forsøg med Eemler fra Skagen og Nørre Lyngby.

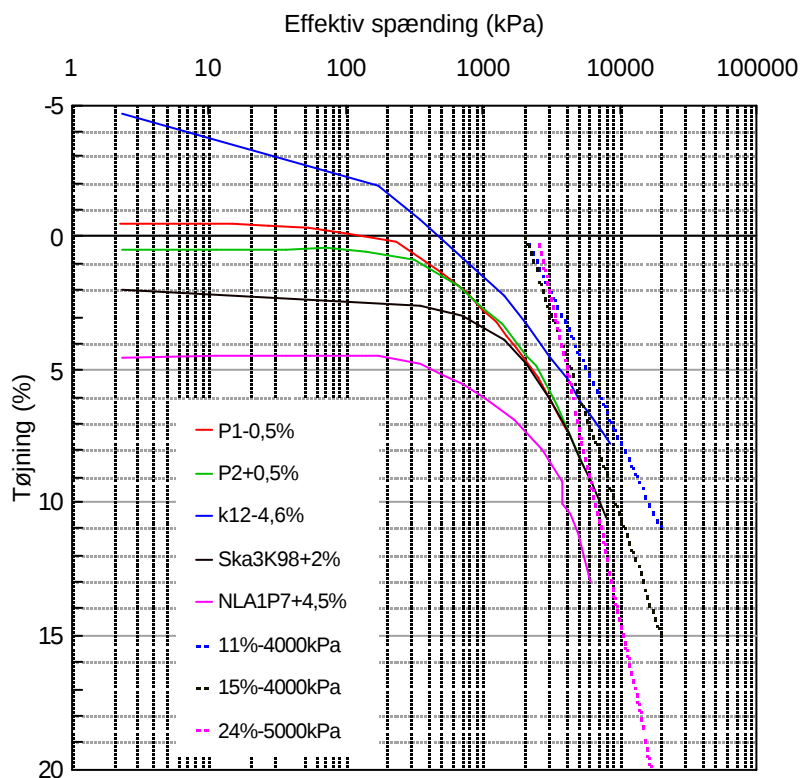


Fig. 4 Arbejdskurver med korrektioner svarende til Terzaghi-kurver samt de dertil svarende asymptoter.

For prøverne P1, P2 og Ska3K98 (beregnete begyndelsesvandindhold på henholdsvis ~23, ~25 og ~27 %) er ved tilpassede Terzaghi-kurver fundet ens værdier for tøjningsindeks, $Q = 15 \%$, og forkonsolideringsspænding, $\sigma'_{pc} = 4000 \text{ kPa}$.

For prøve k12 (beregnet begyndelsesvandindhold på $w = \sim 18 \%$) er fundet tøjningsindeks $Q = 11 \%$ og forkonsolideringsspænding $\sigma'_{pc} = 4000 \text{ kPa}$.

For prøve NLA1P7 (beregnet begyndelsesvandindhold på $w = \sim 29 \%$) er fundet tøjningsindeks $Q = 24 \%$ og forkonsolideringsspænding $\sigma'_{pc} = 5000 \text{ kPa}$.

De aktuelle forsøgsresultater viser ikke markante forskelle, der kan henføres til prøvernes kvalitet.

8. Konklusion

Der er udført 5 konsolideringsforsøg med 5 kerneprøver, 3 prøver af interglacialt ler Eem, 1 af ler fra mellem Jura og 1 af ler fra nedre Jura.

Det væsentligste formål med forsøgene var at forsøge at bestemme aflejringeres forkonsolideringsspænding.

Ved tolkning af forsøgenes tidskurver er anvendt en adskillelse af konsolideringstøjning og krybningstøjning som angivet af Moust Jacobsen (jfr. afsnit 5).

Resultaterne af forsøgene fremgår af afsnit 6.

De aktuelle arbejdskurver er sammenlignet med Terzaghi-kurver med indlagt Casagrandekonstruktion. Resultaterne fremgår af bilag 7 samt afsnit 7.1.

Prøvematerialet er udtaget af kerneprøver, der efter optagningen har været opbevaret i plastikrør, en ikke lufttæt opbevaring. Forsøgsresultaterne kunne derfor være påvirket af en eventuel ændring af prøvematerialet efter optagning. Der er derfor foretaget en sammenligning med resultater fra andre forsøg (jfr. afsnit 7.2 og 7.3).

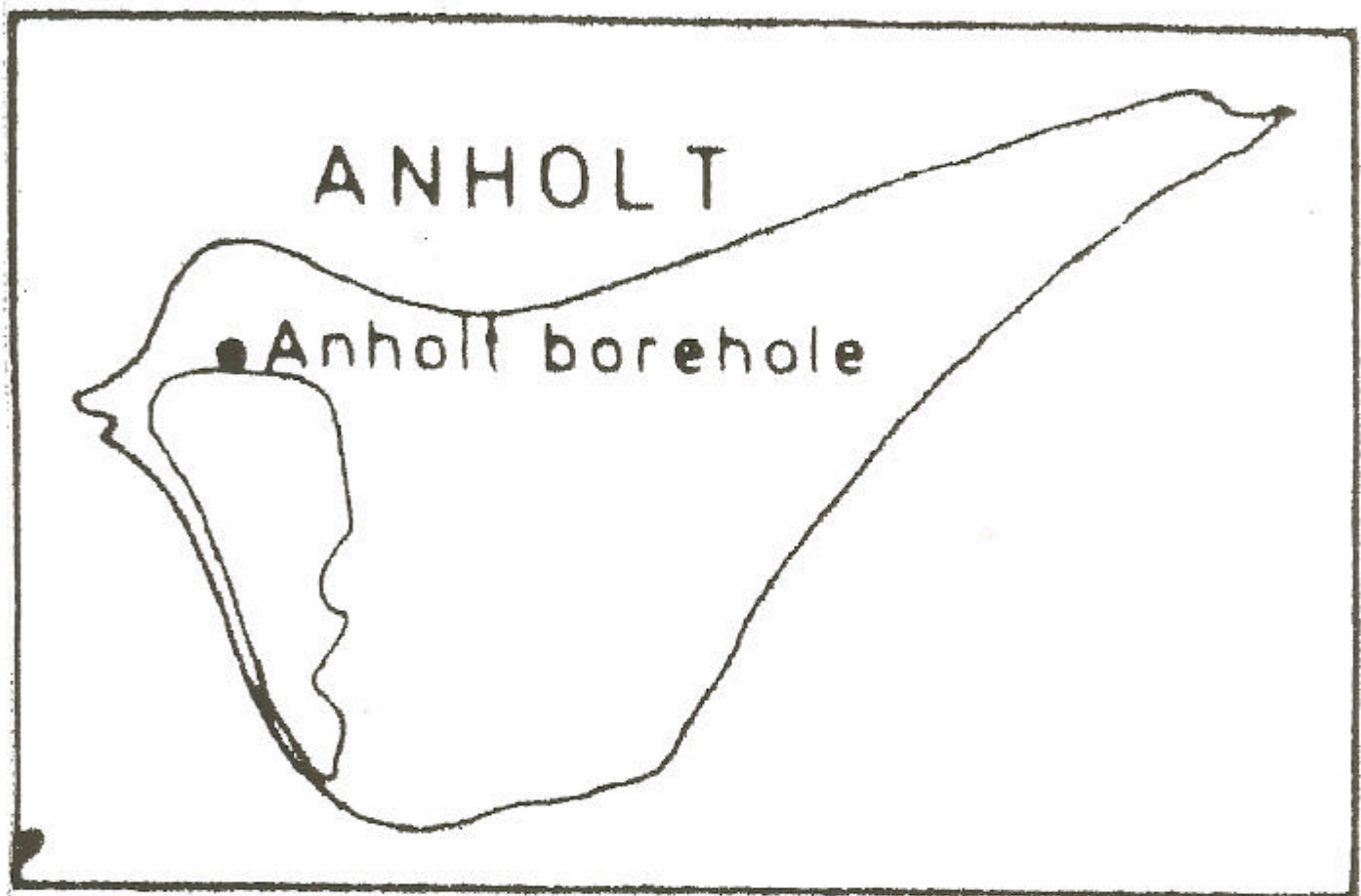
Den foreliggende sammenligning mellem resultaterne af konsolideringsforsøg med kerneprøverne af Eem-ler fra Anholt med en naturfugtig kerneprøve af Eem-ler fra Skagen og en intakt rørprøve af Eem-ler fra Nørre Lyngby viser ikke markante forskelle, der kan henføres til prøvernes kvalitet.

Forkonsolideringsspændingen for Eem-leret er fundet til $\sigma'_{pc} \sim 4000 \text{ kPa}$, og for mellem og nedre juraler til $\sigma'_{pc} \sim 6000 \text{ kPa}$.

I forsøgene med prøverne fra Jura er normalkonsolideret tilstand næppe nået. Forkonsolideringsspændingen er sandsynligvis højere end den maksimale spænding under forsøget.

9. Referencer

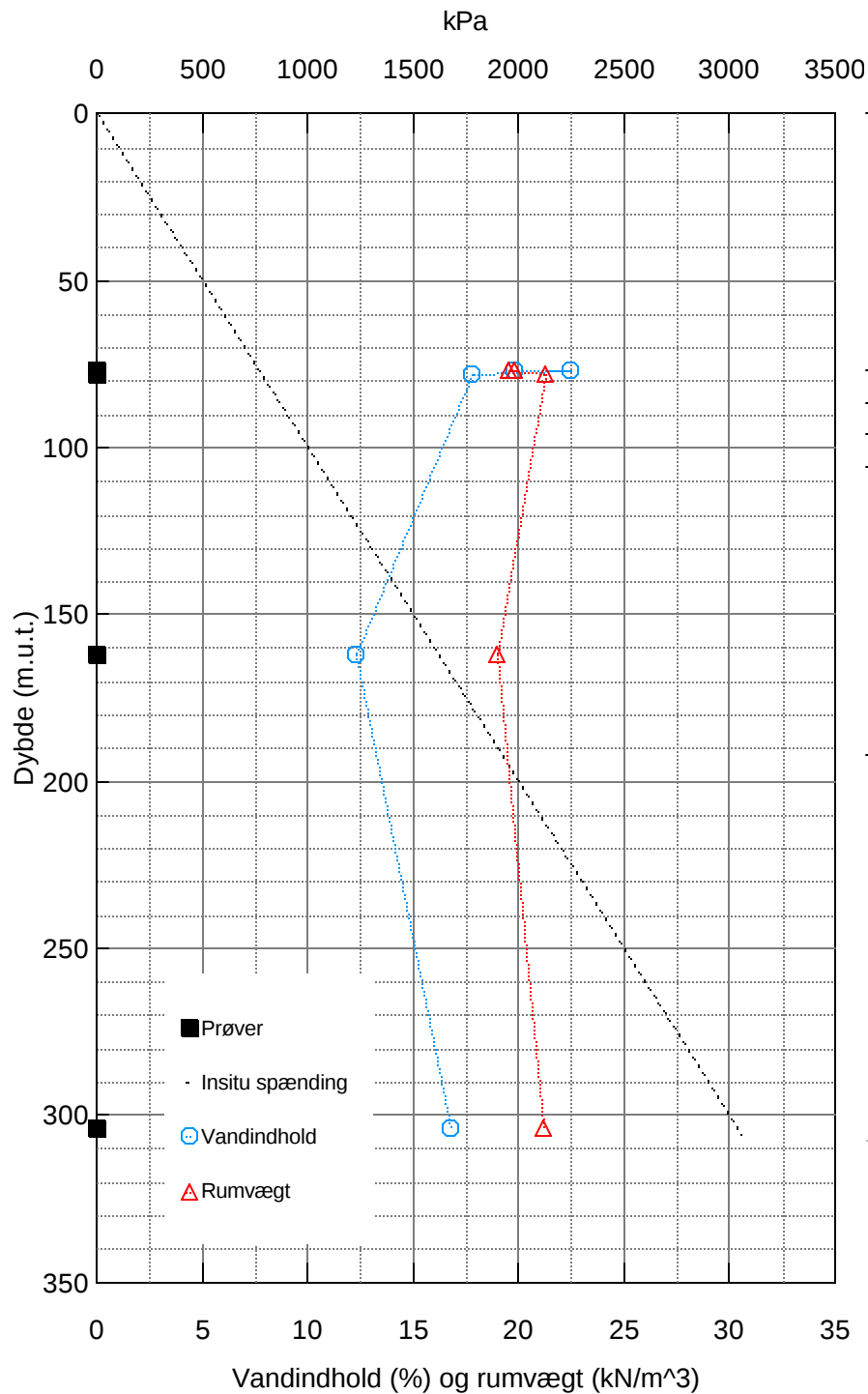
- DS415:84: *Dansk Ingeniørforenings norm for fundering*. 1984. ISBN 87-571-0765-3.
- Dgf-Bulletin 15: *Laboratoriehåndbogen, afsnit 5, konsolideringsforsøg*. Dgf's laboratoriekomité, December 2001. ISBN NO 87-89833-12-0.
- Jacobsen, H. Moust, 1992: *Bestemmelse af forbelastningstryk i laboratoriet*. Proceedings Nordisk Geoteknikermøde NGM-92, Aalborg. Danish Geotechnical Society, Bulletin 9, Vol.2, pp 455-460 ISBN 87-983058-7-5.
- Nielsen, O.B., 1992: *Lithologi, lithostratigrafi og aflejringsmiljø i Anholtboringen*. Dansk Geologisk Forening, Årsskrift for 1990-91, pp 67-72, København 1992.
- Thorsen, G. 1996: *Oedometer tests – an aid in determination of the geological load history?* Bulletin of the Geological Society of Denmark. Vol. 43 pp. 41-50. Copenhagen 1996
- Thorsen, G. 2006a: *Skagen 3. Konsolideringsforsøg. Postglacialt marint silt og ler. Senglacialt marint ler. Glacialt ler fra Weichsel og Eem*. Datarapport. AAU Geotechnical Engineering Papers. Laboratory testing paper no. R0601, ISSN 1398-6465
- Thorsen, G. 2006b: *Nørre Lyngby. Konsolideringsforsøg. Senglacialt marint ler. Glacialt ler og marint ler fra Eem*. Datarapport no.2. AAU Geotechnical Engineering Papers. Laboratory testing paper no. R0602, ISSN 1398-6465



Efter: Nielsen: Lithologi, Anholtboringen, fig.1, Geologisk Forening, Årsskrift for 1990-91. (1992)

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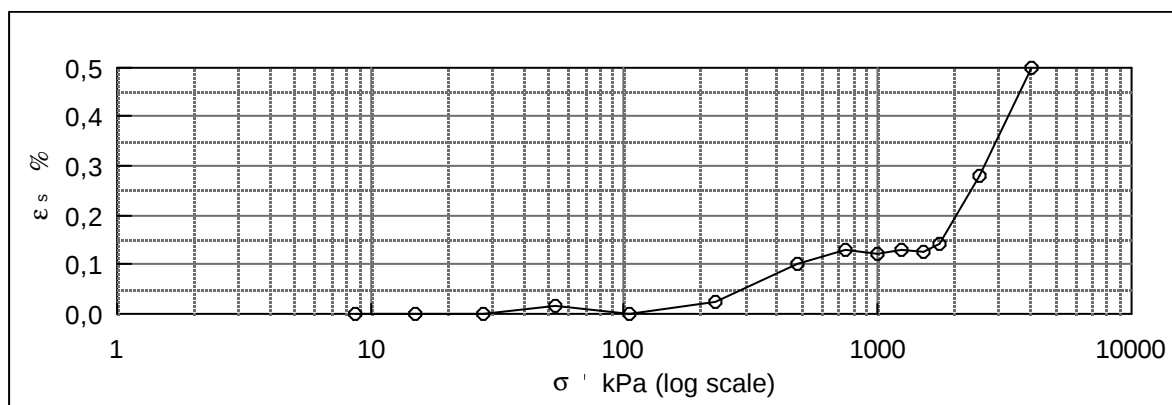
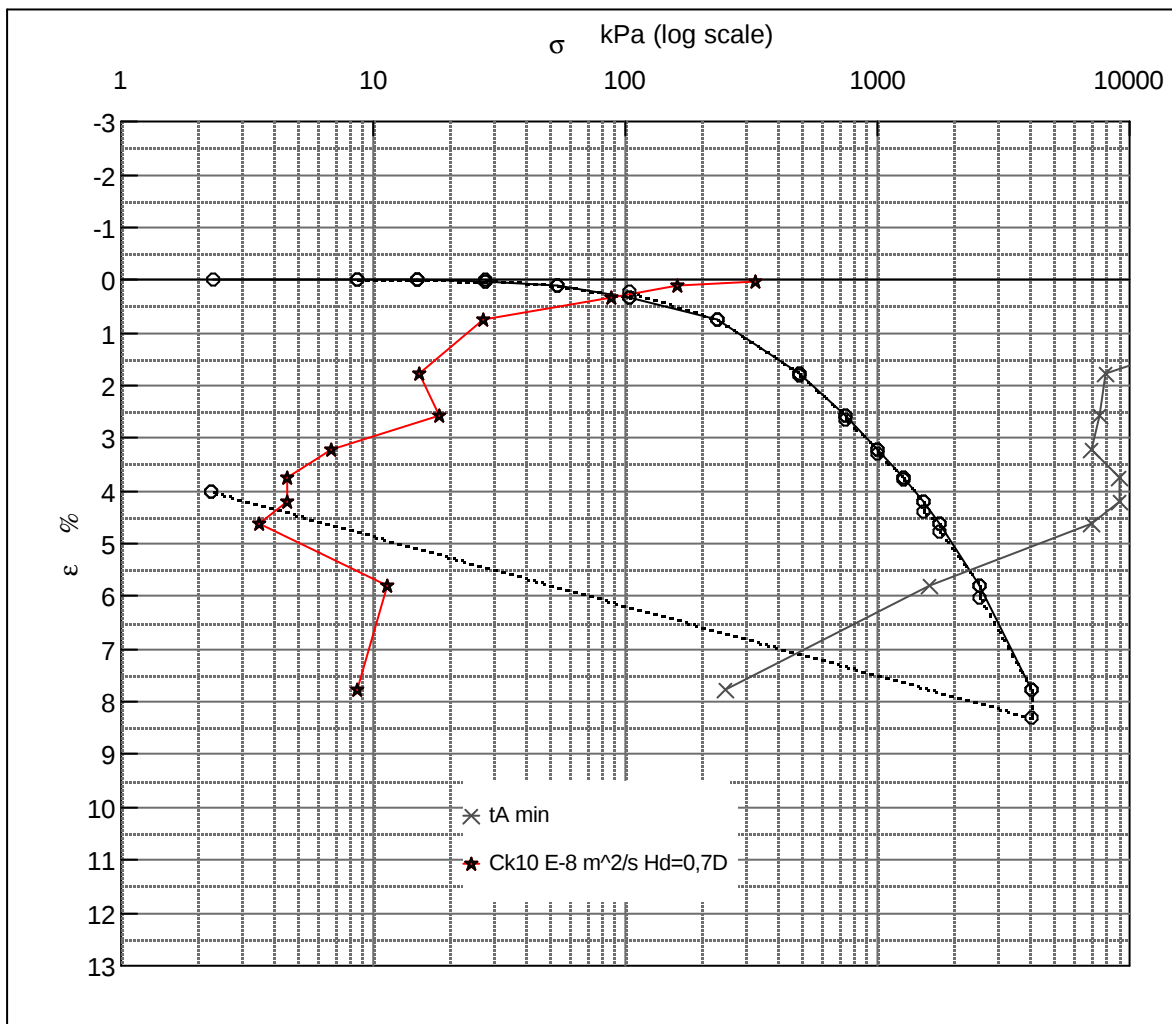
Anholtboringen
Udtagne prøver til konsolideringsforsøg
samt vandindhold og rumvægt for de udtagne prøver



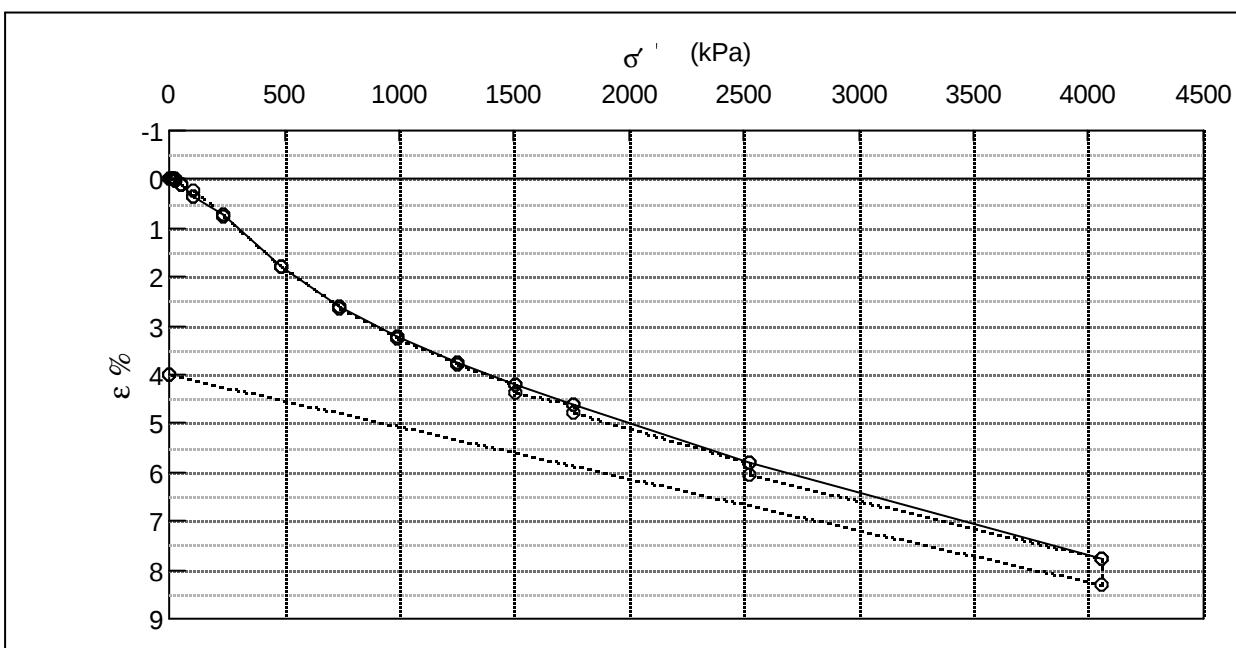
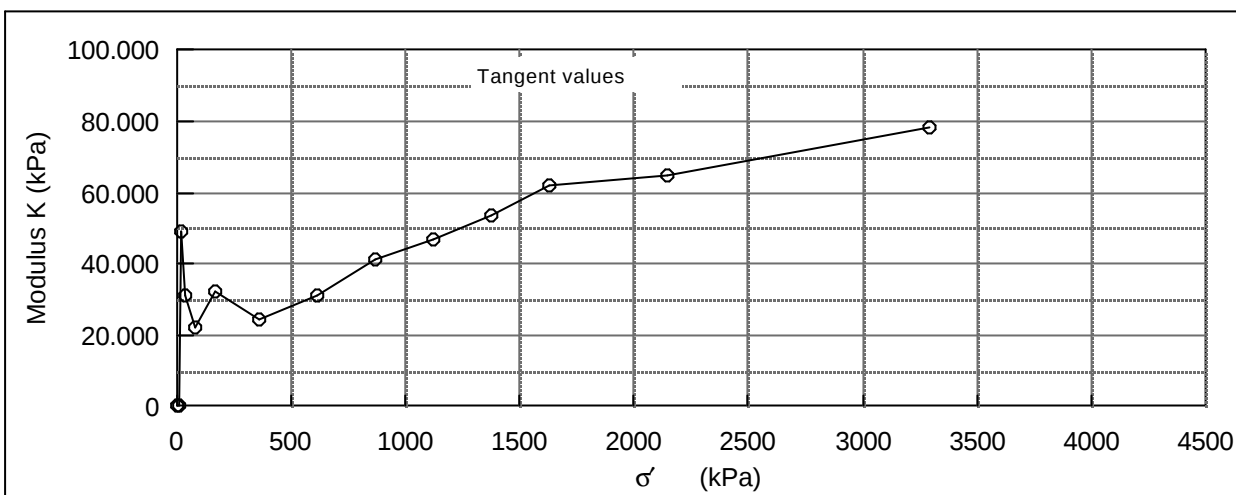
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Description of soil: Clay Eemian Glacial			Water content %	Before	After
			Bulk density Mg / m ³	~19.8	~20.2
			Grain density Mg / m ³	2,02	~2.11
			Void ratio	~2.72	~0.61
Bor no :	Overburden pressure σ'_o	~780 kPa	Degr. of Saturation %	~88	~100
Lab. no: Pr 1	Vane strength c_v	kPa	Dimension H x D mm	35x70	33.6x70
Level : 76.7 m.b.s	CPT - value q_c	MPa			



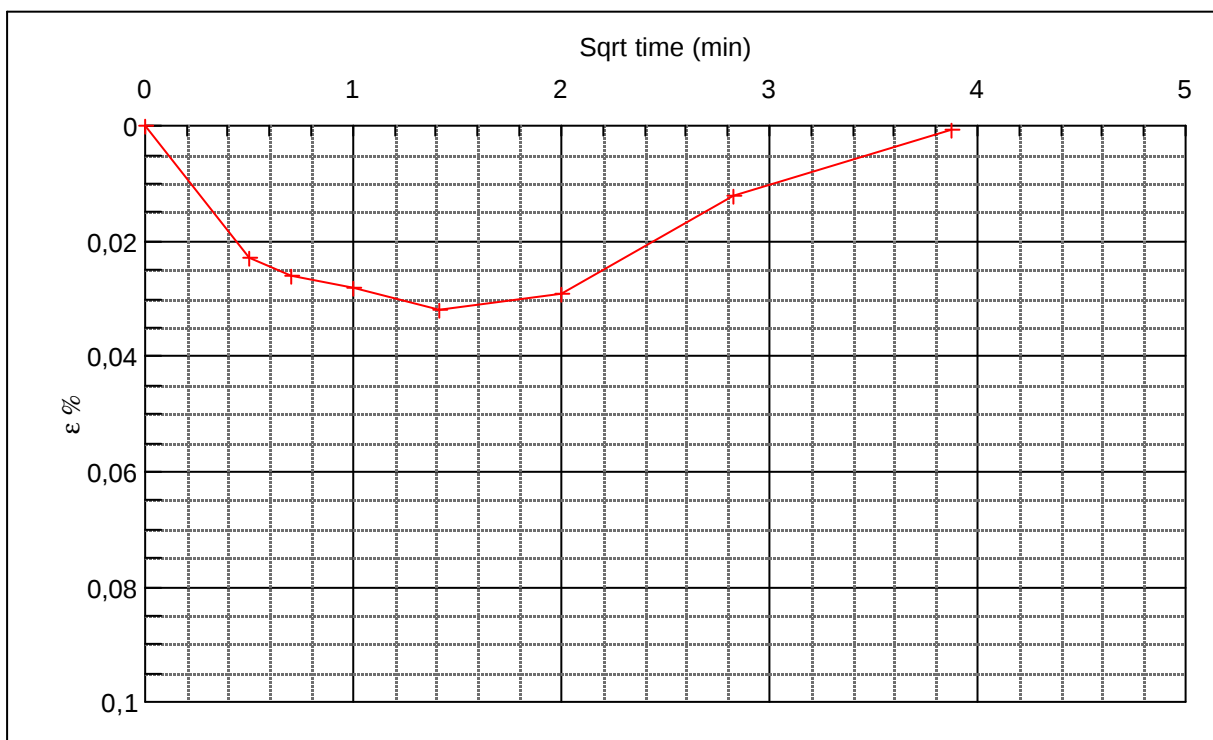
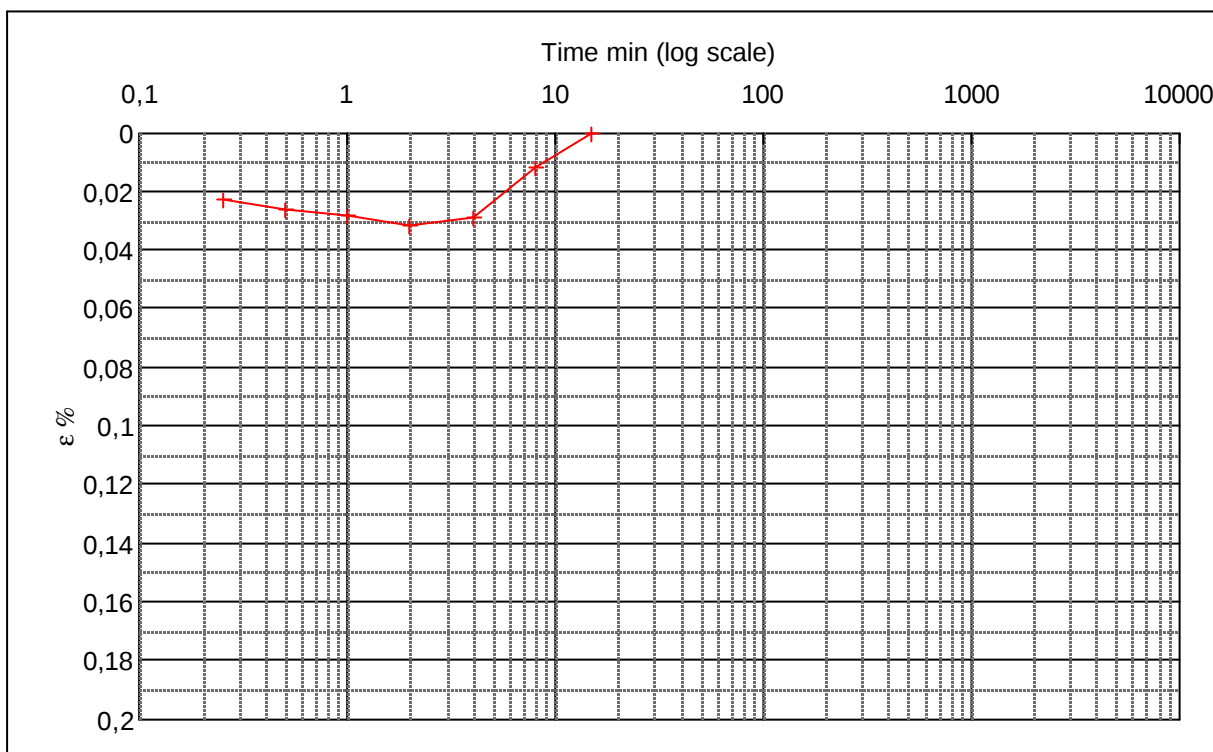
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Test results		σ' kPa	ϵ_c %	ϵ_s % / lct	Ck10 m ² /s	σ'_m kPa	K kPa	w %
Q	9,5 % ?	2,3	0,00	-	-	-	-	22,6
Qs	~0.5 %	8,7	0,00	0,00	0	5,5		22,6
σ'_{pc}	>2500 kPa	15,0	0,00	0,00	0	11,9		22,6
		27,8	0,03	0,00	3,3E-06	21,4	49020,7	22,6
		53,3	0,11	0,02	1,6E-06	40,5	31086,3	22,5
		104,3	0,34	0,00	8,8E-07	78,8	21974,8	22,4
		231,7	0,74	0,03	2,7E-07	168,0	32266,8	22,2
		486,6	1,77	0,10	1,5E-07	359,2	24557,6	21,5
		741,5	2,59	0,13	1,8E-07	614,1	31200,5	21,1
		996,4	3,20	0,12	6,8E-08	869,0	41515,9	20,7
		1.251,3	3,75	0,13	4,5E-08	1.123,9	46944,3	20,4
		1.506,2	4,22	0,13	4,5E-08	1.378,8	53891,7	20,1
		1.761,2	4,63	0,14	3,5E-08	1.633,7	62172,6	19,9
		2.525,9	5,81	0,28	1,1E-07	2.143,5	64862,0	19,2
		4.055,3	7,76	0,50	8,6E-08	3.290,6	78473,4	18,0
		2,3	4,00	0,00	0	2.028,8	107850,8	20,2

Remark: "Genbelastningsgren" Normalkonsolideret tilstand næppe nået		Job: Anholt		AAU
				Encl. No 2.2
		Executed:	AMS/mj/gt	Check:
		Approved:		

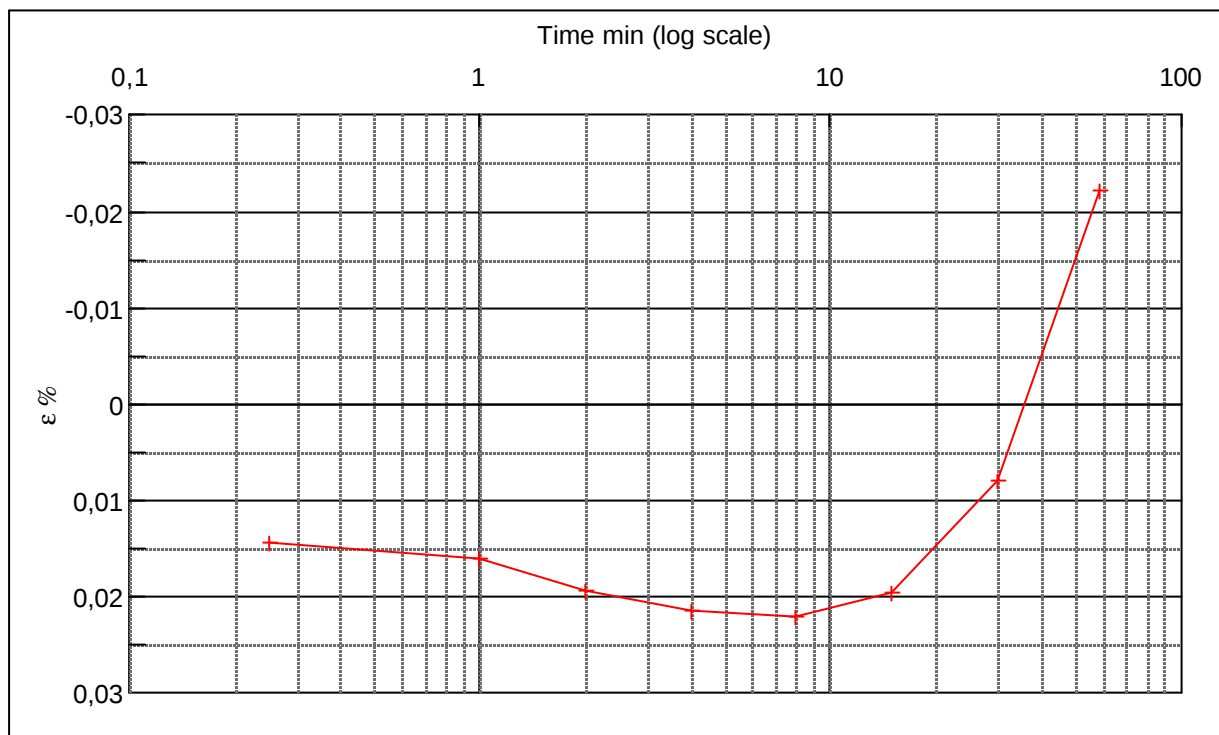
Step no	σ	kPa	ϵ	%	ϵ_i	tc in sec
1	Before	2,29	ϵ_0	0,00	ϵ_c %	K i kPa
	After	8,67	$\epsilon_{-#}$	0,001	ϵ_s	k10 m/sec
					ϵ_{kyb}	ck10 m^2 /sec



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.3
Executed:	AMS/mj/gt	Check:
Approved:		

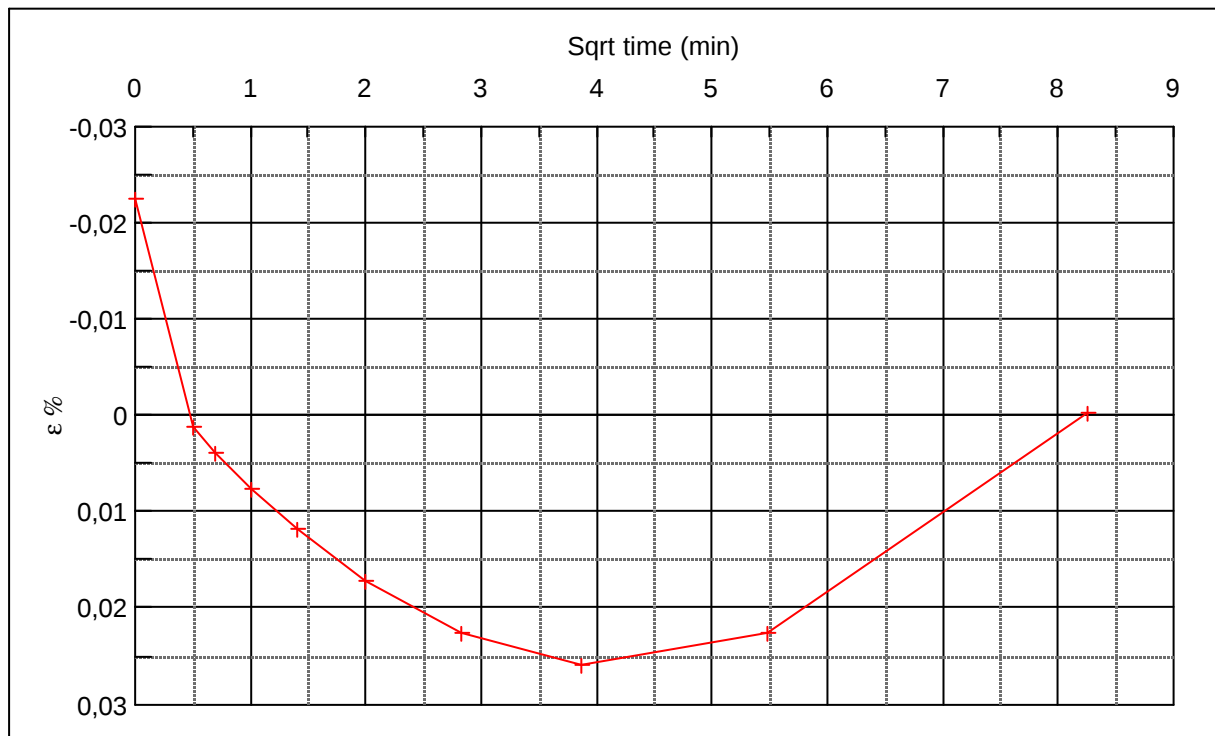
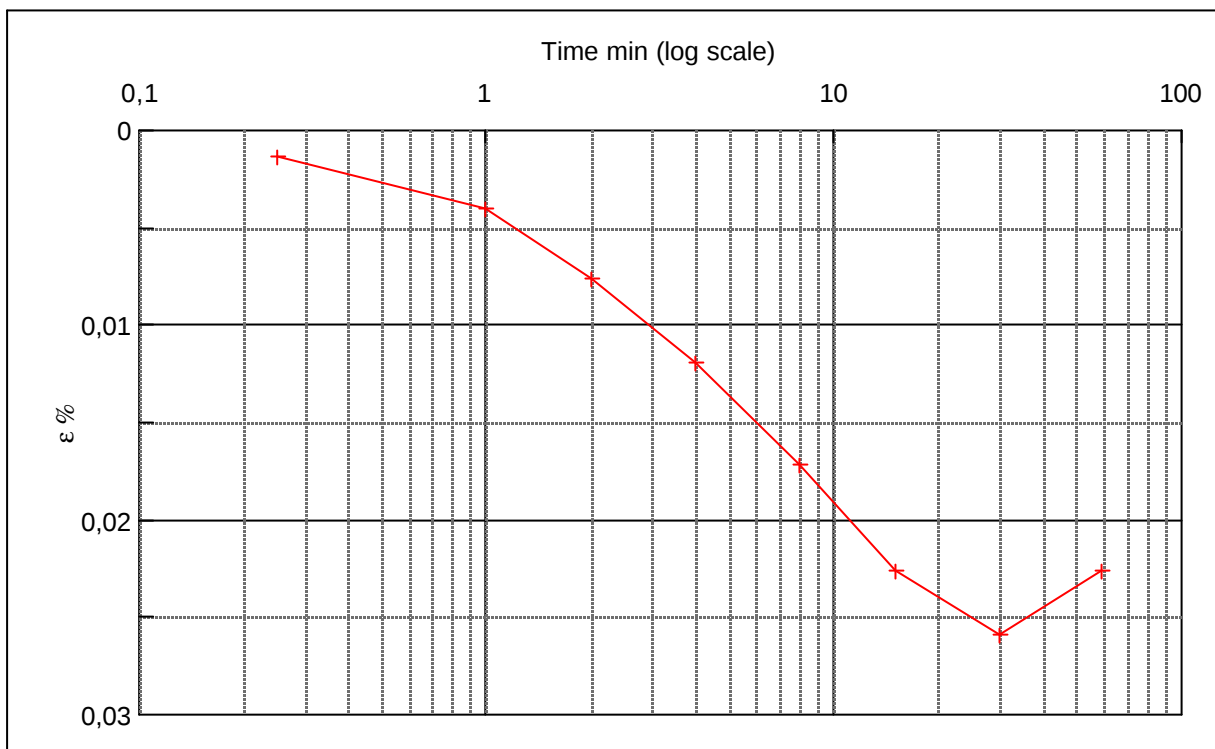
Step no 2	σ	kPa	ϵ	%	ϵ_i	tc in sec	
	Before	8,7	ϵ_0	0,001	ϵ_c %	K i kPa	
	After	15,0	$\epsilon_{-#}$	(0,022)	ϵ_s	k10 m/sec	
					ϵ_{kryb}	ck10 m ² /sec	



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.4
Executed:	AMS/mj/gt	Check:
Approved:		

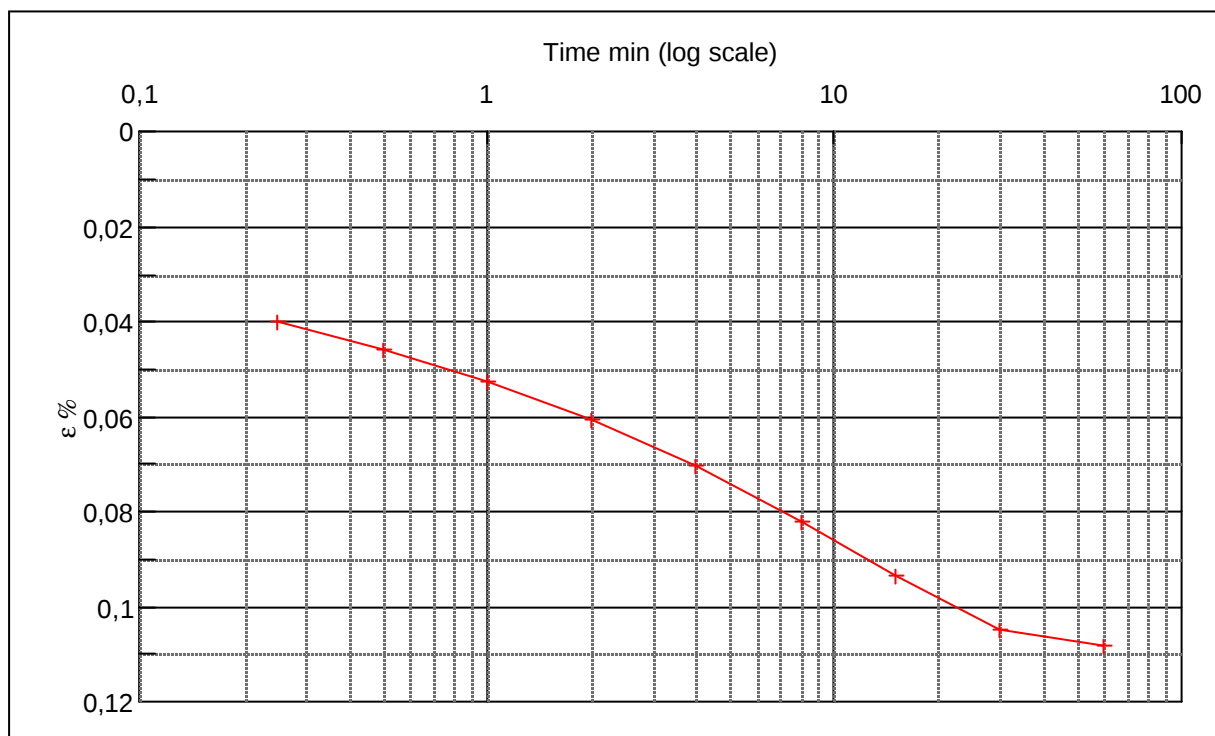
Step no 3	σ	kPa	ϵ	%	ϵ_i		tc in sec	405,6
	Before	15,0	ϵ_0	(0,022)	ϵ_c	% 0,026	K i kPa	26.318
	After	27,8	$\epsilon_{-#}$	0,000	ϵ_s		k10 m/sec	1,2E-09
					ϵ_{kryb}		ck10 m ² /sec	3,25E-06



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.5
Executed:	AMS/mj/gt	Check:
Approved:		

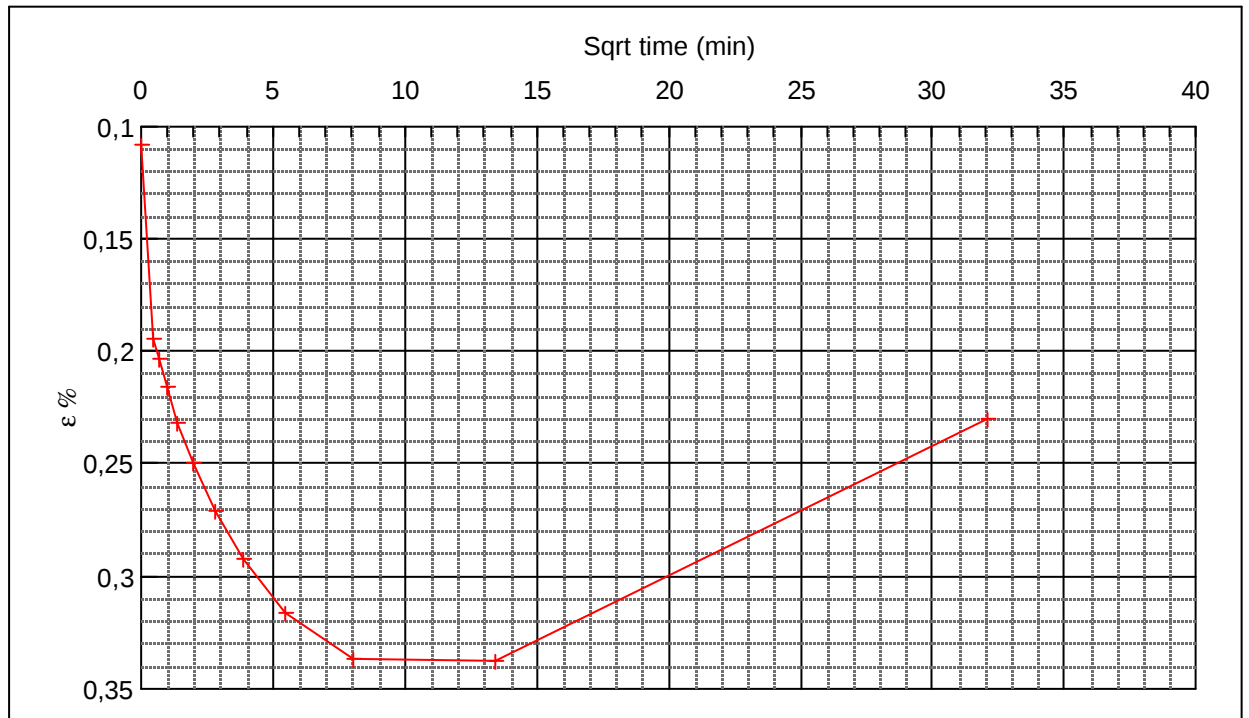
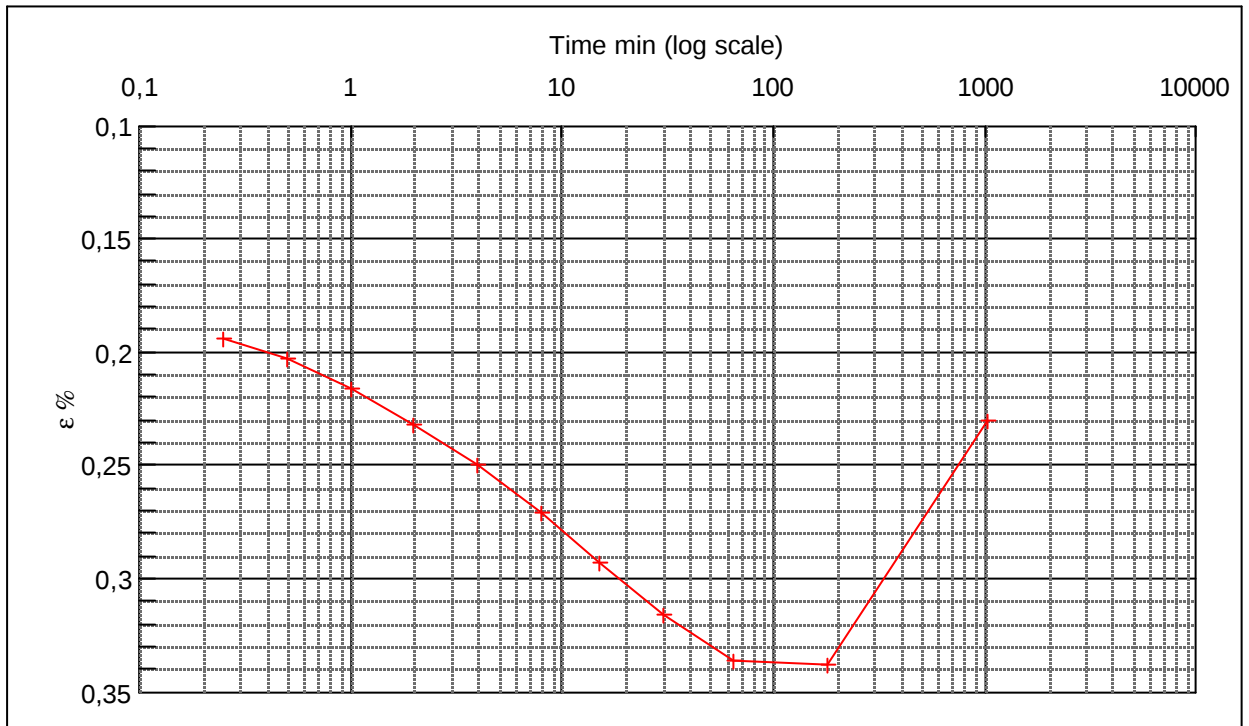
Step no 4	σ	kPa	ϵ	%	ϵ_i		tc in sec	821,4
	Before	27,8	ϵ_0	(0,00)	ϵ_c %	0,11	K i kPa	23.540
	After	53,3	$\epsilon_{-#}$	0,11	ϵ_s	0,02	k10 m/sec	6,7E-10
					ϵ_{kryb}	0,00	ck10 m ² /sec	1,61E-06



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.6
Executed:	AMS/mj/gt	Check:
Approved:		

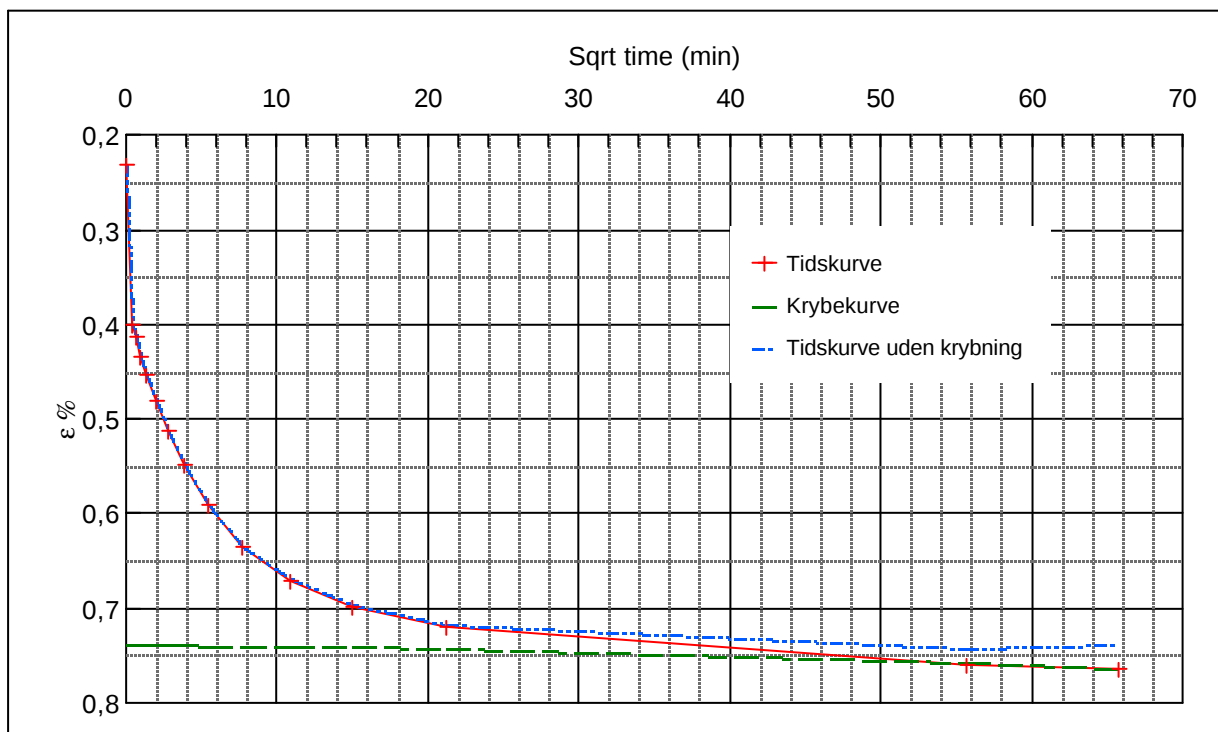
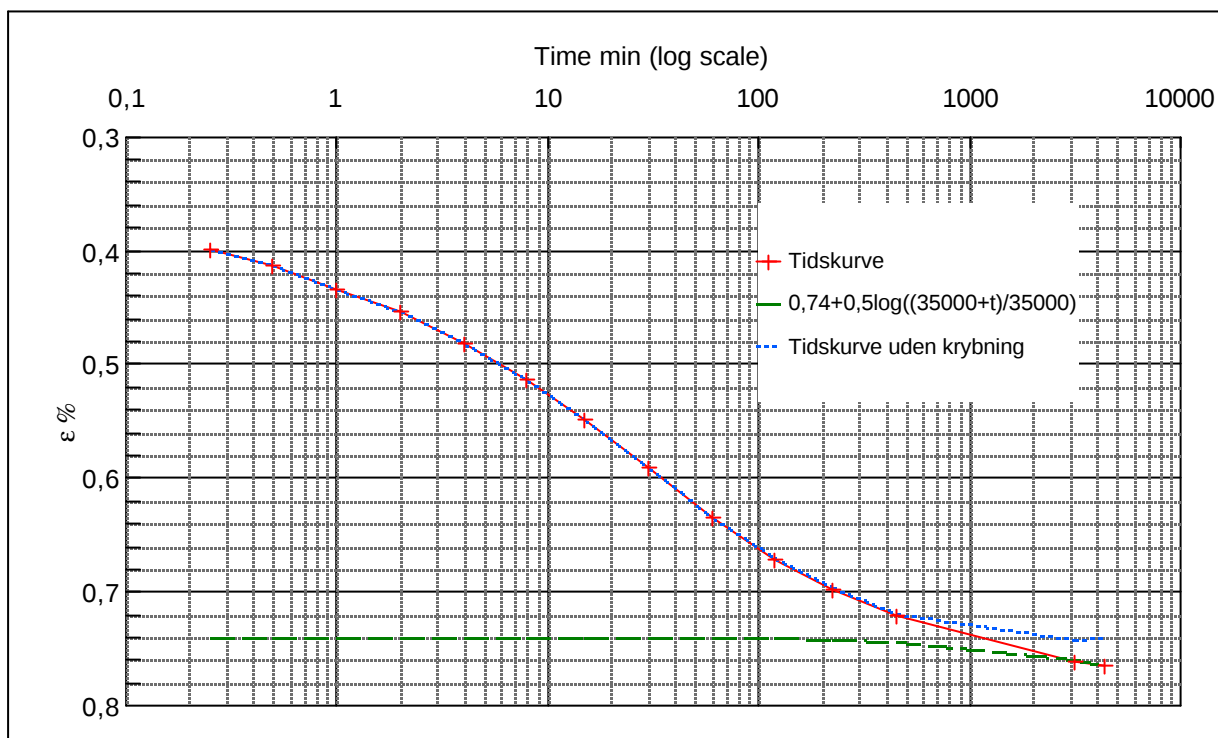
Step no 5	σ	kPa	ϵ	%	ϵ_i		tc in sec	1500
	Before	53,3	ϵ_0	0,11	ϵ_c %	0,34	K i kPa	22.002
	After	104,3	$\epsilon_{\sim\#}$	0,23	ϵ_s		k10 m/sec	3,9E-10
					ϵ_{kyb}	-0,11	ck10 m^2 /sec	8,80E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 2.7
Executed:	AMS/mj/gt	Check:
Approved:		

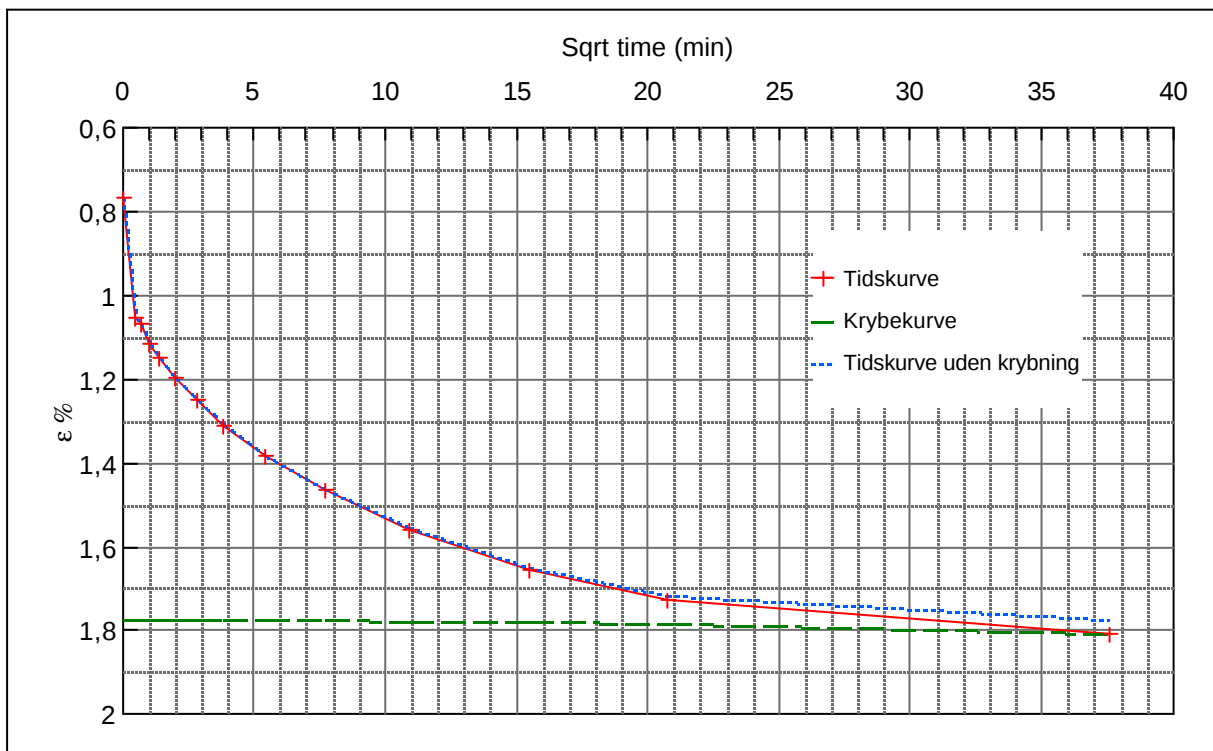
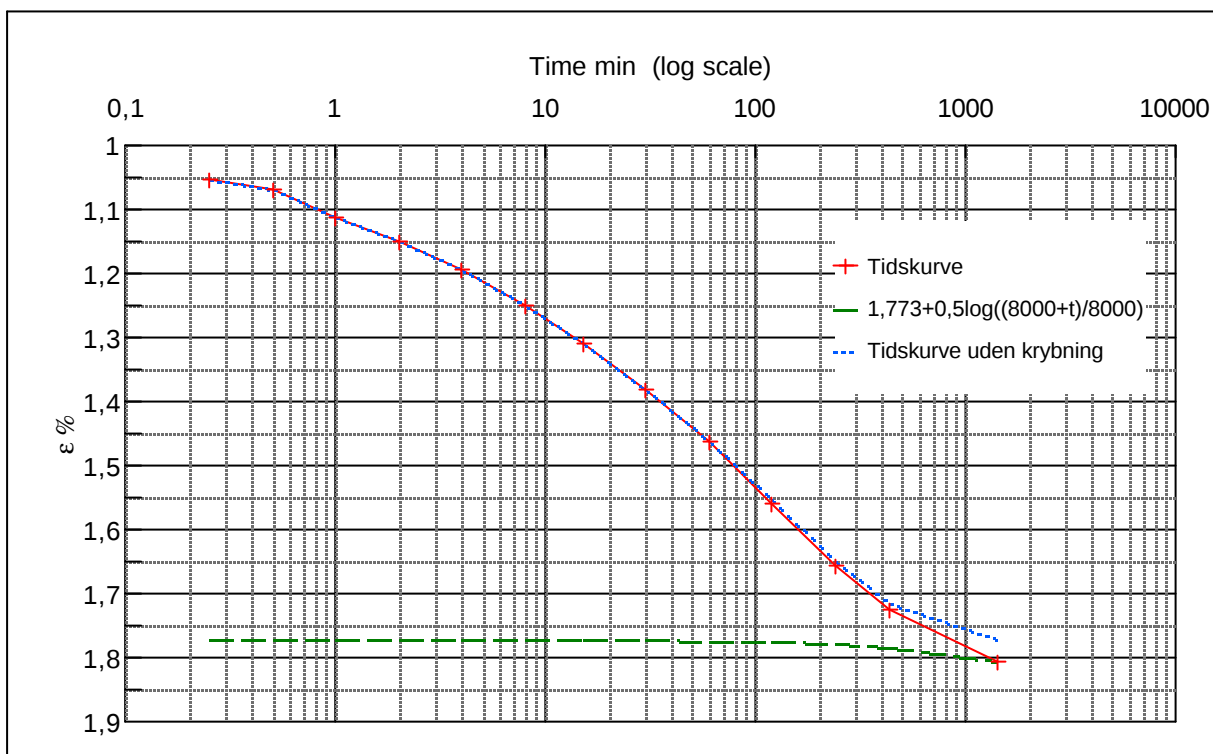
Step no 6	σ	kPa	ϵ	%	ϵ_i		tc in sec	4860
	Before	104,3	ϵ_0	0,23	ϵ_c %	0,74	K i kPa	25.238
	After	231,7	$\epsilon_{-#}$	0,77	ϵ_s	0,03	k10 m/sec	1,1E-10
					ϵ_{kryb}	0,03	ck10 m ² /sec	2,7E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.8
Executed:	AMS/mj/gt	Check:
Approved:		

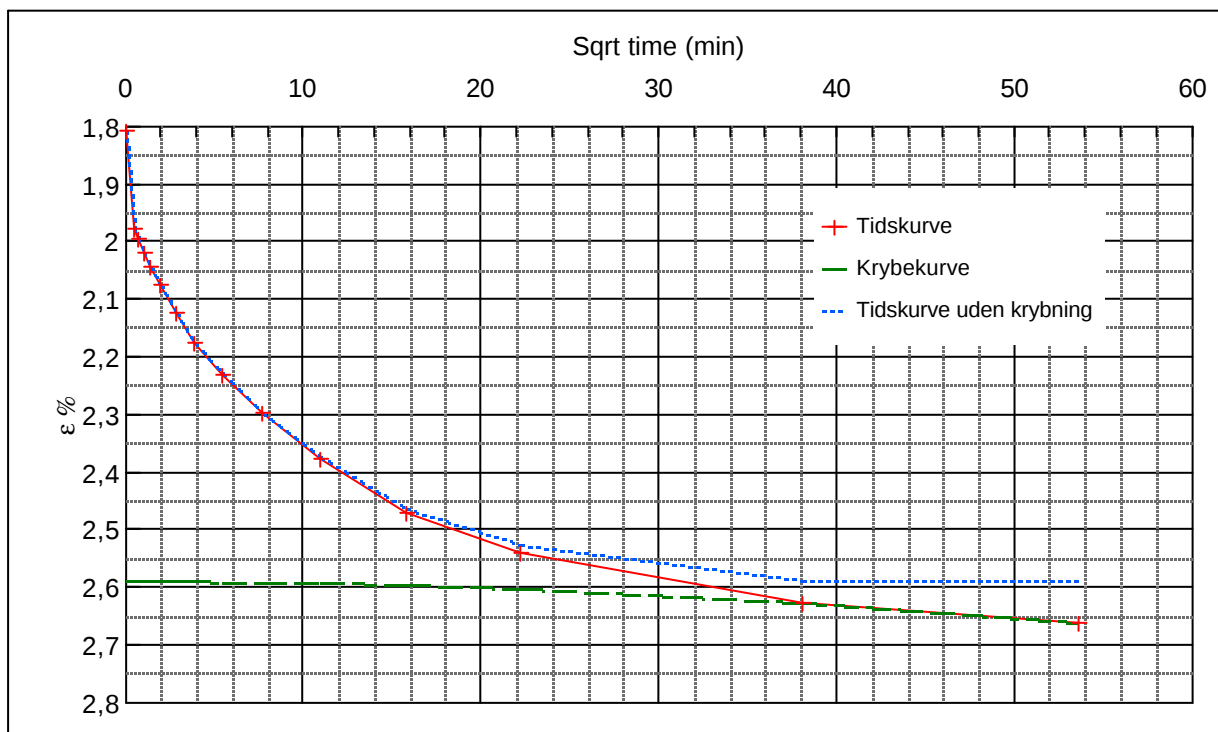
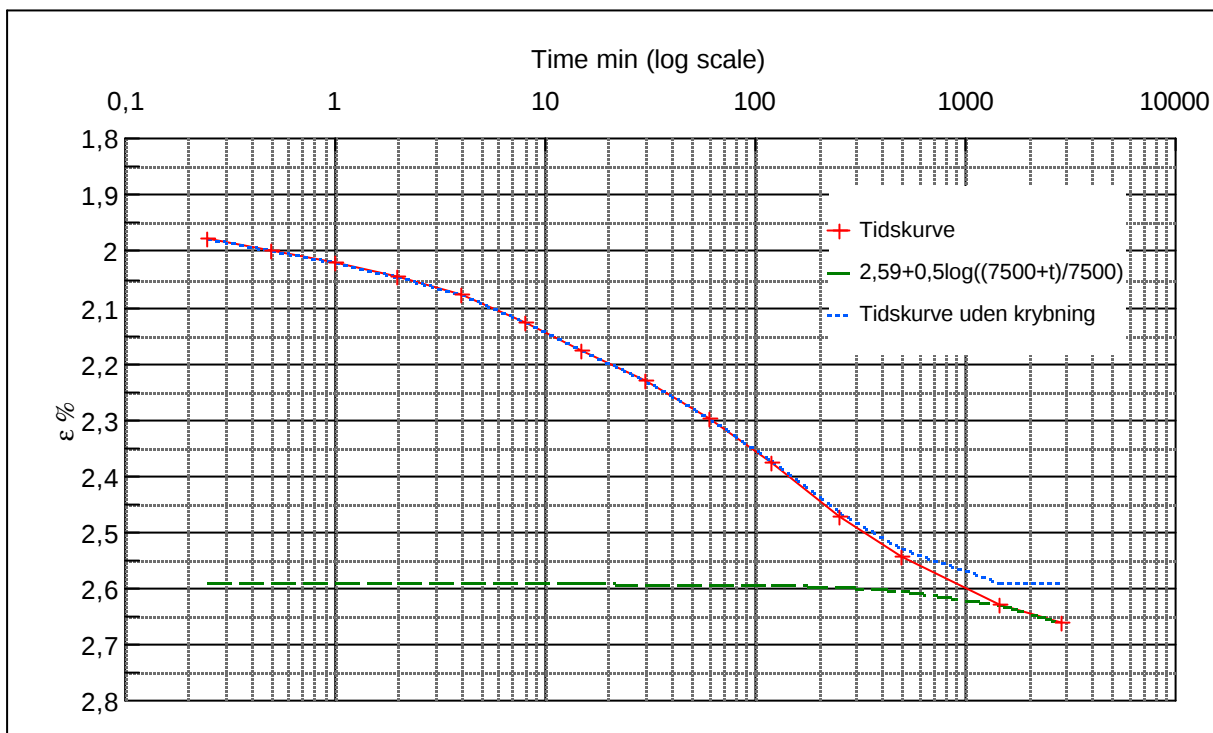
Step no 7	σ	kPa	ϵ	%	ϵ_i		tc in sec	8640
	Before	231,7	ϵ_0	0,77	ϵ_c %	1,77	K i kPa	25.288
	After	486,6	$\epsilon_{\sim\#}$	1,81	ϵ_s	0,1	k10 m/sec	5,9E-11
					ϵ_{kryb}	0,03	ck10 m^2/sec	1,53E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.9
Executed:	AMS/mj/gt	Check:
Approved:		

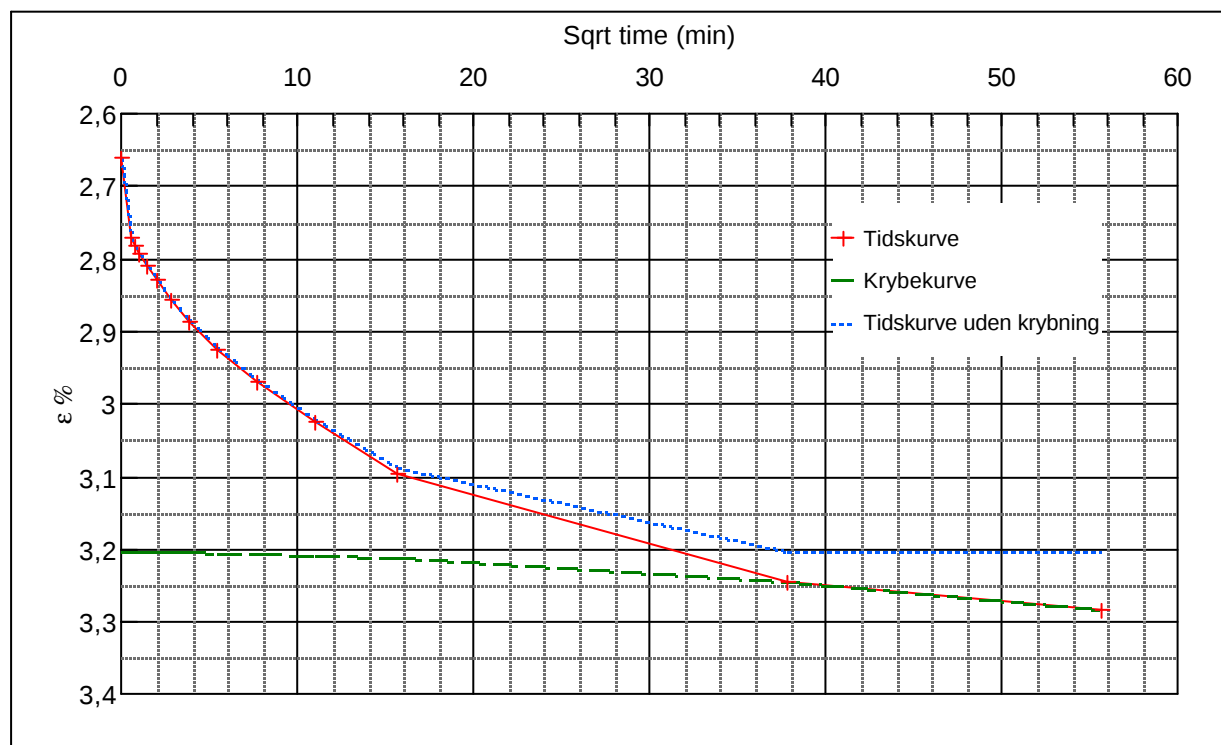
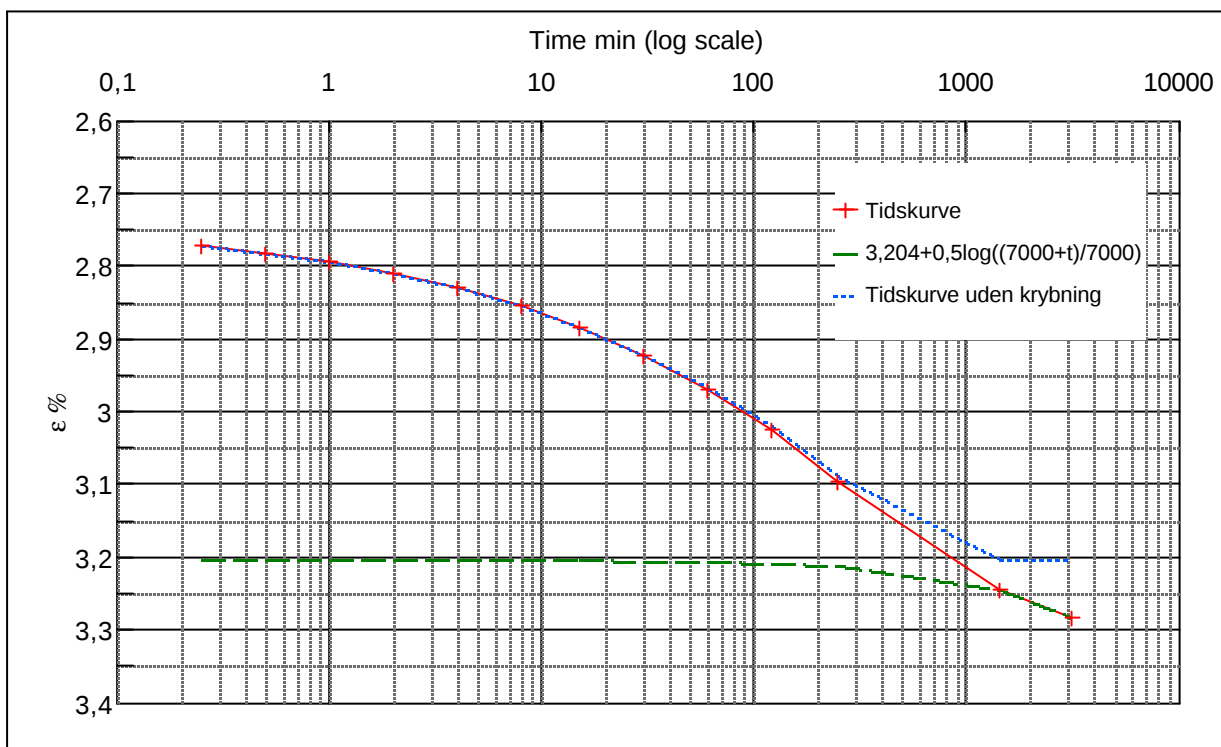
Step no 8	σ	kPa	ϵ	%	ϵ_i		tc in sec	7260
	Before	486,6	ϵ_0	1,81	ϵ_c %	2,59	K i kPa	32.585
	After	741,5	$\epsilon_{-#}$	2,66	ϵ_s	0,13	k10 m/sec	5,5E-11
					ϵ_{kryb}	0,07	ck10 m ² /sec	1,82E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.10
Executed:	AMS/mj/gt	Check:
Approved:		

Step no 9	σ	kPa	ϵ	%	ϵ_i		tc in sec	19440
	Before	741,5	ϵ_0	2,66	ϵ_c %	3,20	K i kPa	46.932
	After	996,4	$\epsilon_{\sim\#}$	3,28	ϵ_s	0,12	k10 m/sec	1,4E-11
					ϵ_{kryb}	0,08	ck10 m ² /sec	6,79E-08



Material:
Clay Eemian Glacial

Bor no :
Lab. no: Pr 1

Depth: 76.7 m.b.s
Insitu stress. ~780 kPa

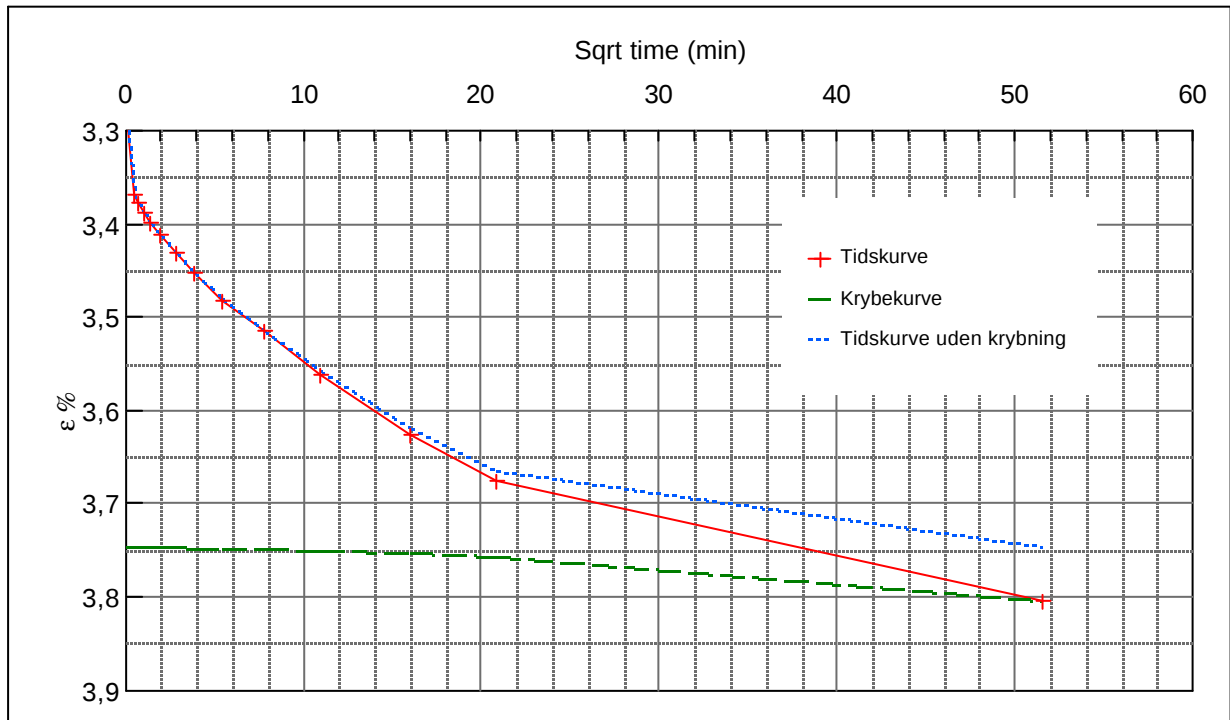
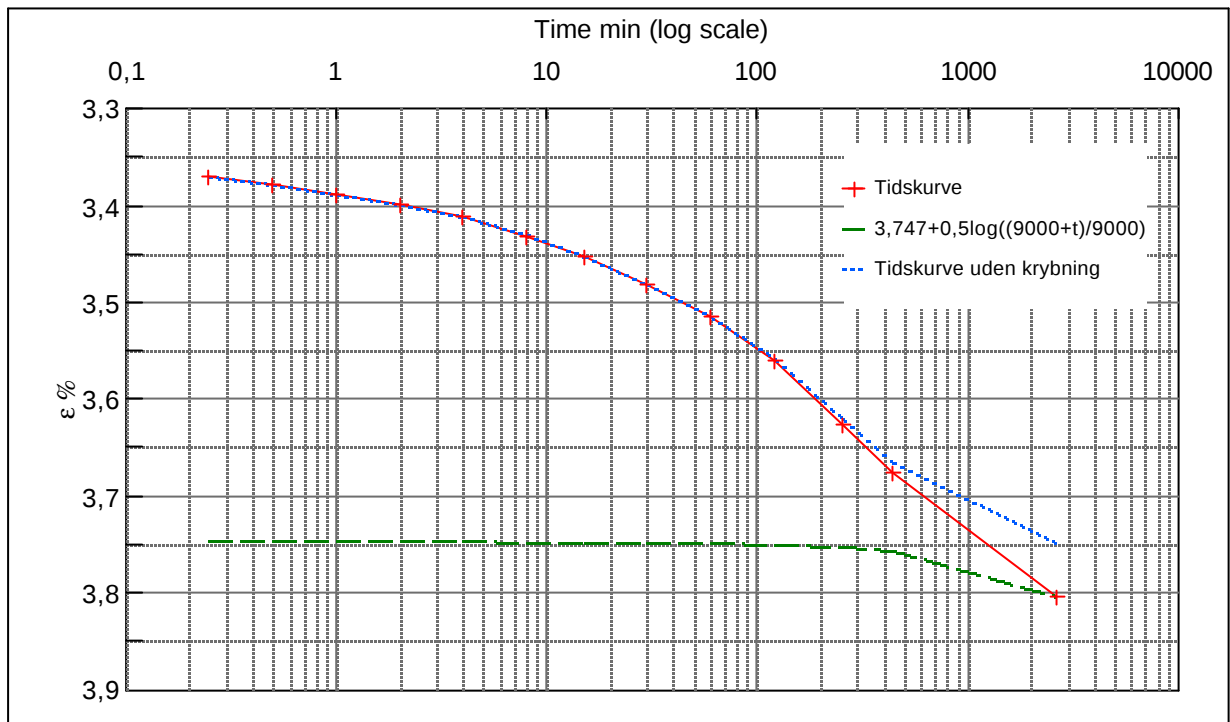
Job: Anholt

Executed: AMS/mj/gt

Approved:

AAU
Encl. No
2.11
Check:

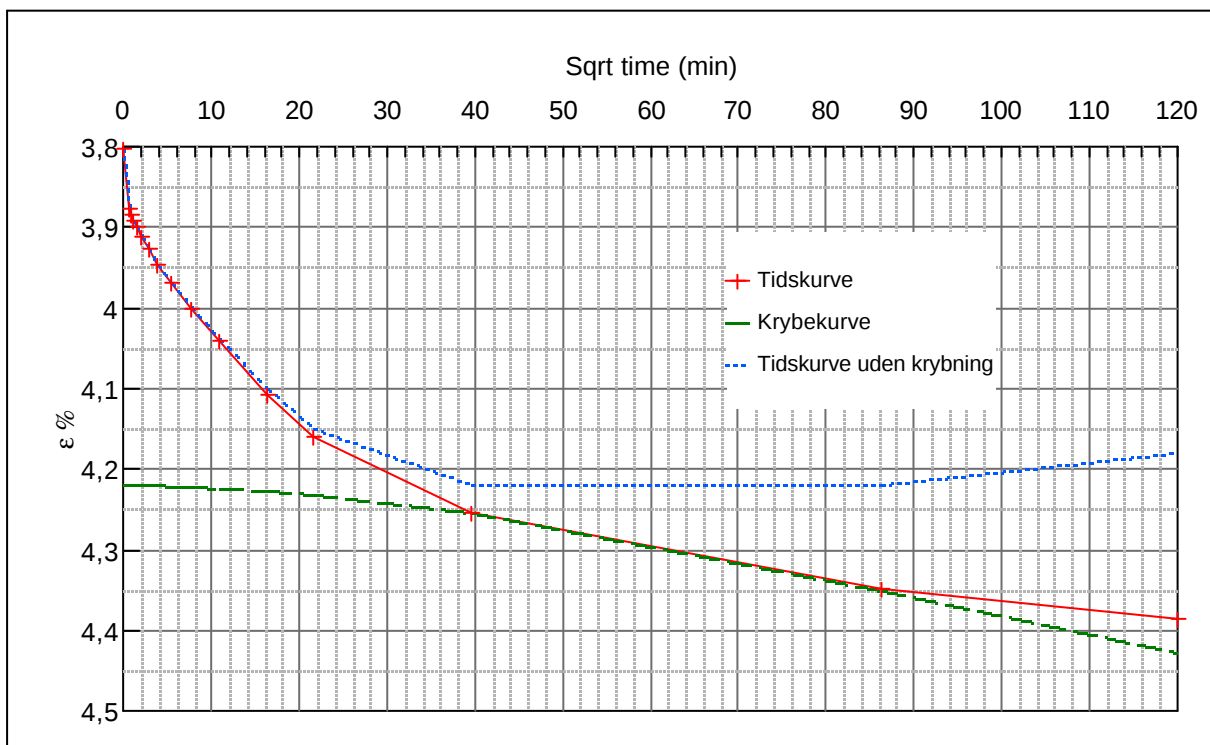
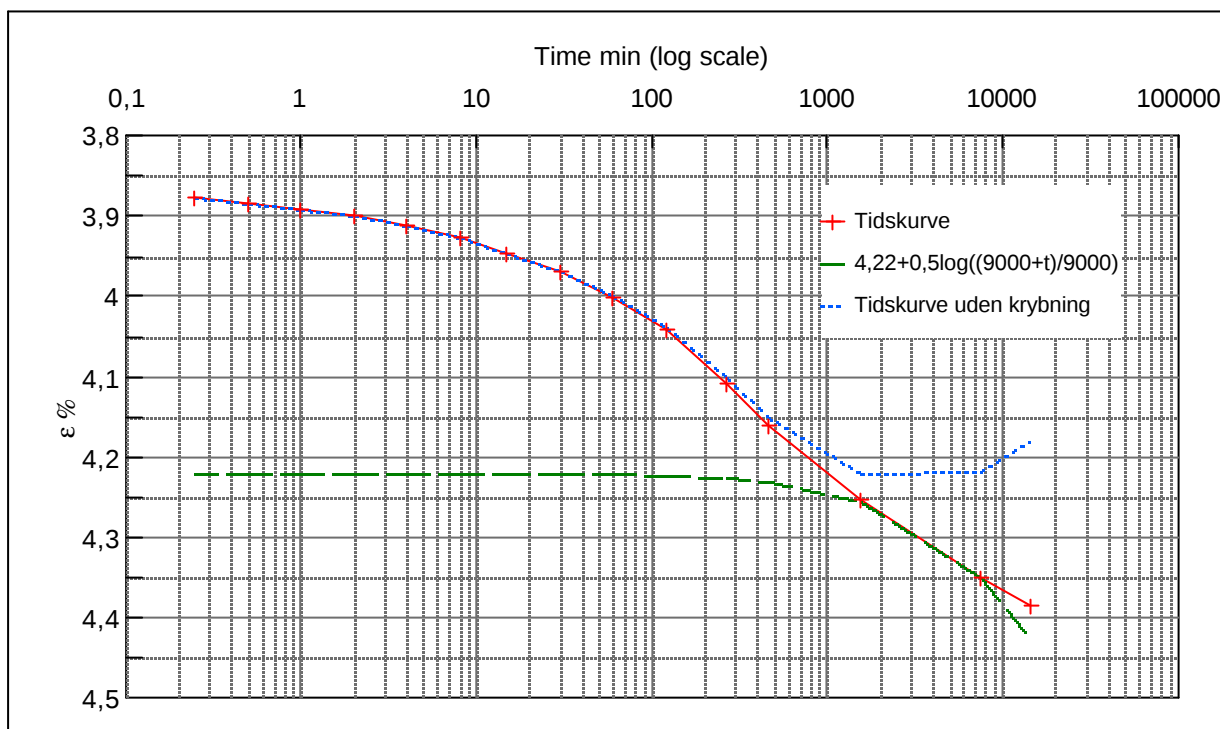
Step no 10	σ	kPa	ϵ	%	ϵ_i		tc in sec	29040
	Before	996,4	ϵ_0	3,28	ϵ_c %	3,75	K i kPa	55.056
	After	1.251,3	$\epsilon_{\sim\#}$	3,80	ϵ_s	0,13	k10 m/sec	8,10E-12
					ϵ_{kryb}	0,06	ck10 m ² /sec	4,55E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 2.12
Executed:	AMS/mj/gt	Check:
Approved:		

Step no 11	σ	kPa	ϵ	%	ϵ_i		tc in sec	29040
	Before	1.251,3	ϵ_0	3,80	ϵ_c %	4,22	K i kPa	61.192
	After	1.506,2	$\epsilon_{-#}$	4,39	ϵ_s	0,13	k10 m/sec	7,3E-12
					ϵ_{kryb}	0,17	ck10 m^2/sec	4,55E-08



Material:
Clay Eemian Glacial

Bor no :
Lab. no: Pr 1

Depth: 76.7 m.b.s
Insitu stress. ~780 kPa

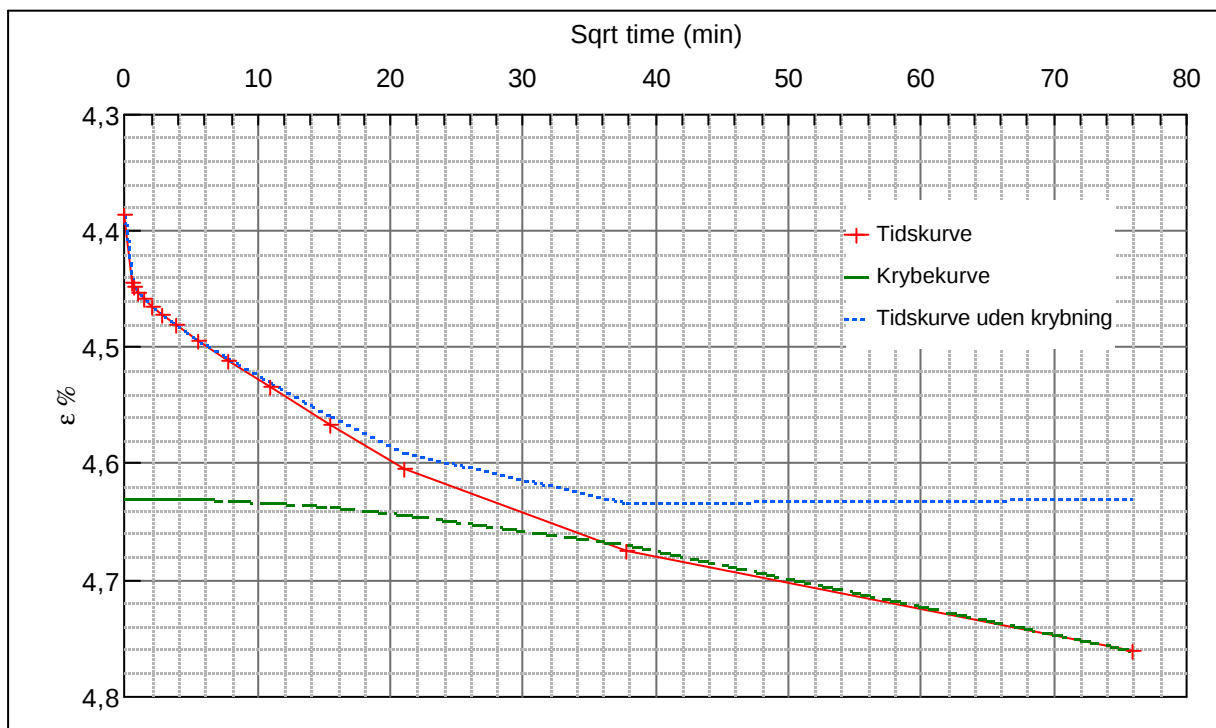
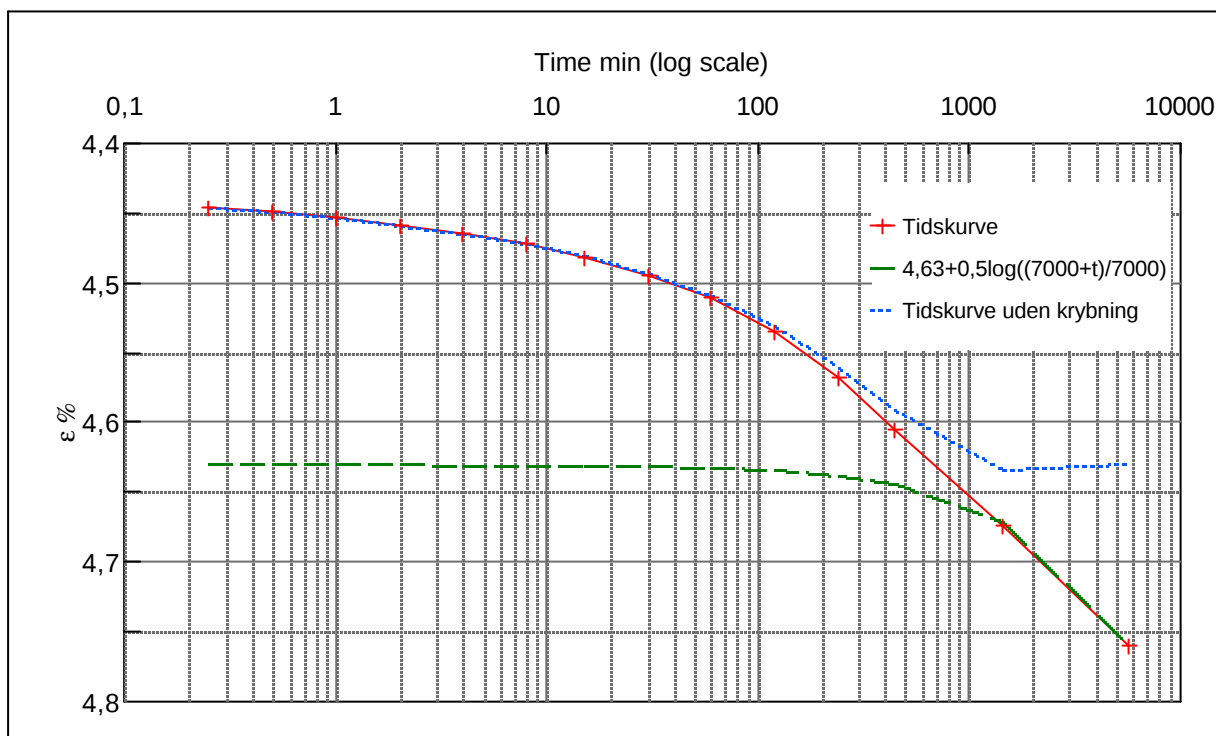
Job: Anholt

Executed: AMS/mj/gt

Approved:

AAU
Encl. No 2.13
Check:

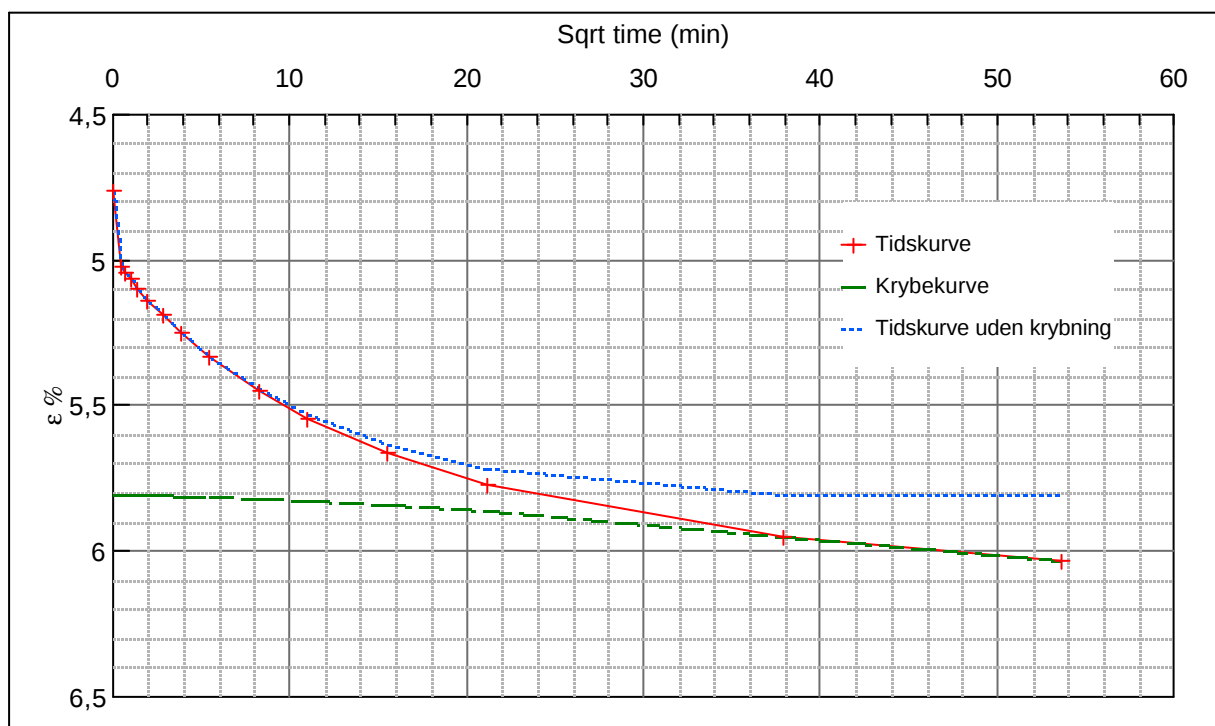
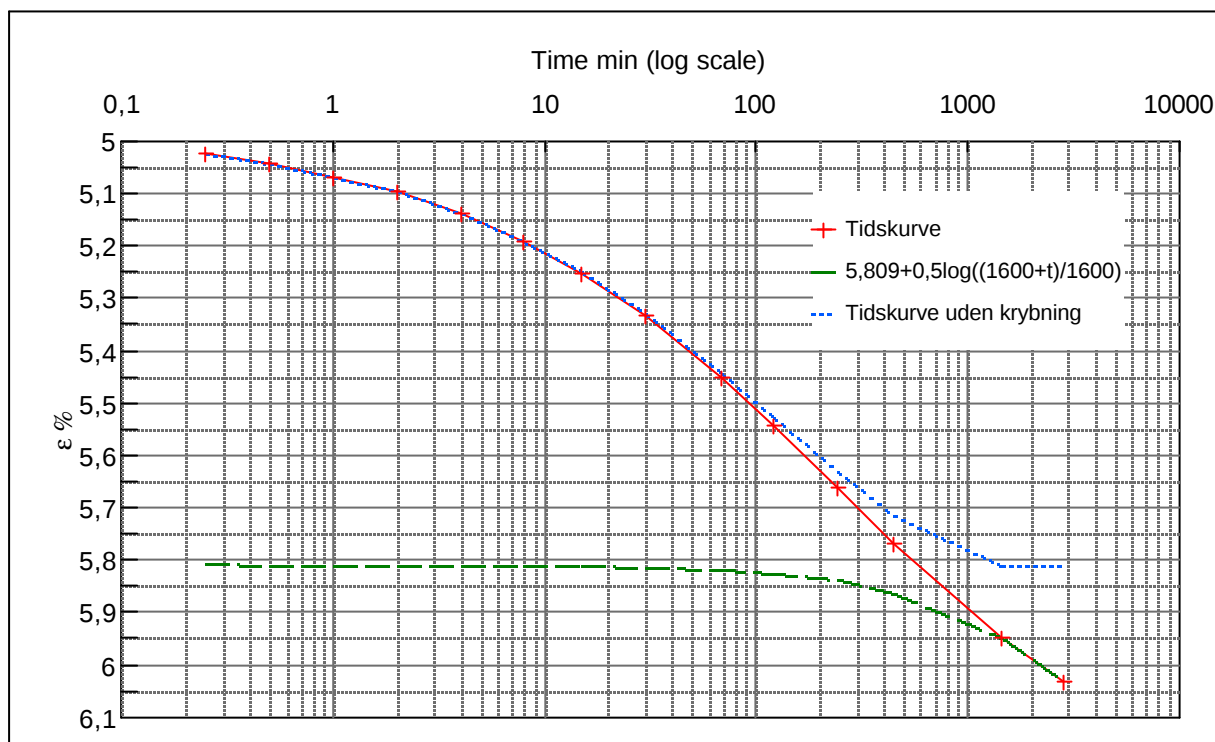
Step no 12	σ	kPa	ϵ	%	ϵ_i		tc in sec	37500
	Before	1.506,2	ϵ_0	4,39	ϵ_c %	4,63	K i kPa	104.348
	After	1.761,2	$\epsilon_{-#}$	4,76	ϵ_s	0,14	k10 m/sec	3,3E-12
					ϵ_{kryb}	0,13	ck10 m ² /sec	3,52E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.14
Executed:	AMS/mj/gt	Check:
Approved:		

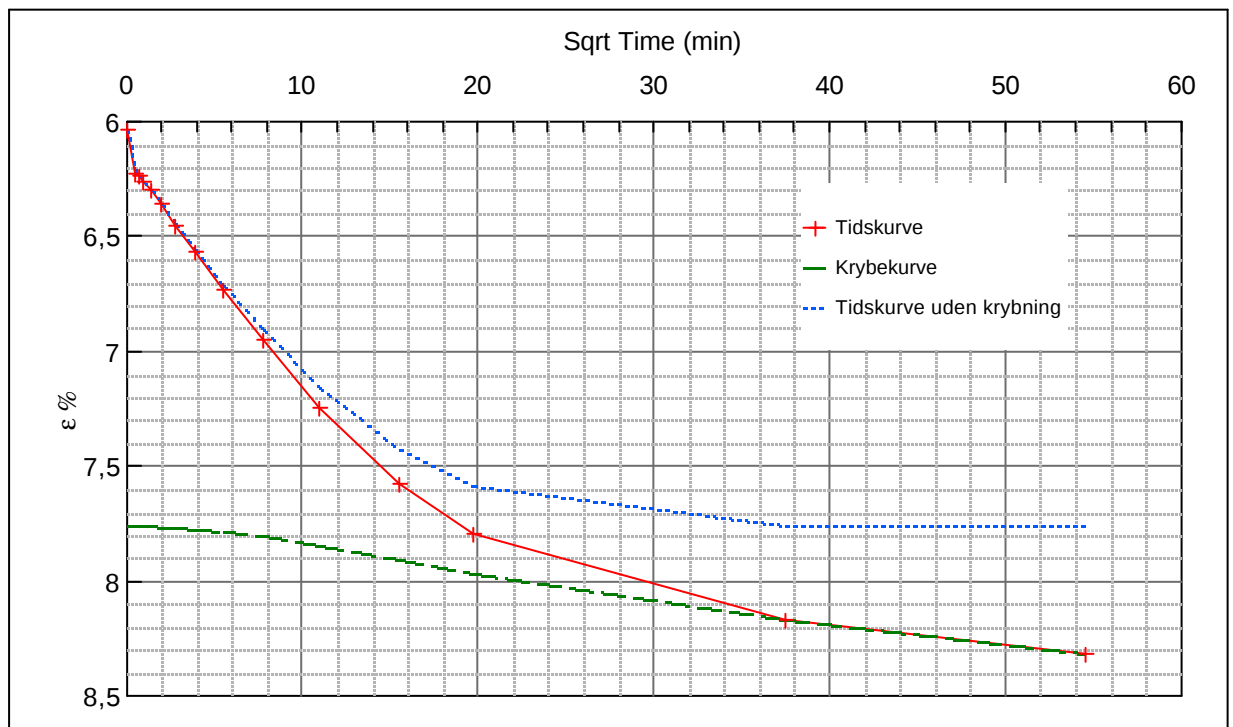
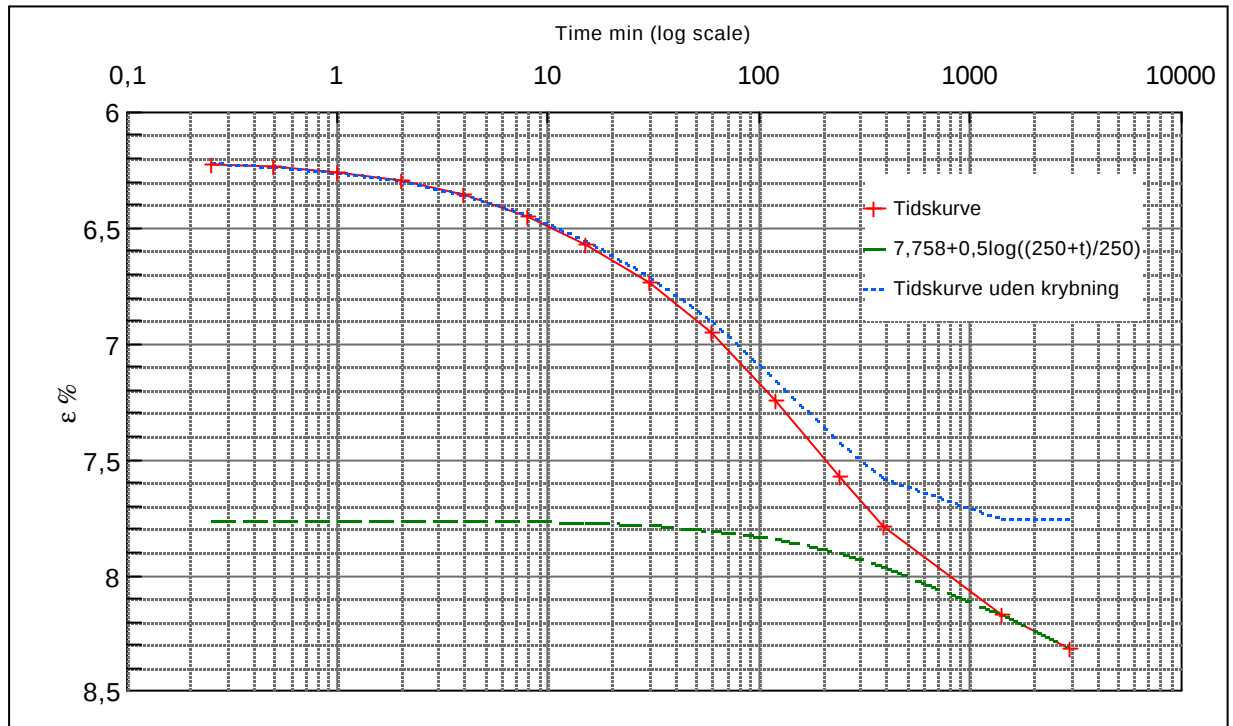
Step no 13	σ	kPa	ϵ	%	ϵ_i		tc in sec	11760
	Before	1.761,2	ϵ_0	4,76	ϵ_c %	5,81	K i kPa	72.910
	After	2.525,9	$\epsilon_{-#}$	6,03	ϵ_s	0,28	k10 m/sec	1,5E-11
					ϵ_{kryb}	0,22	ck10 m ² /sec	1,12E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 2.15
Executed:	AMS/mj/gt	Check:
Approved:		

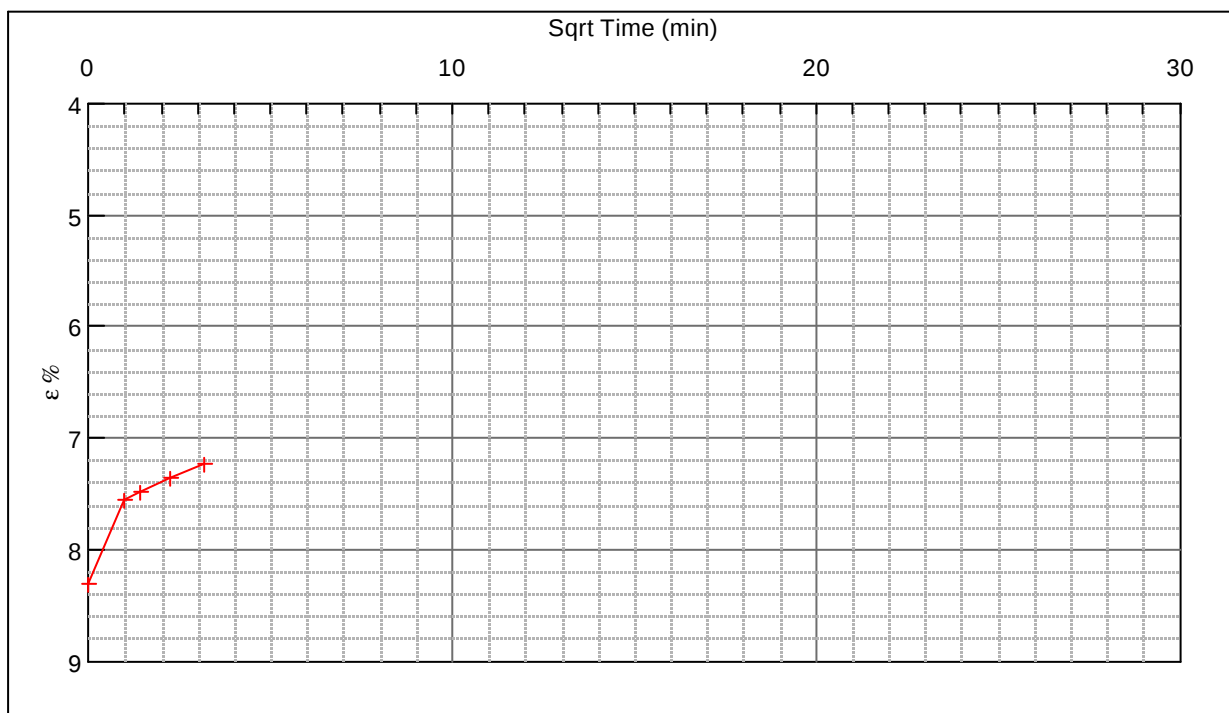
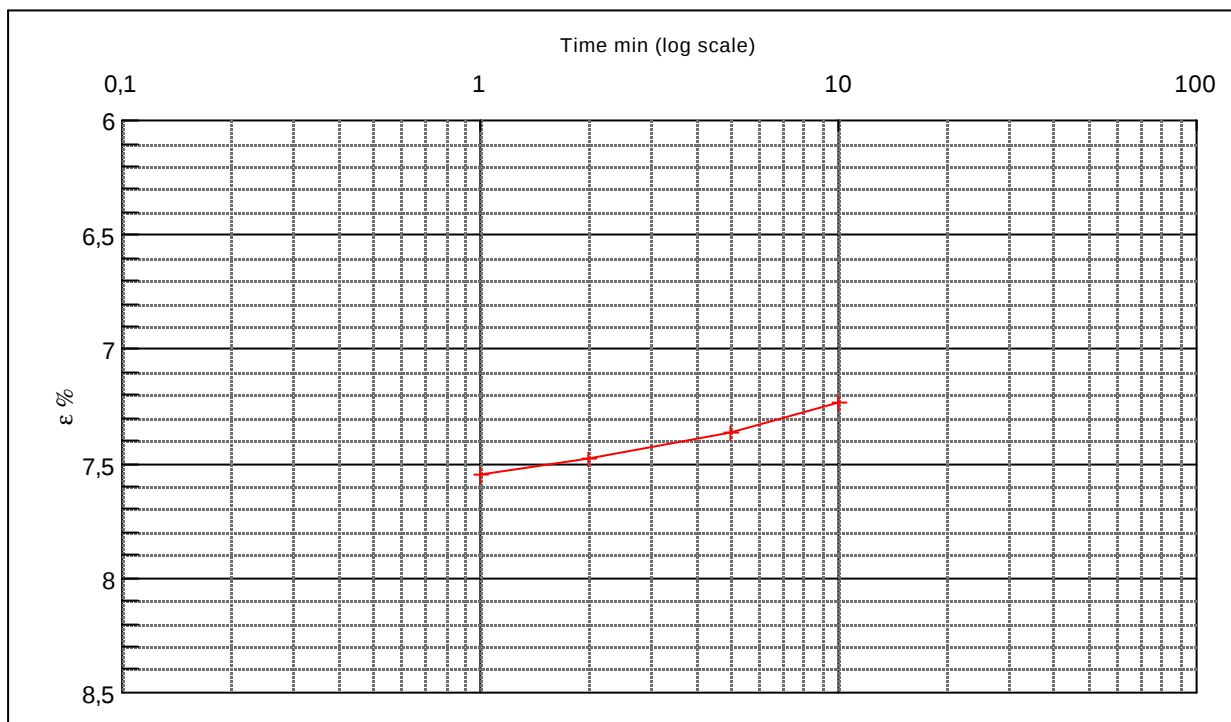
Step no 14	σ	kPa	ϵ	%	ϵ_i		tc in sec	15360
	Before	2.525,9	ϵ_0	6,03	ϵ_c %	7,76	K i kPa	88.649
	After	4.055,3	$\epsilon_{\sim\#}$	8,31	ϵ_s	0,5	k10 m/sec	9,5E-12
					ϵ_{kryb}	0,55	ck10 m ² /sec	8,59E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 2.16
Executed:	AMS/mj/gt	Check:
Approved:		

Step no 15	σ	kPa	ϵ	%	ϵ_i	4	tc in sec	114.198
	Before	4.055,3	ϵ_0	7,55	ϵ_c		K i kPa	
	After	2,29	$\epsilon_{\sim\#}$	4	ϵ_s		k10 m/sec	
					ϵ_{kvyb}	ck10 m^2 /sec		

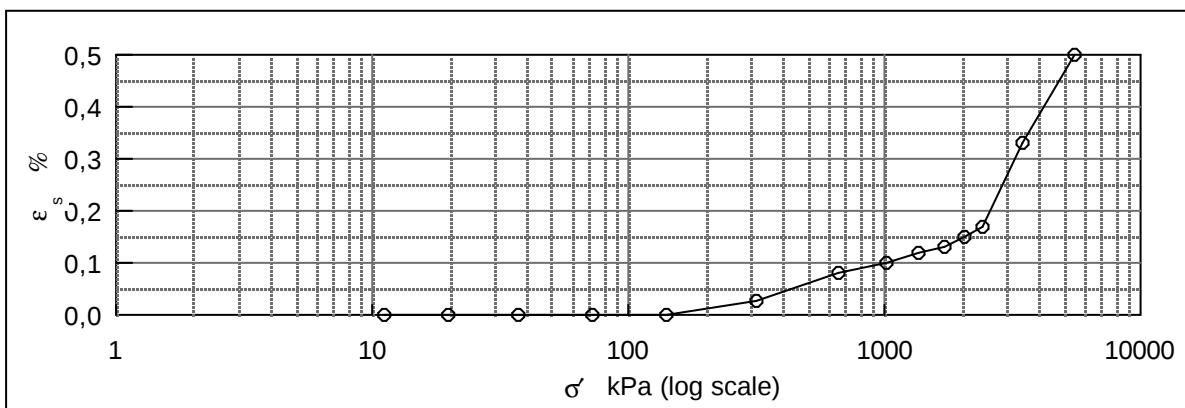
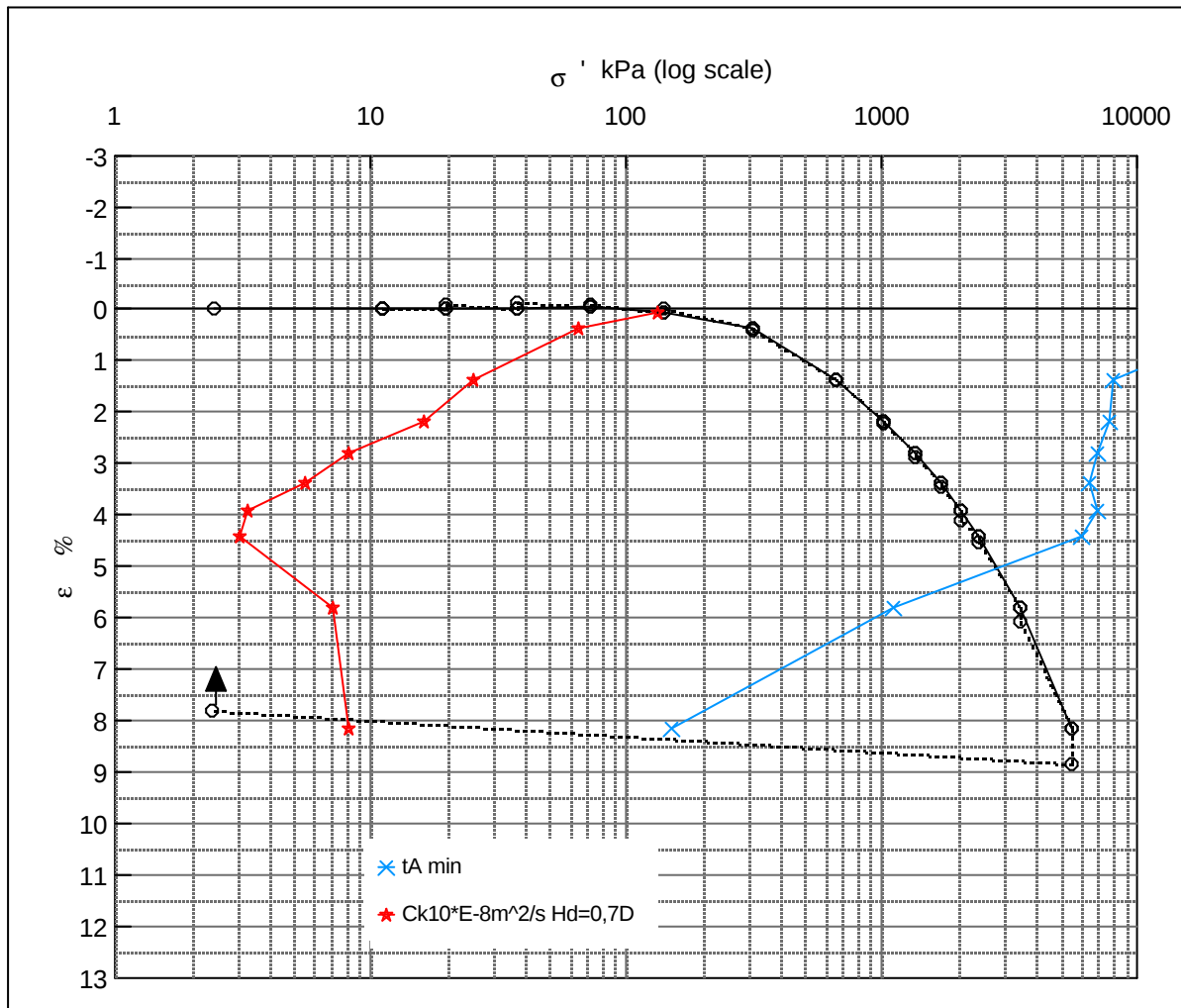


Material: Clay Eemian Glacial	
Bor no : Lab. no: Pr 1	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

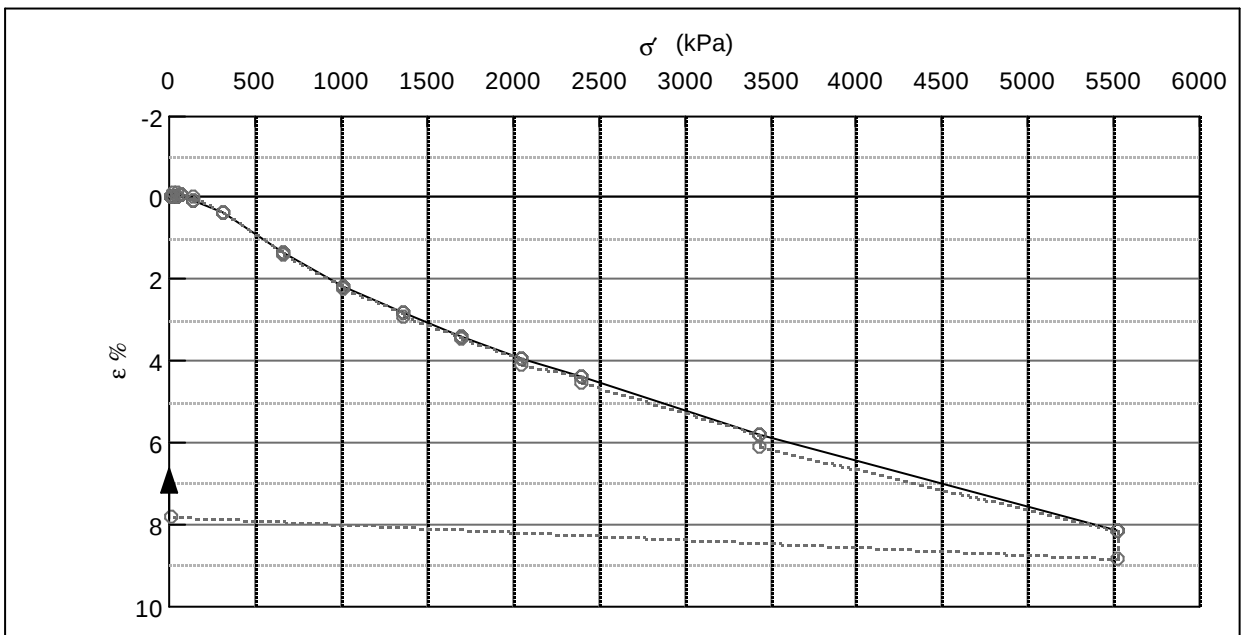
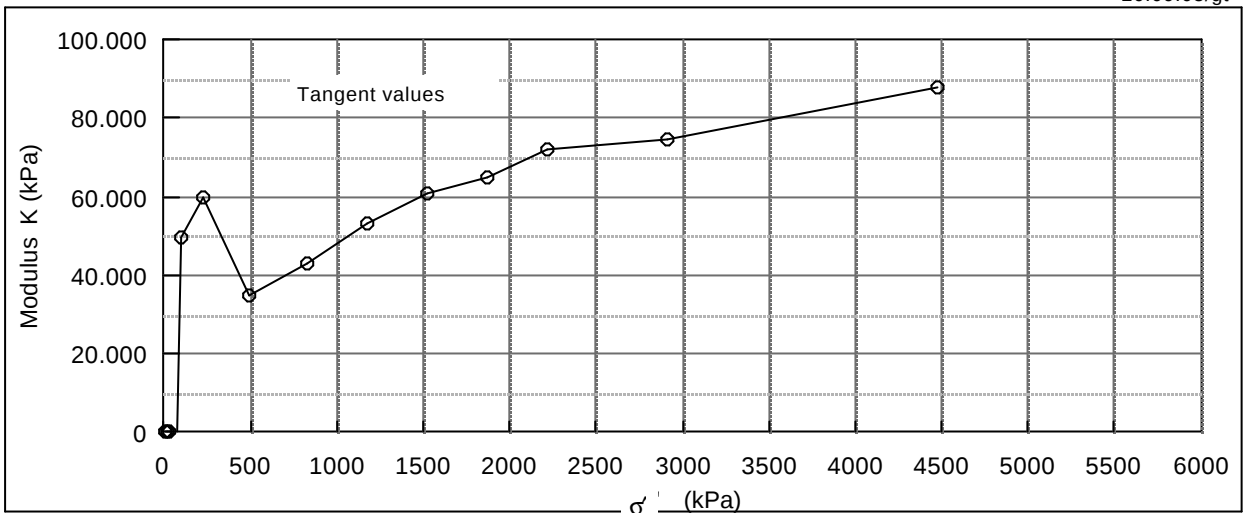
Job:	Anholt	AAU
		Encl. No 2.17
Executed:	AMS/mj/gt	Check:
Approved:		

20.09.05/gt

Description of soil: Clay Eemian Glacial			Water content %	Before	After
			Bulk density Mg/m ³	22,5	20,1
			Grain density Mg/m ³	1,99	2,11
			Void ratio	~2.72	0,68
Bor no :	Overburden pressure σ'_o	~780 kPa	Degr. of Saturation %	91	100
Lab. no: Pr.2	Vane strength c_v	kPa	Dimension H x D mm	30x60	27.7x60
Level : 76.7 m.b.s	CPT - value q_c	MPa			



Job: Anholt		AAU
		Encl. No 3.1
Executed:	AMS/mj/gt	Check:
Approved:		



Test results		σ kPa	ϵ_c %	ϵ_s % / lct	Ck10 m ² /s	σ_m kPa	K kPa	w %
Q	13 % ?	2,4				-	-	24,9
Qs	~0.5 %	11,1				6,8		24,9
σ_{pc}	>4000 kPa	19,8				15,4		24,9
		37,1				28,5		24,9
		71,8	(0,07)			54,5	-49565,4	24,9
		141,2	0,07	0,00	1,3E-06	106,5	49565,4	24,8
		314,7	0,36	0,03	6,5E-07	228,0	59820,3	24,6
		661,6	1,35	0,08	2,5E-07	488,2	35046,2	24,0
		1.008,6	2,16	0,10	1,6E-07	835,1	42834,3	23,5
		1.355,6	2,81	0,12	8,2E-08	1.182,1	53378,1	23,1
		1.702,5	3,38	0,13	5,6E-08	1.529,0	60869,8	22,8
		2.049,5	3,92	0,15	3,3E-08	1.876,0	64851,9	22,4
		2.396,4	4,40	0,17	3,1E-08	2.223,0	71982,9	22,2
		3.437,3	5,80	0,33	7,2E-08	2.916,9	74454,5	21,3
		5.519,1	8,17	0,50	8,2E-08	4.478,2	87726,4	19,8
		2,4	7,80			2.760,7	1499083,9	20,1

Remark:
"Genbelastningsgren"
Normalkonsolideret tilstand næppe nået

Job: Anholt

AAU

Encl. No

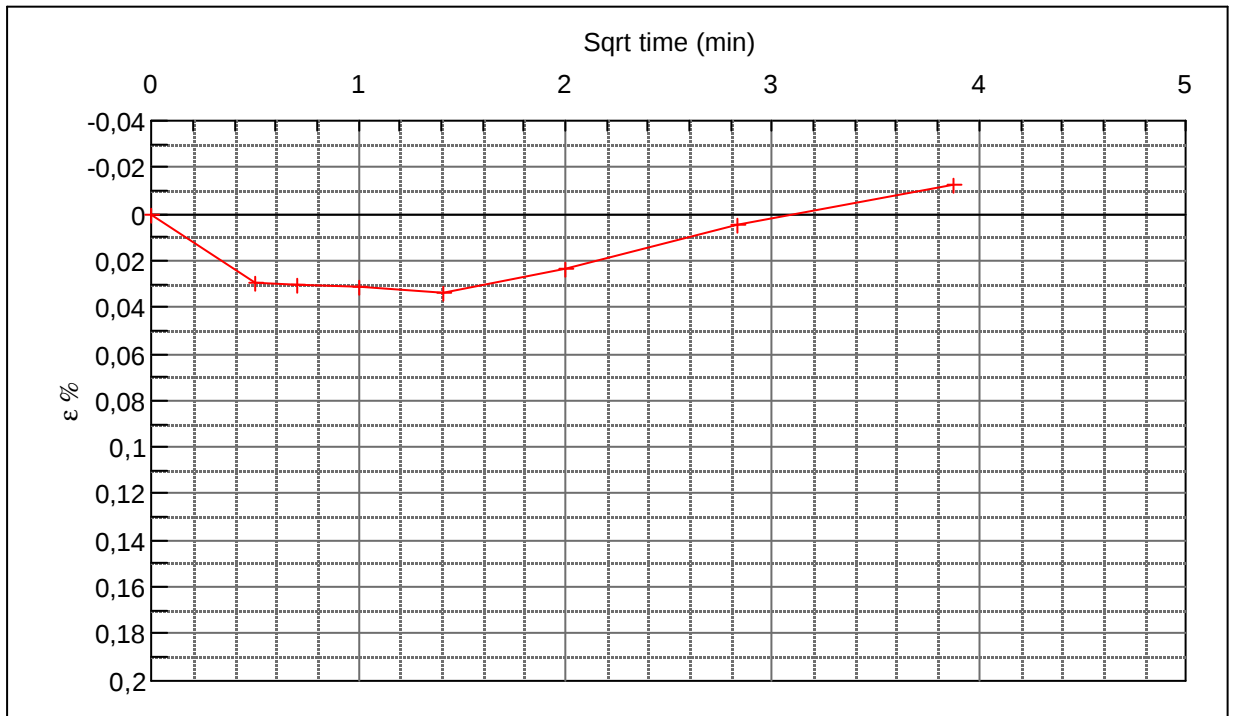
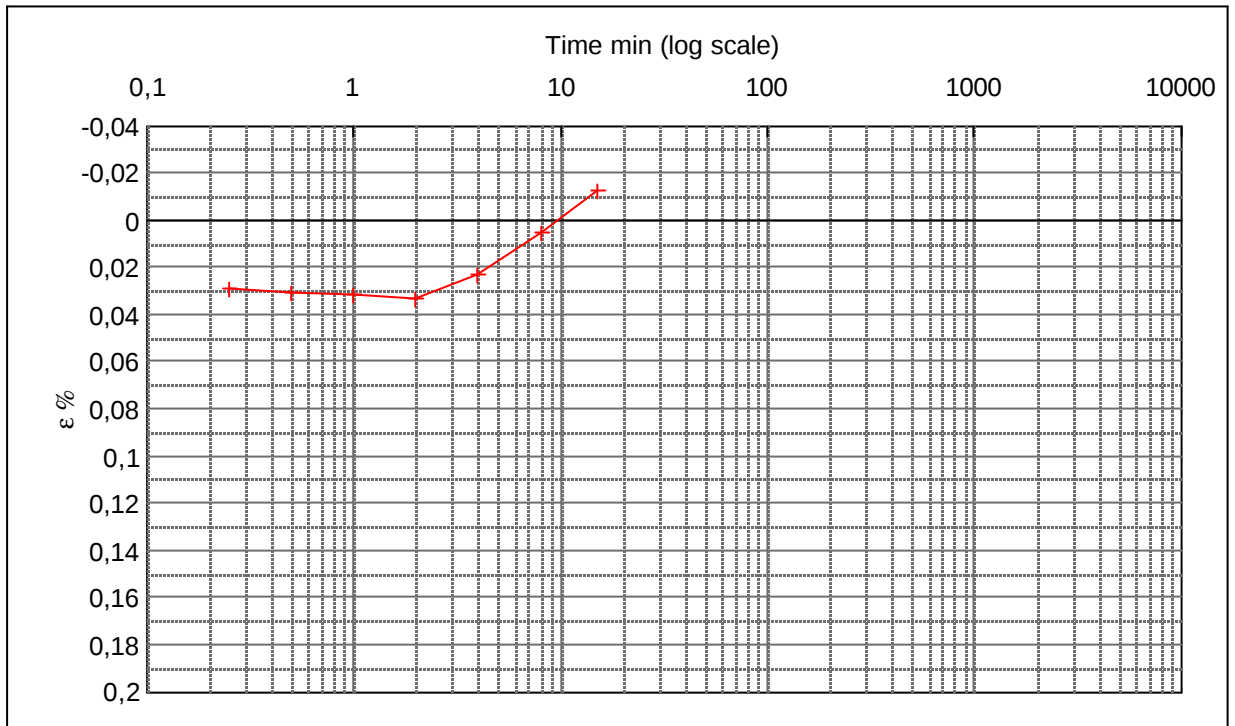
3.2

Executed: AMS/mj/gt

Check:

Approved:

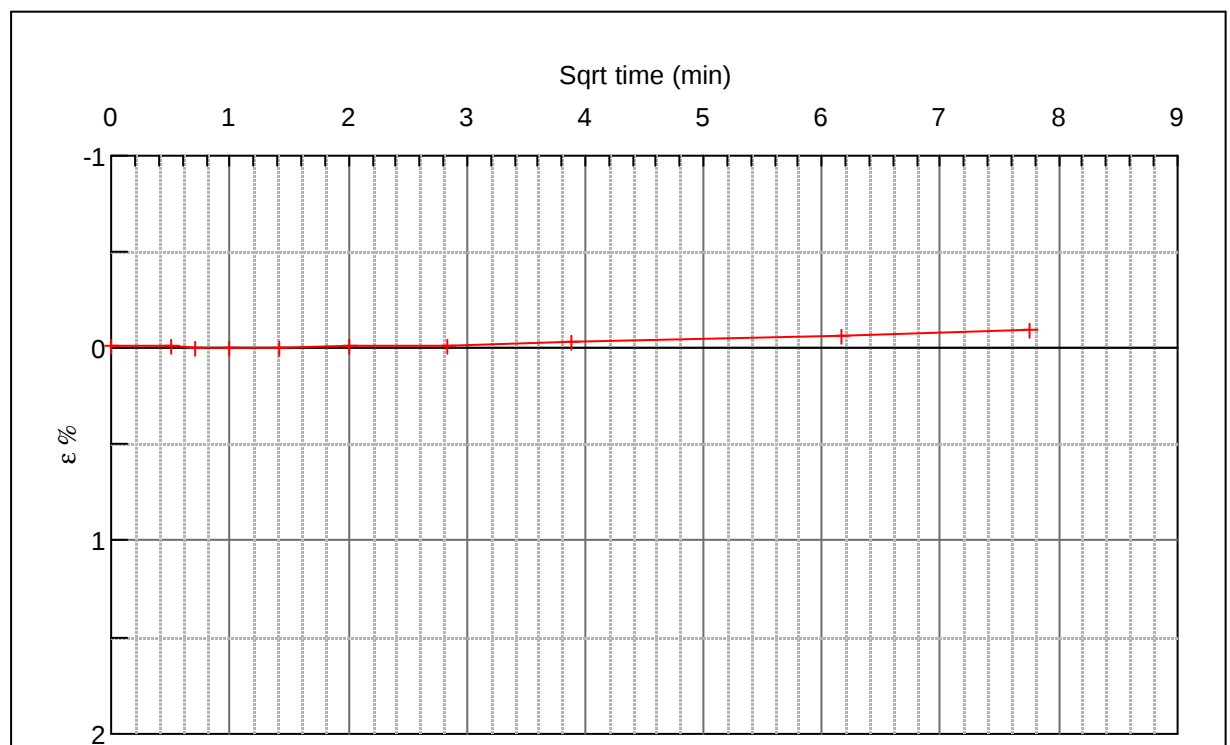
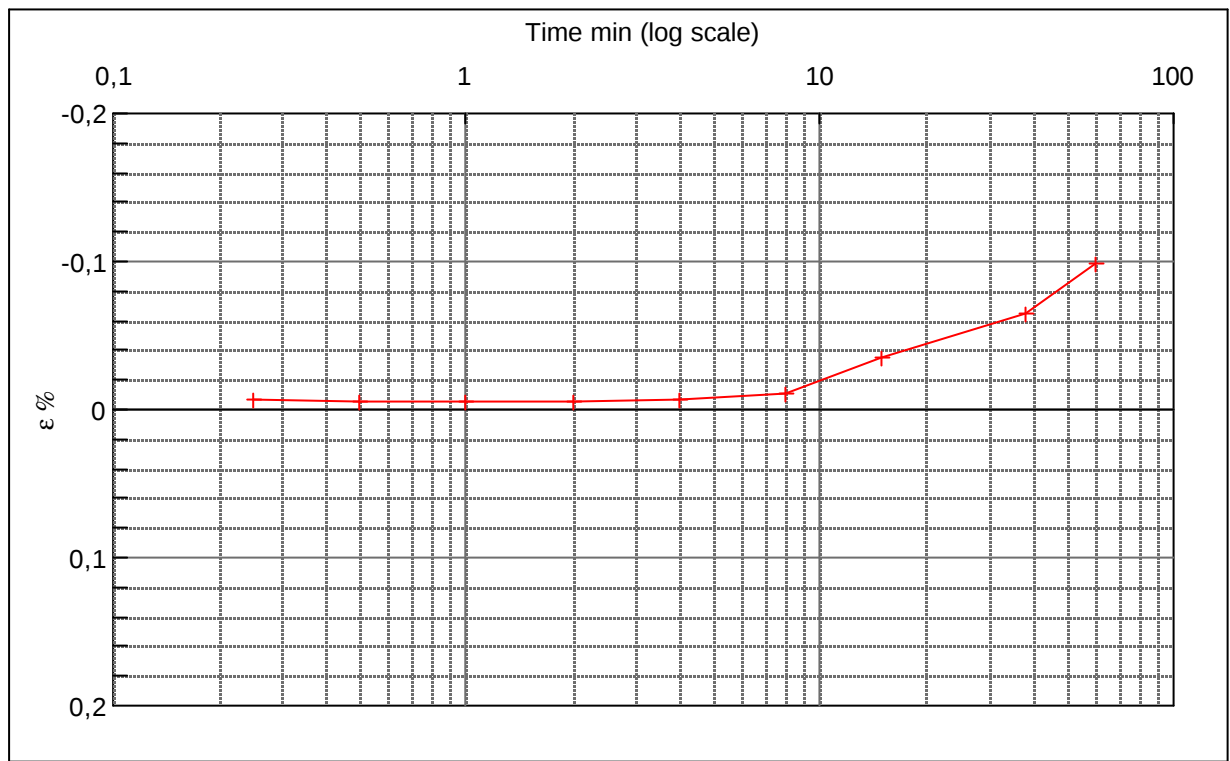
Step no 1	σ	kPa	ϵ	%	ϵ_i	tc in sec	
	Before	2,43	ϵ_0	0,000	ϵ_c %	K i kPa	
	After	11,1	$\epsilon_{\sim\#}$	(0,013)	ϵ_s	k10 m/sec	
					ϵ_{kyb}	ck10 m ² /sec	



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job: Anholt	AAU
	Encl. No 3.3
Executed: AMS/mj/gt	Check:
Approved:	

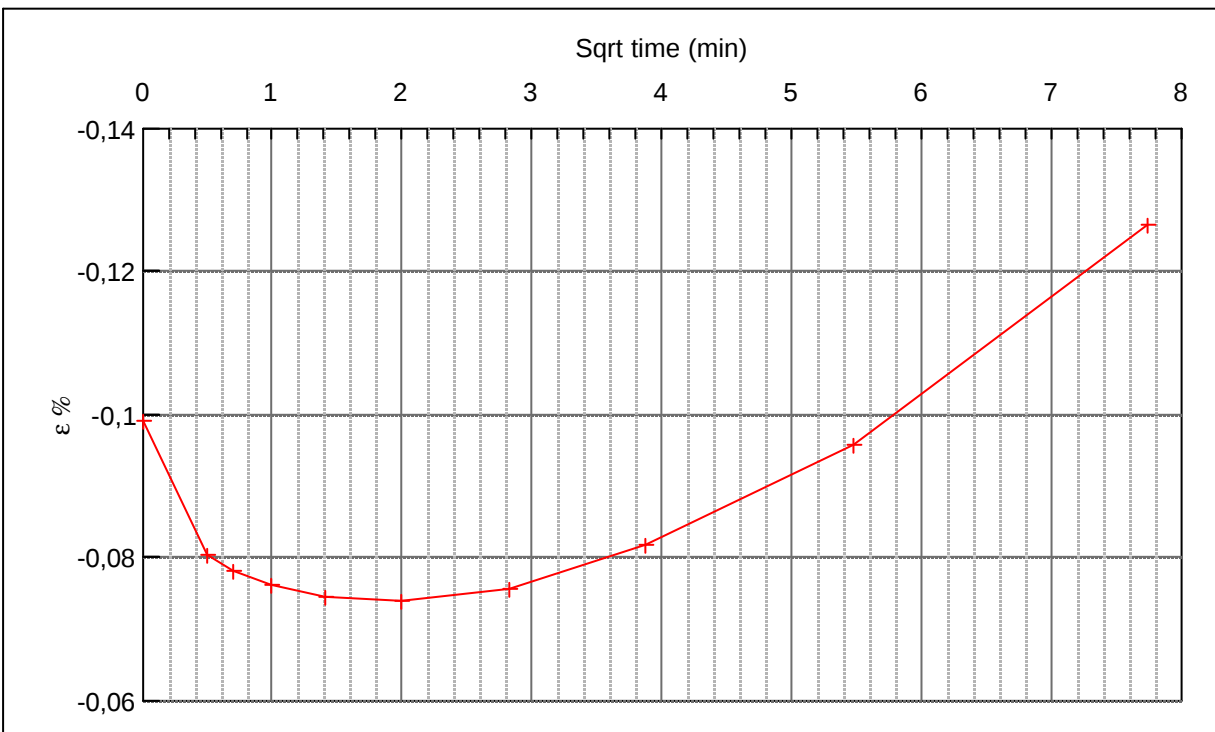
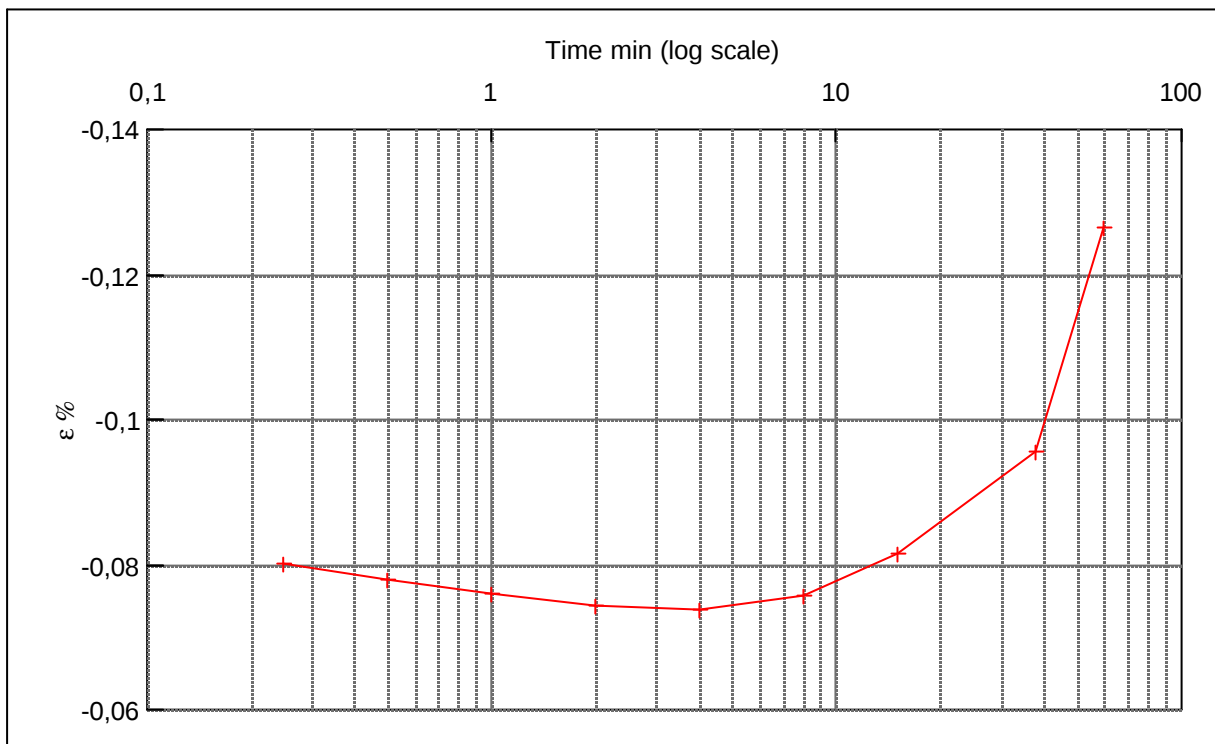
Step no	σ	kPa	ε	%	ε_i	tc in sec		
2	Before	11,1	ε_0	(0,012)	ε_c %	K i kPa		
	After	19,8	$\varepsilon_{\sim\#}$	(0,099)	ε_s	k10 m/sec		
					ε_{kylb}	ck10 m^2 /sec		



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job: Anholt	AAU
	Encl. No 3.4
Executed: AMS/mj/gt	Check:
Approved:	

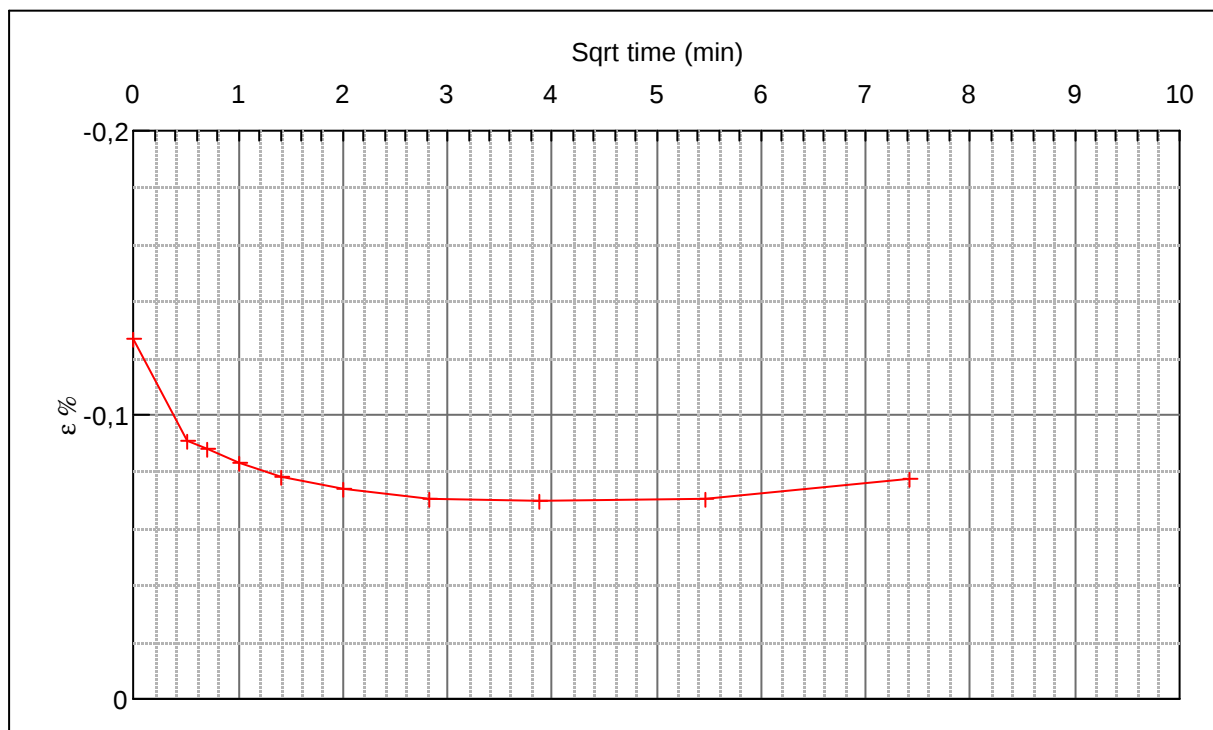
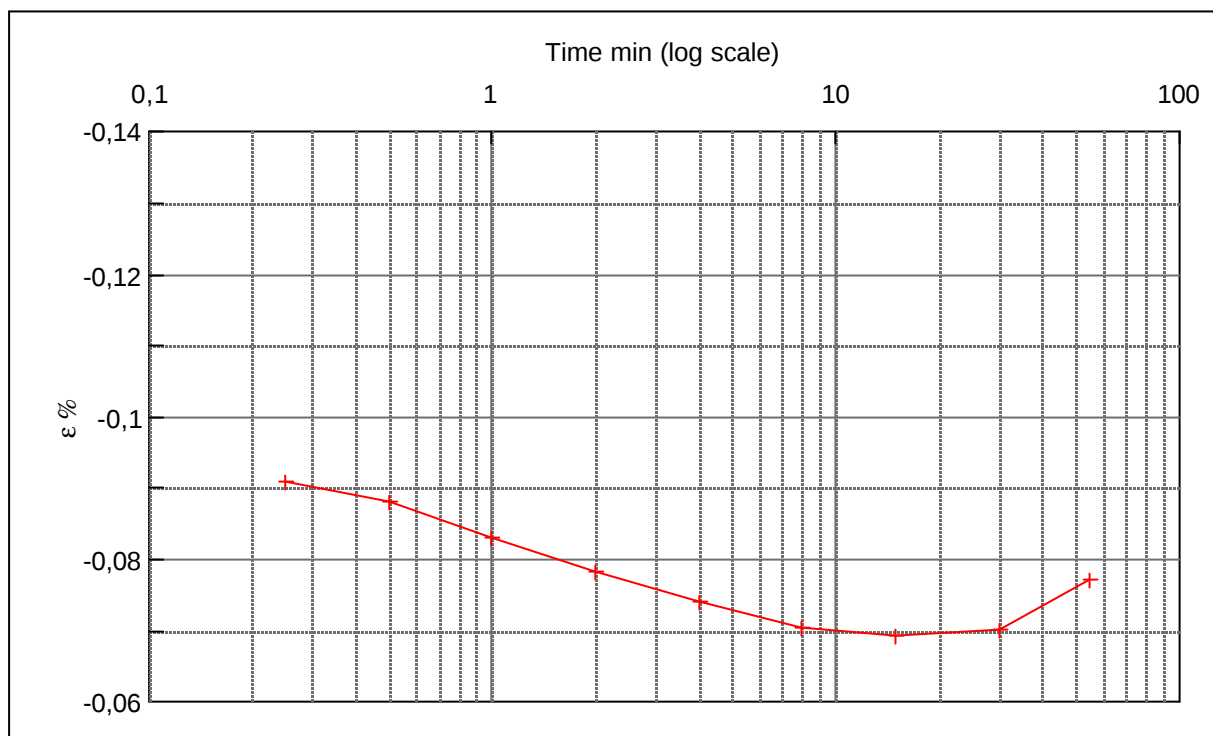
Step no 3	σ	kPa	ϵ %	ϵ_i	tc in sec	
	Before	19,8	ϵ_0 (0,099)	ϵ_c %	K i kPa	
	After	37,1	$\epsilon_{-#}$ (0,127)	ϵ_s	k10 m/sec	
				ϵ_{kryb}	ck10 m ² /sec	



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job: Anholt	AAU
	Encl. No 3.5
Executed: AMS/mj/gt	Check:
Approved:	

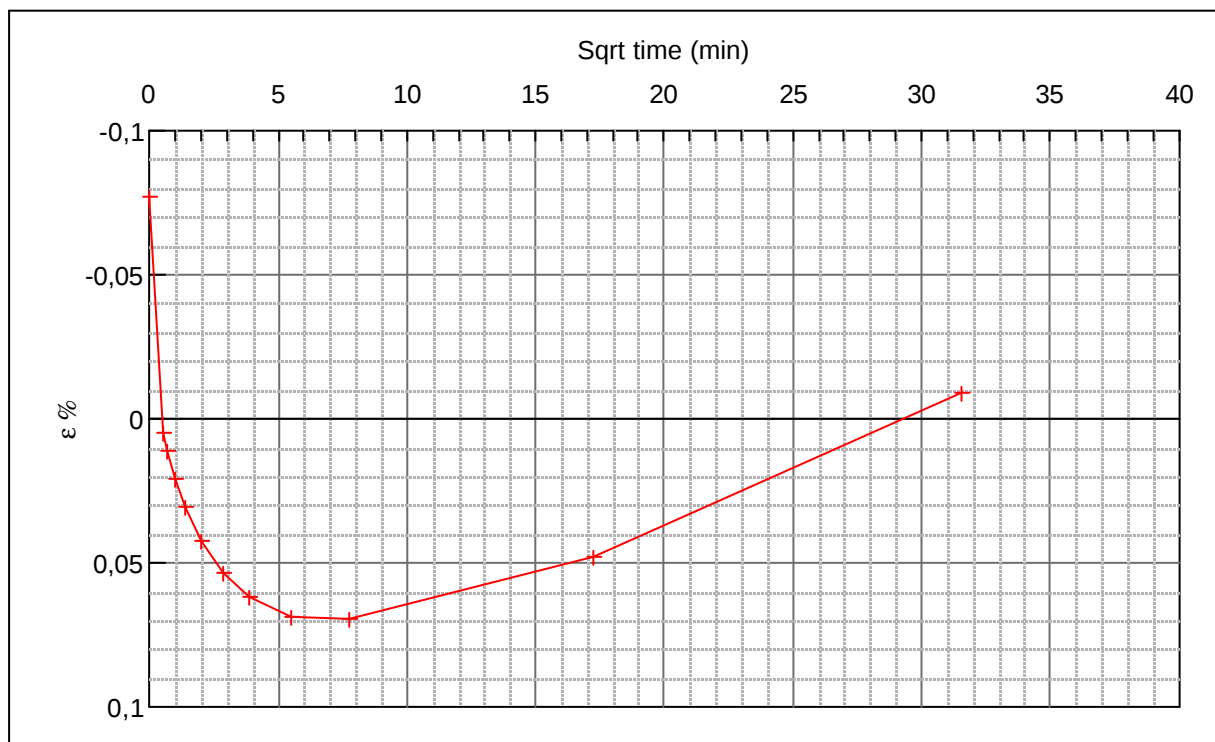
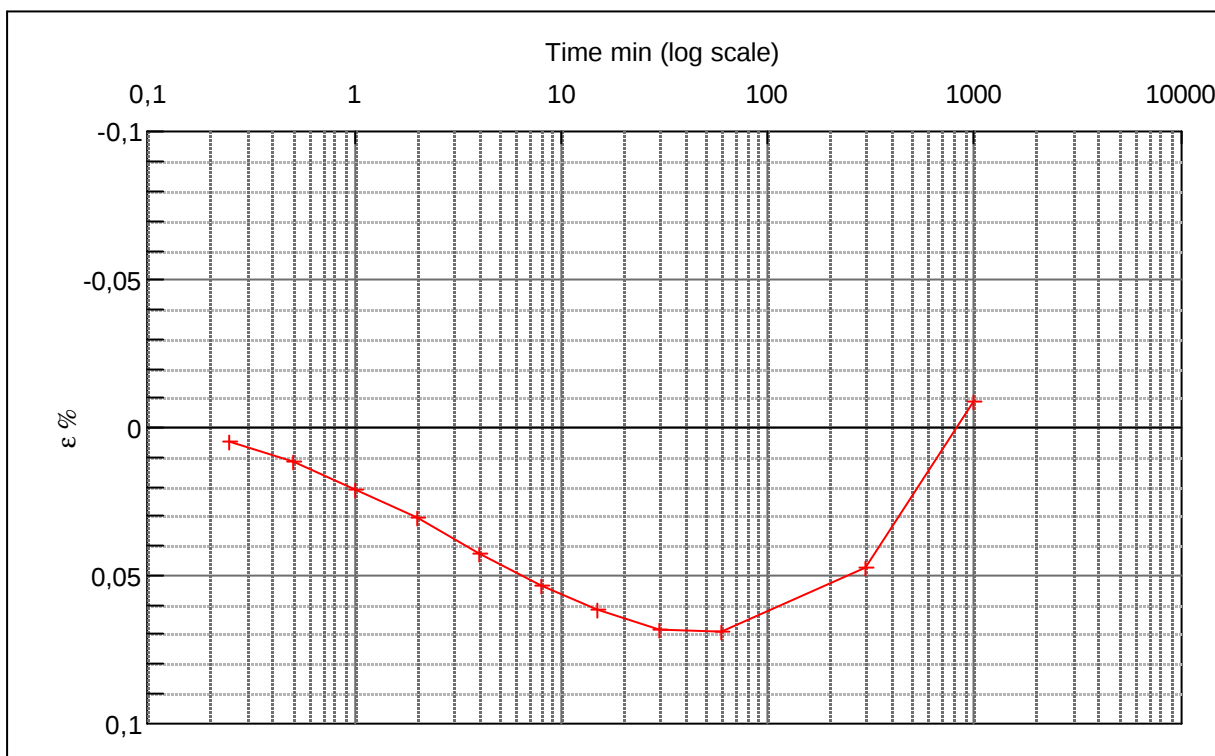
Step no 4	σ	kPa	ϵ %	ϵ_i	tc in sec	
	Before	37,1	ϵ_0 (0,127)	ϵ_c % -0,07	K i kPa	
	After	71,8	$\epsilon_{-#}$ (0,077)	ϵ_s	k10 m/sec	
				ϵ_{kryb}	ck10 m ² /sec	



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.6
Executed:	AMS/mj/gt	Check:
Approved:		

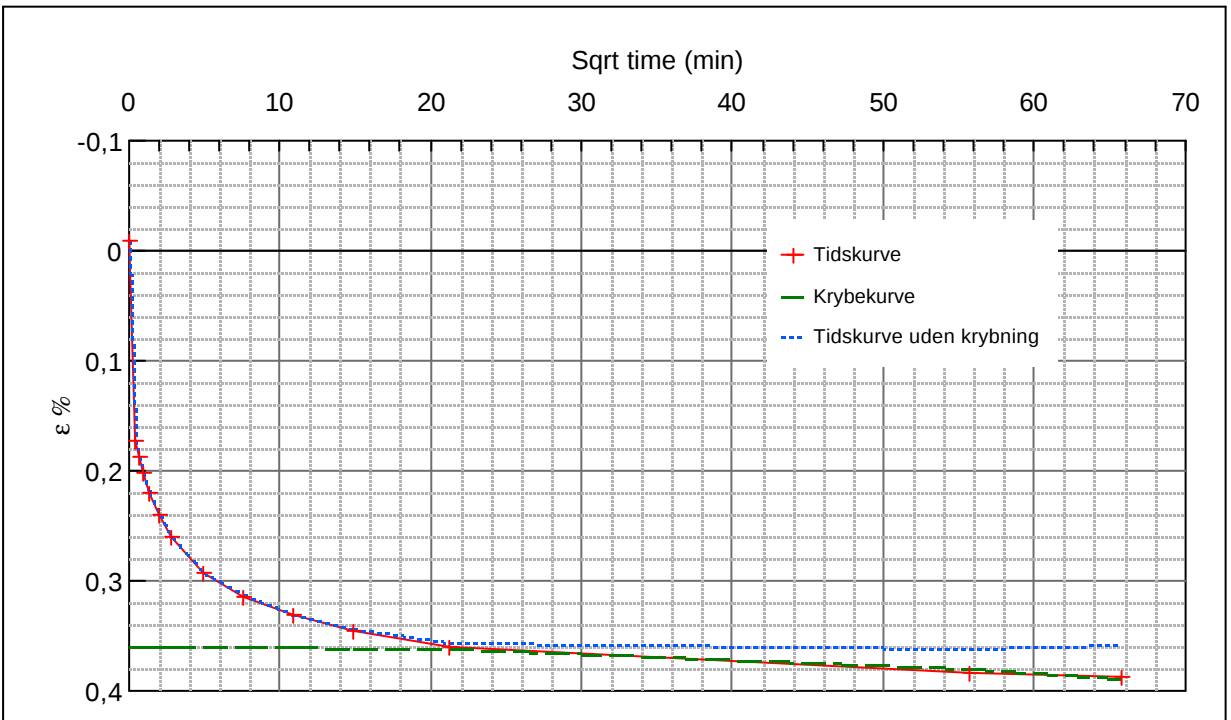
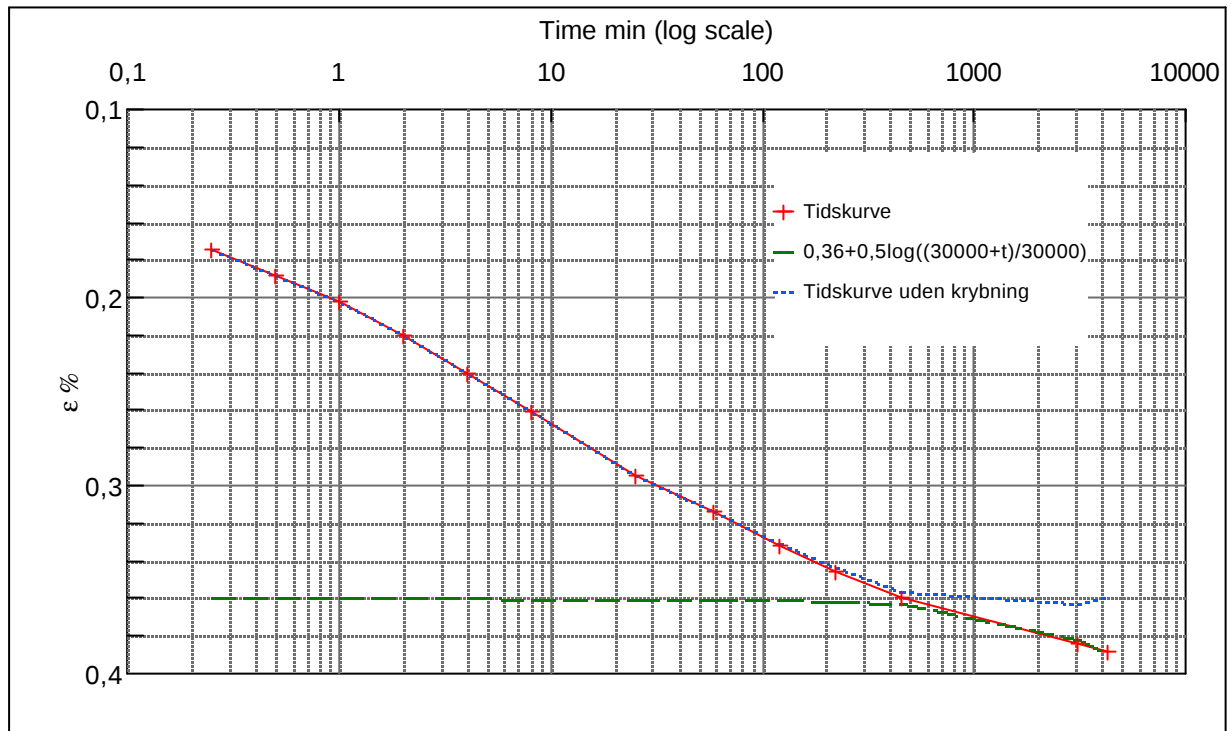
Step no 5	σ	kPa	ϵ	%	ϵ_i		tc in sec	735
	Before	71,8	ϵ_0	(0,08)	ϵ_c %	0,07	K i kPa	47.205
	After	141,2	$\epsilon_{\sim\#}$	(0,01)	ϵ_s		k10 m/sec	2,7E-10
					ϵ_{kyb}		ck10 m^2 /sec	1,32E-06



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.7
Executed:	AMS/mj/gt	Check:
Approved:		

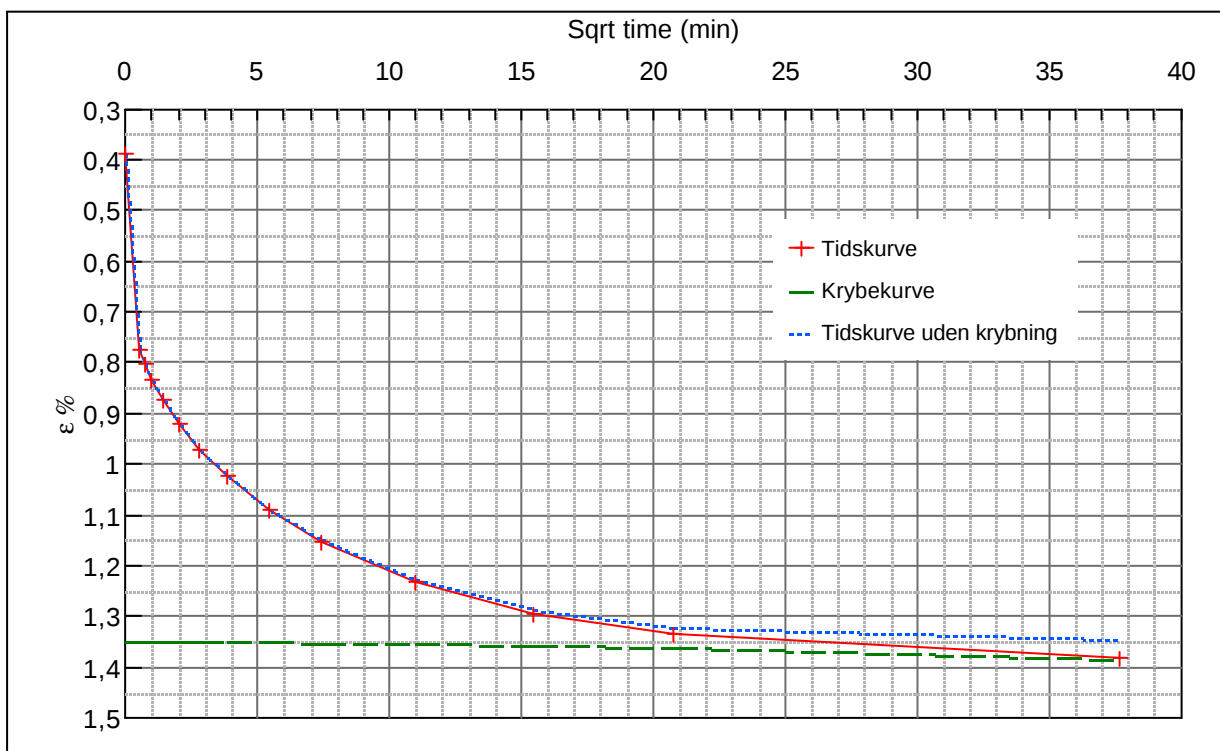
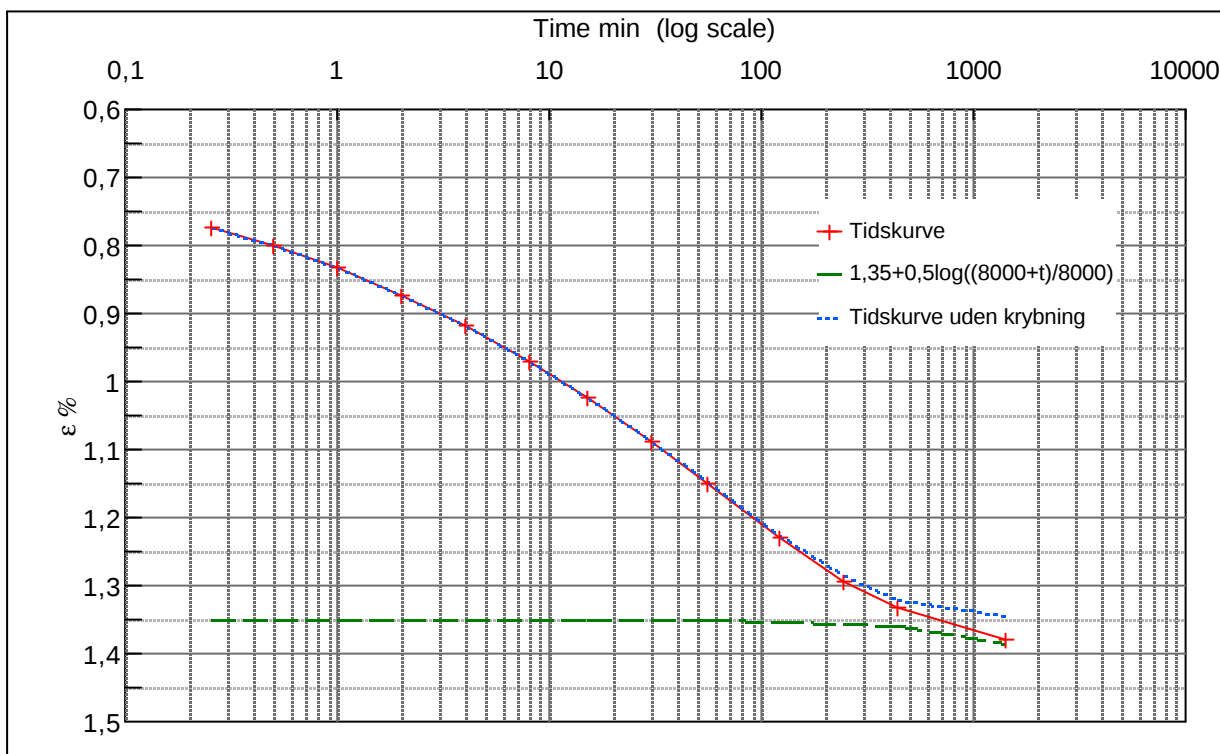
Step no 6	σ	kPa	ϵ	%	ϵ_i		tc in sec	1500
	Before	141,2	ϵ_0	(0,01)	ϵ_c %	0,36	K i kPa	47.013
	After	314,7	$\epsilon_{\sim\#}$	0,39	ϵ_s	0,028	k10 m/sec	1,3E-10
					ϵ_{kryb}	0,028	ck10 m ² /sec	6,47E-07



Material:	Clay	Eemian	Glacial
Bor no :	P2	Depth:	76.7 m.b.s
Lab. no:		Insitu stress:	~780 kPa

Job:	Anholt	AAU
		Encl. No
		3.8
Executed:	AMS/mj/gt	Check:
Approved:		

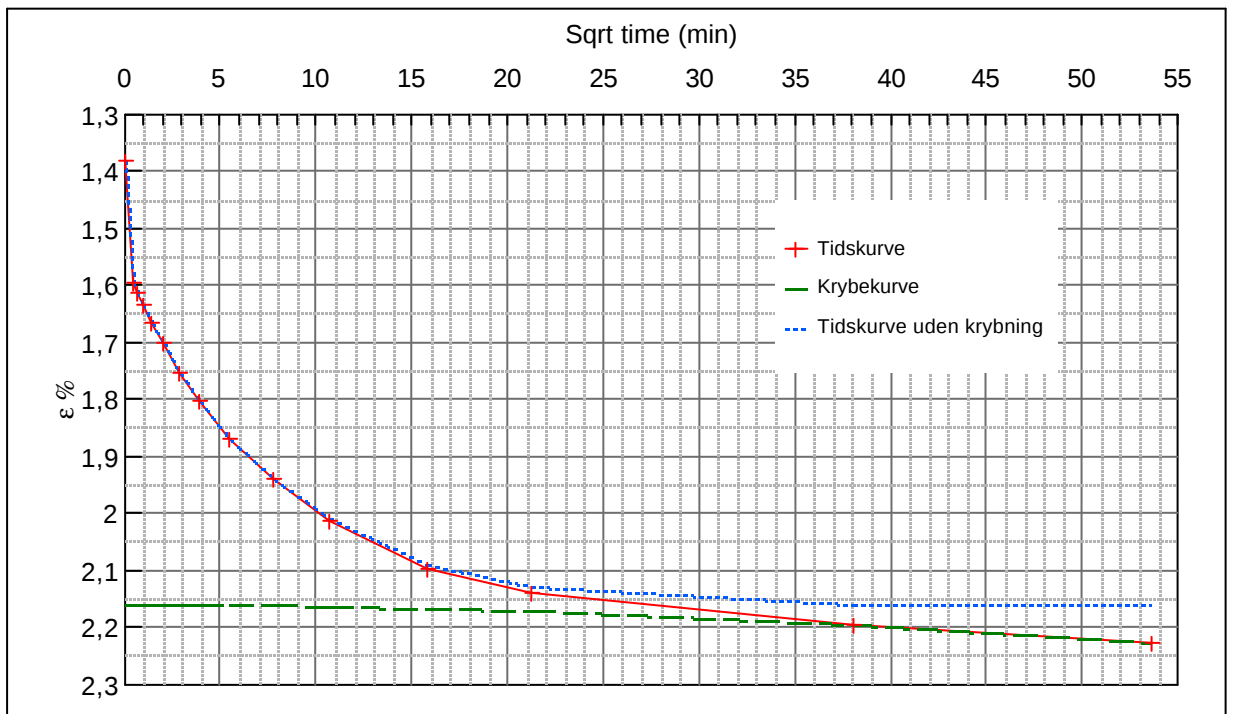
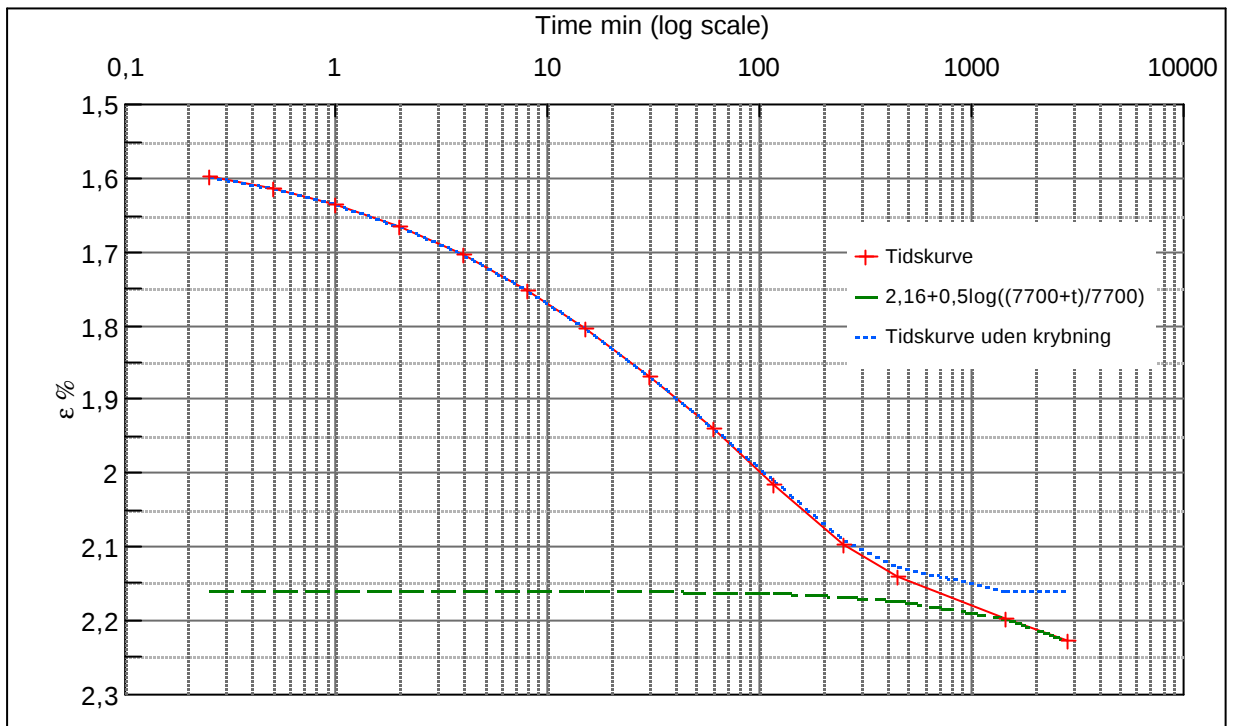
Step no 7	σ	kPa	ε	%	ε_i		tc in sec	3840
	Before	314,7	ε_0	0,39	ε_c %	1,35	K i kPa	36.060
	After	661,6	$\varepsilon_{\sim\#}$	1,38	ε_s	0,08	k10 m/sec	6,9E-11
					ε_{kryb}	0,032	ck10 m ² /sec	2,52E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.9
Executed:	AMS/mj/gt	Check:
Approved:		

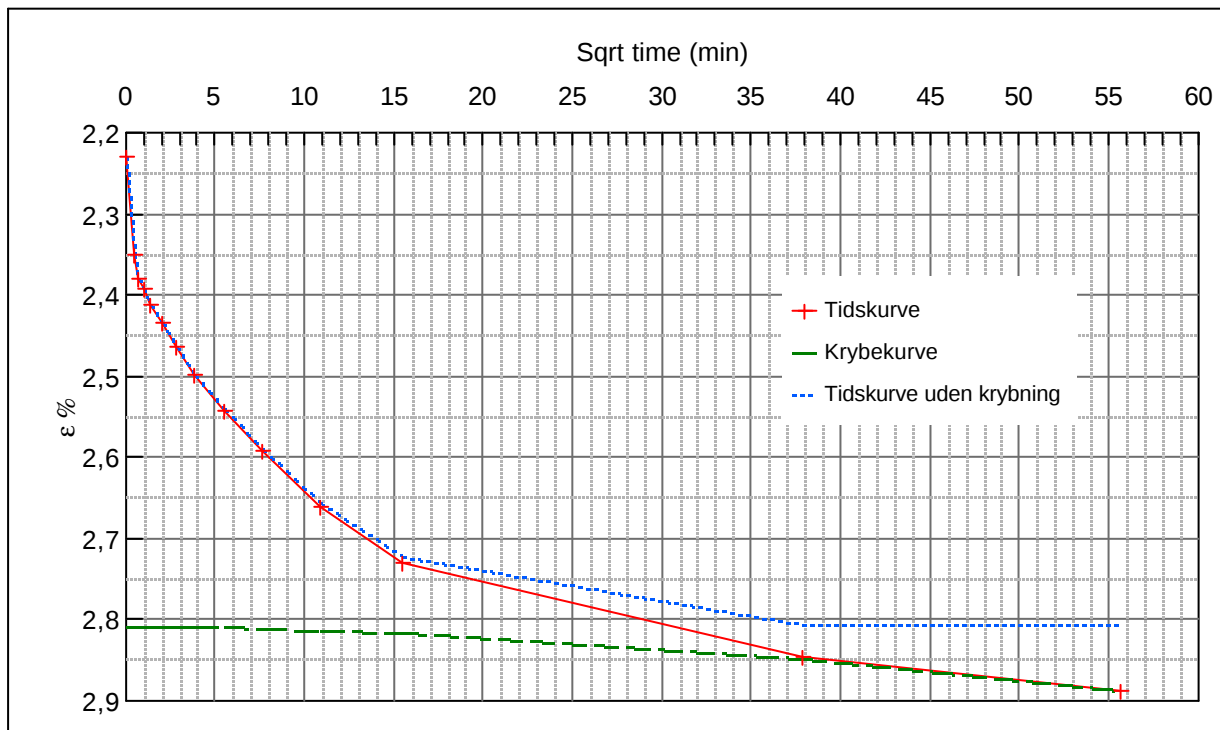
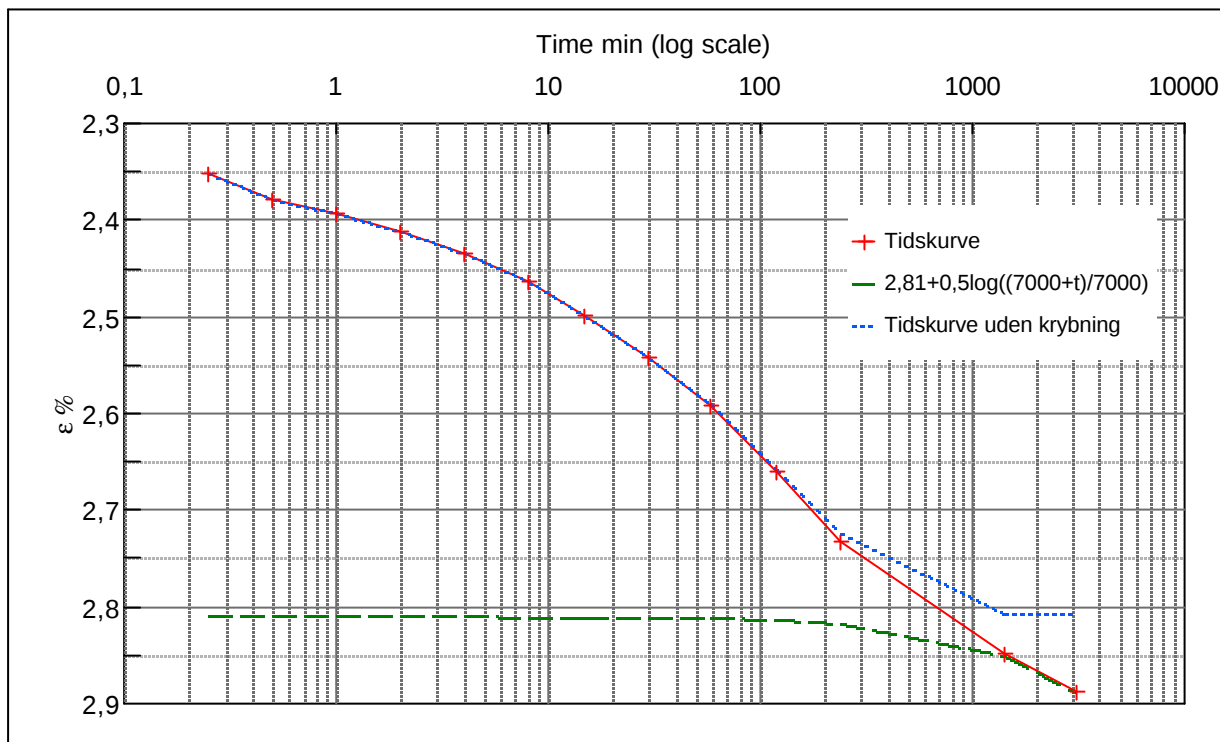
Step no 8	σ	kPa	ϵ	%	ϵ_i		tc in sec	6000
	Before	661,6	ϵ_0	1,38	ϵ_c %	2,16	K i kPa	44.577
	After	1.008,6	$\epsilon_{\sim\#}$	2,23	ϵ_s	0,1	k10 m/sec	3,6E-11
					ϵ_{kryb}	0,069	ck10 m^2/sec	1,62E-07



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 3.10
Executed:	AMS/mj/gt	Check:
Approved:		

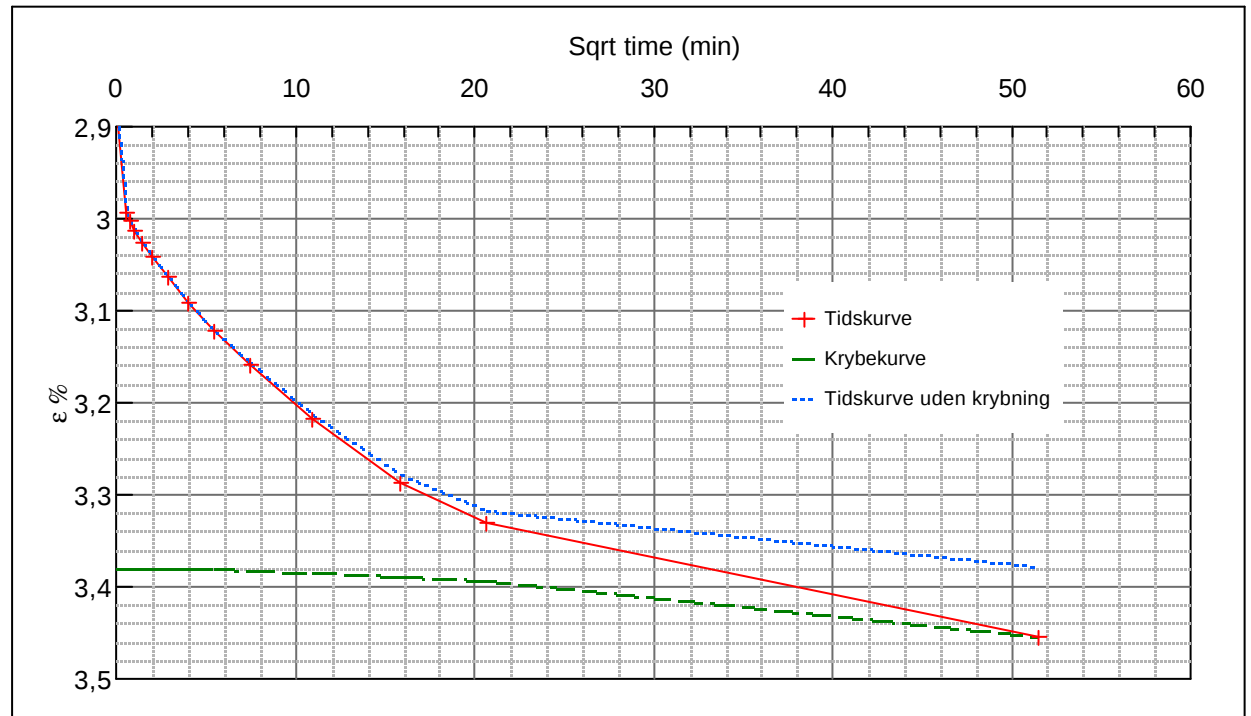
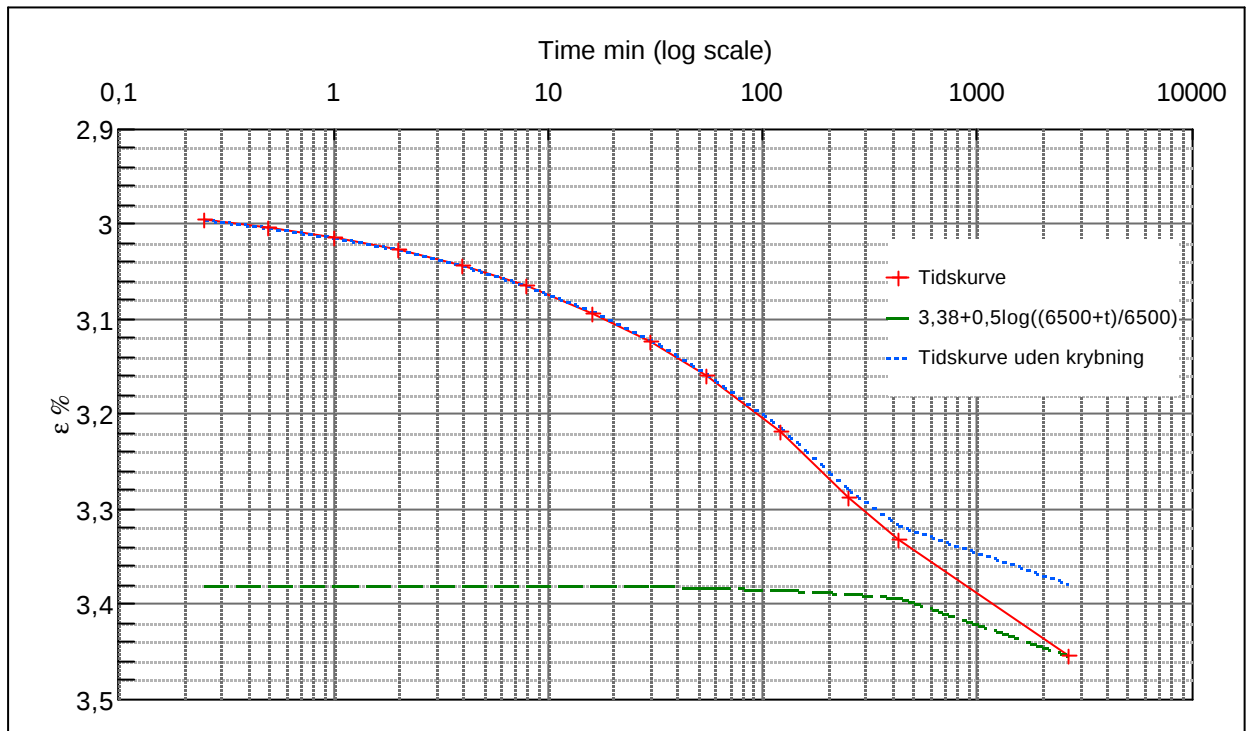
Step no 9	σ	kPa	ϵ	%	ϵ_i		tc in sec	11760
	Before	1.008,6	ϵ_0	2,23	ϵ_c %	2,81	K i kPa	59.666
	After	1.355,6	$\epsilon_{\sim\#}$	2,89	ϵ_s	0,12	k10 m/sec	1,4E-11
					ϵ_{kryb}	0,078	ck10 m^2/sec	8,25E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.11
Executed:	AMS/mj/gt	Check:
Approved:		

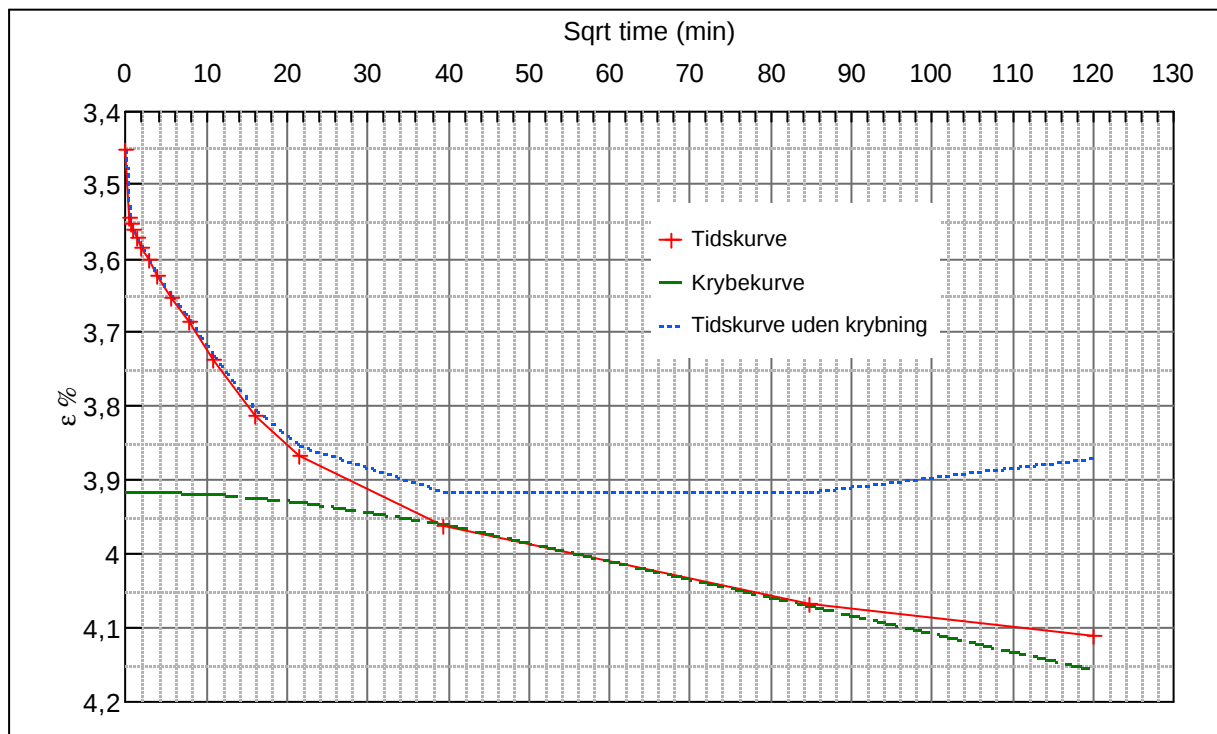
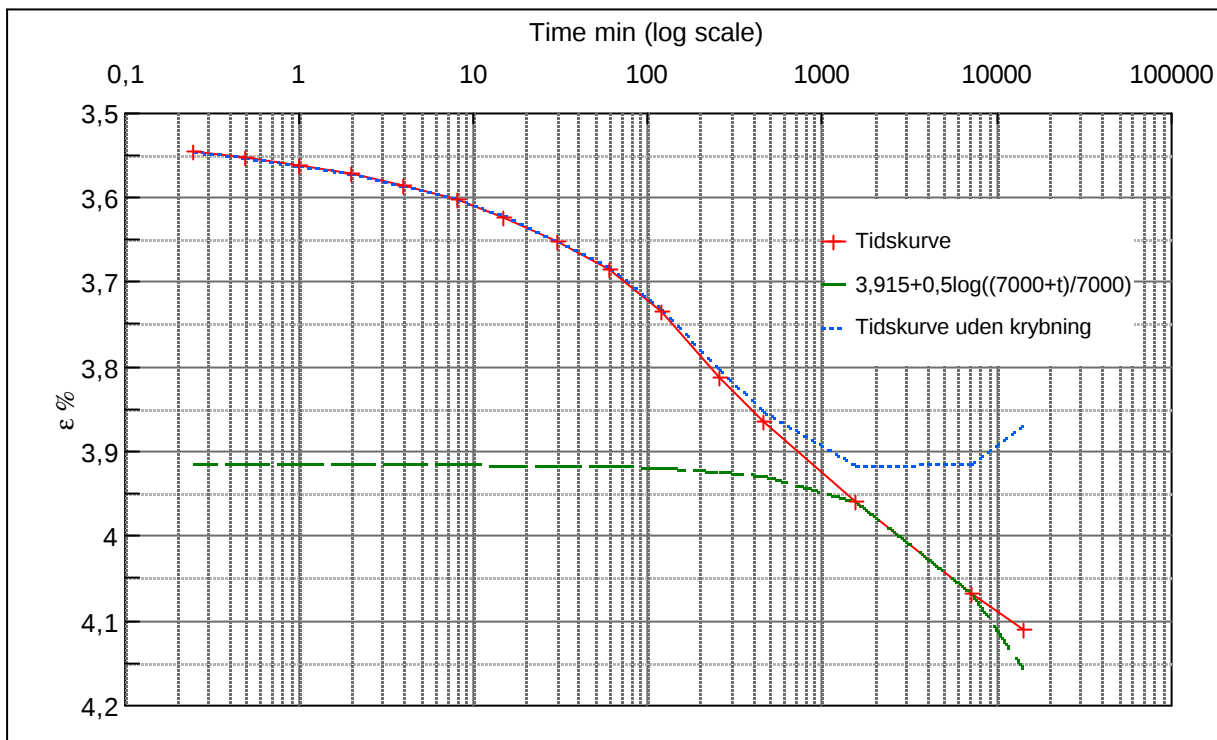
Step no 10	σ	kPa	ϵ	%	ϵ_i		tc in sec	17340
	Before	1.355,6	ϵ_0	2,89	ϵ_c %	3,38	K i kPa	70.448
	After	1.702,5	$\epsilon_{\sim\#}$	3,45	ϵ_s	0,13	k10 m/sec	7,8E-12
					ϵ_{kryb}	0,073	ck10 m ² /sec	5,59E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 3.12
Executed:	AMS/mj/gt	Check:
Approved:		

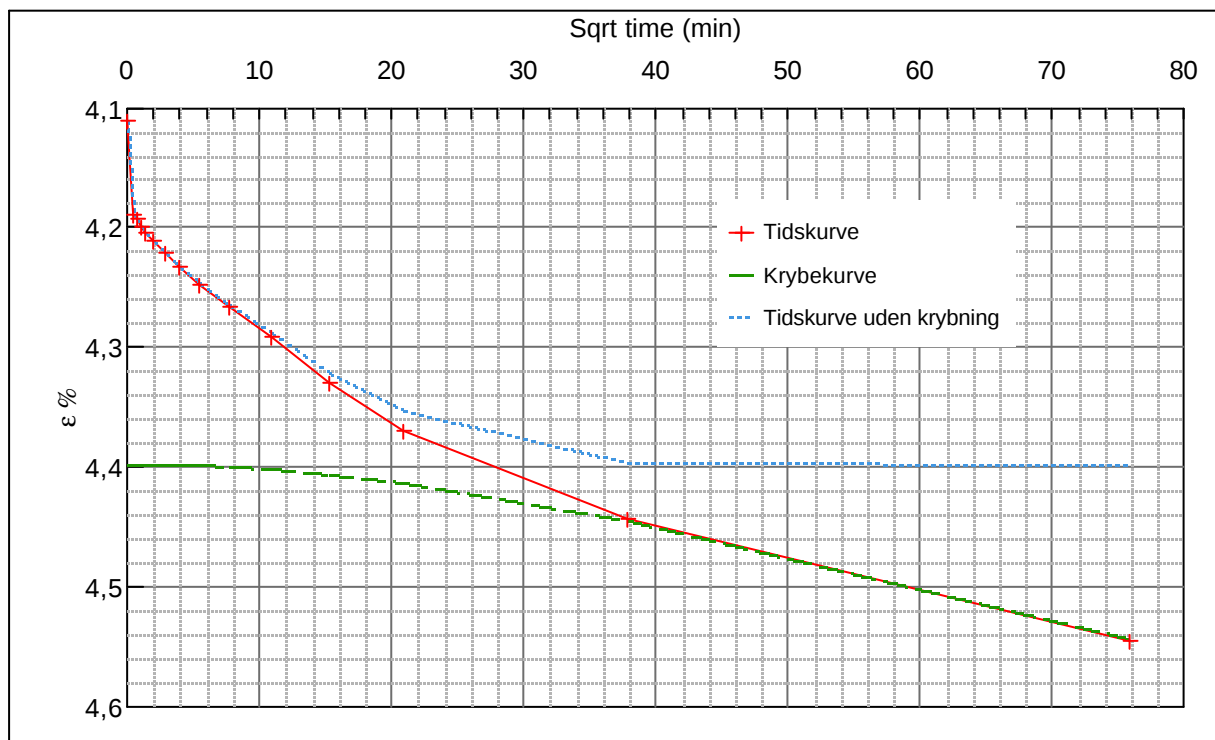
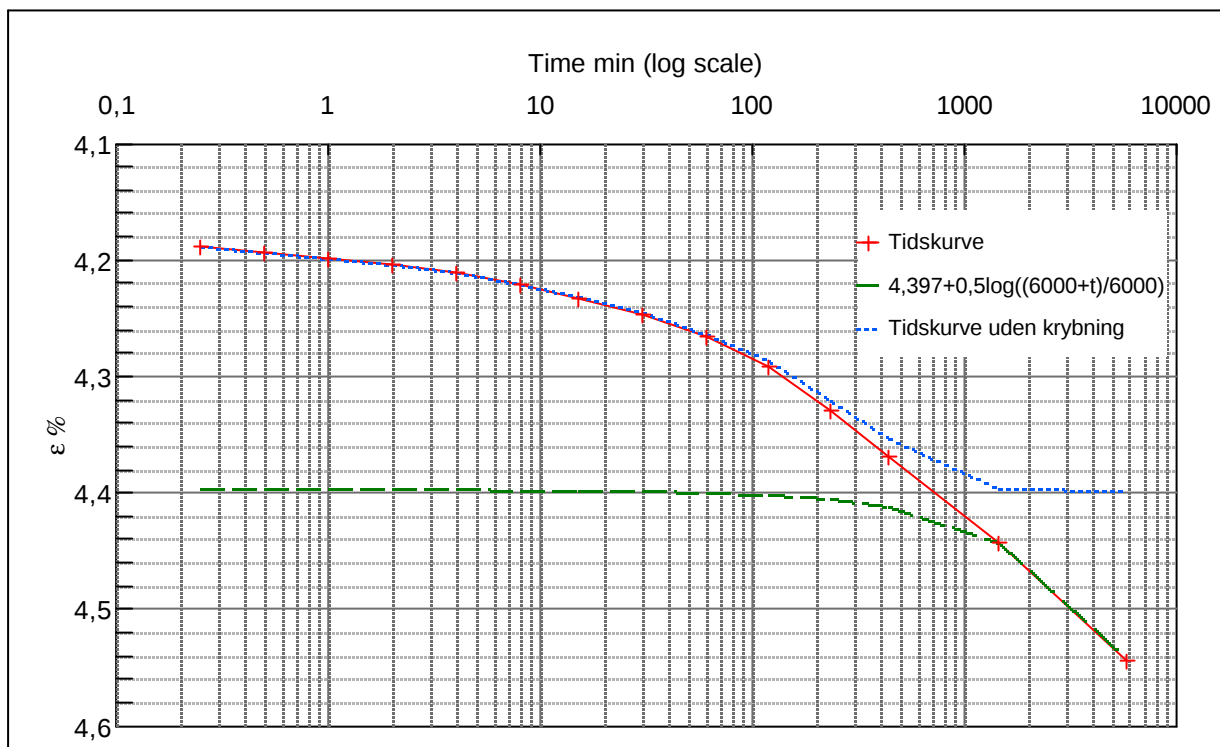
Step no 11	σ	kPa	ϵ	%	ϵ_i	ϵ_c %	ϵ_s	ϵ_{kryb}	tc in sec	29040	K i kPa	75.126	k10 m/sec	4,4E-12	ck10 m ² /sec	3,34E-08
	Before	1.702,5														
	After	2.049,5														



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.13
Executed:	AMS/mj/gt	Check:
Approved:		

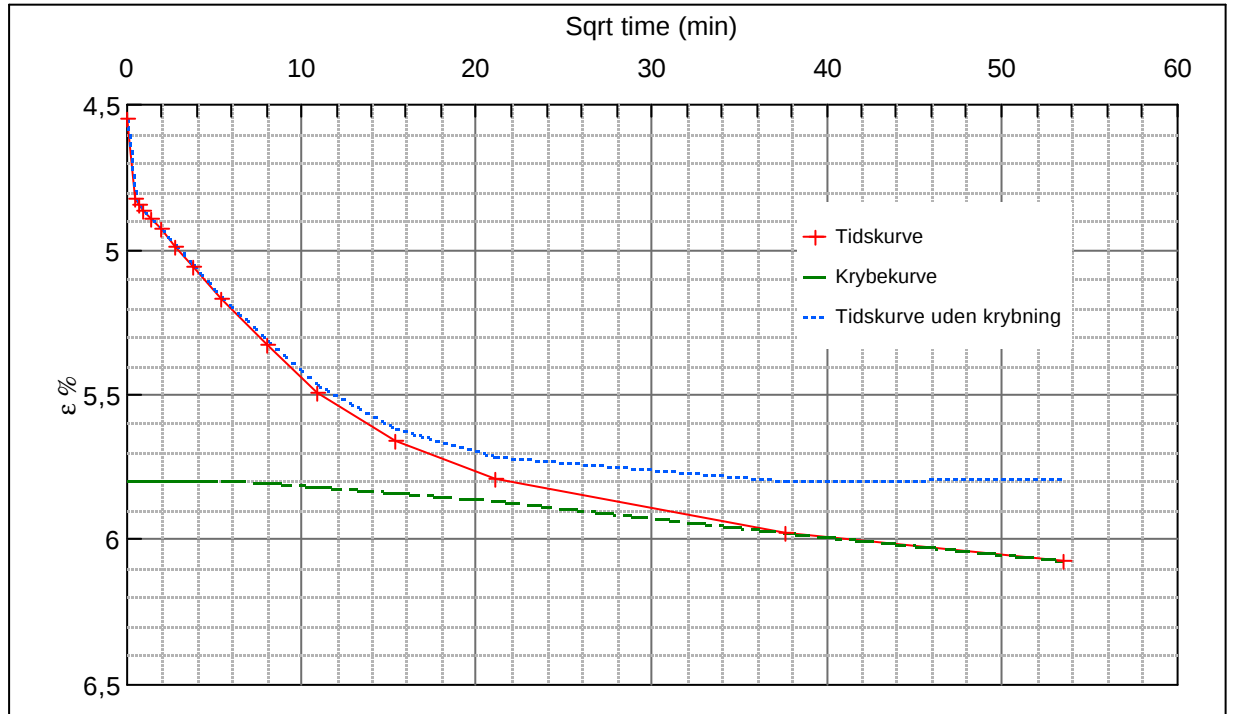
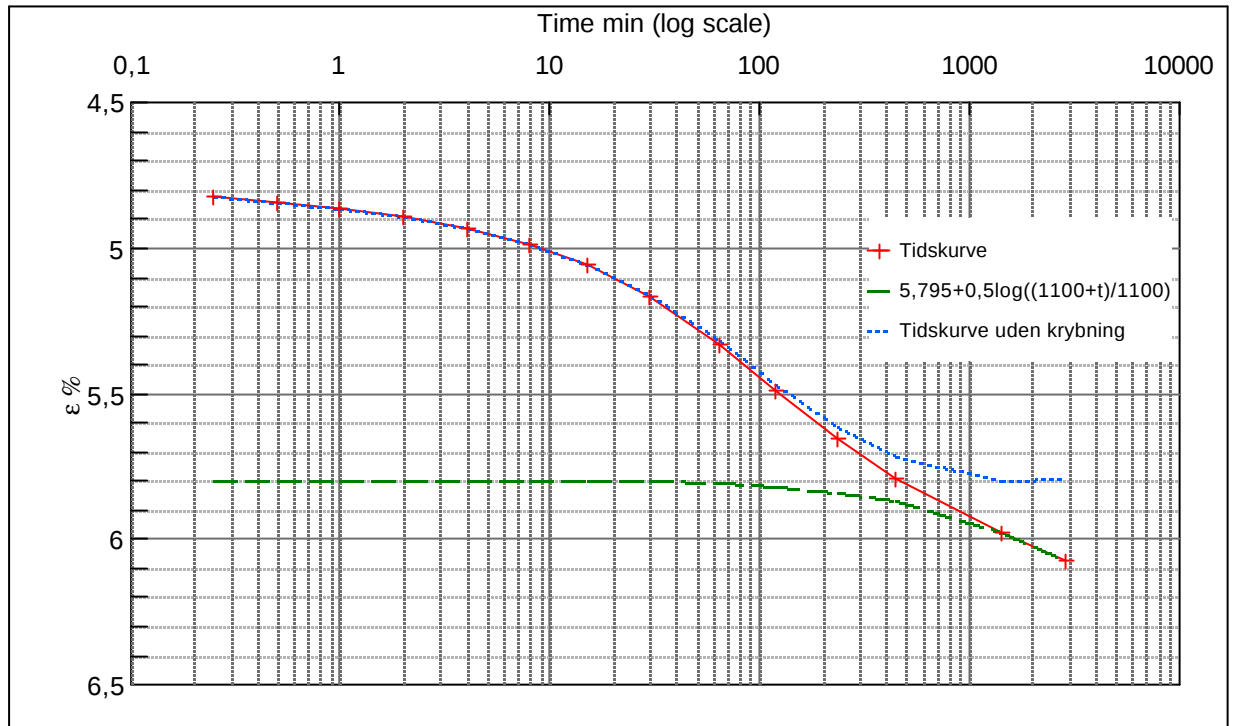
Step no 12	σ	kPa	ϵ	%	ϵ_i		tc in sec	31740
	Before	2.049,5	ϵ_0	4,11	ϵ_c %	4,40	K i kPa	121.102
	After	2.396,4	$\epsilon_{\sim\#}$	4,54	ϵ_s	0,17	k10 m/sec	2,5E-12
					ϵ_{kryb}	0,147	ck10 m^2 /sec	3,06E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.14
Executed:	AMS/mj/gt	Check:
Approved:		

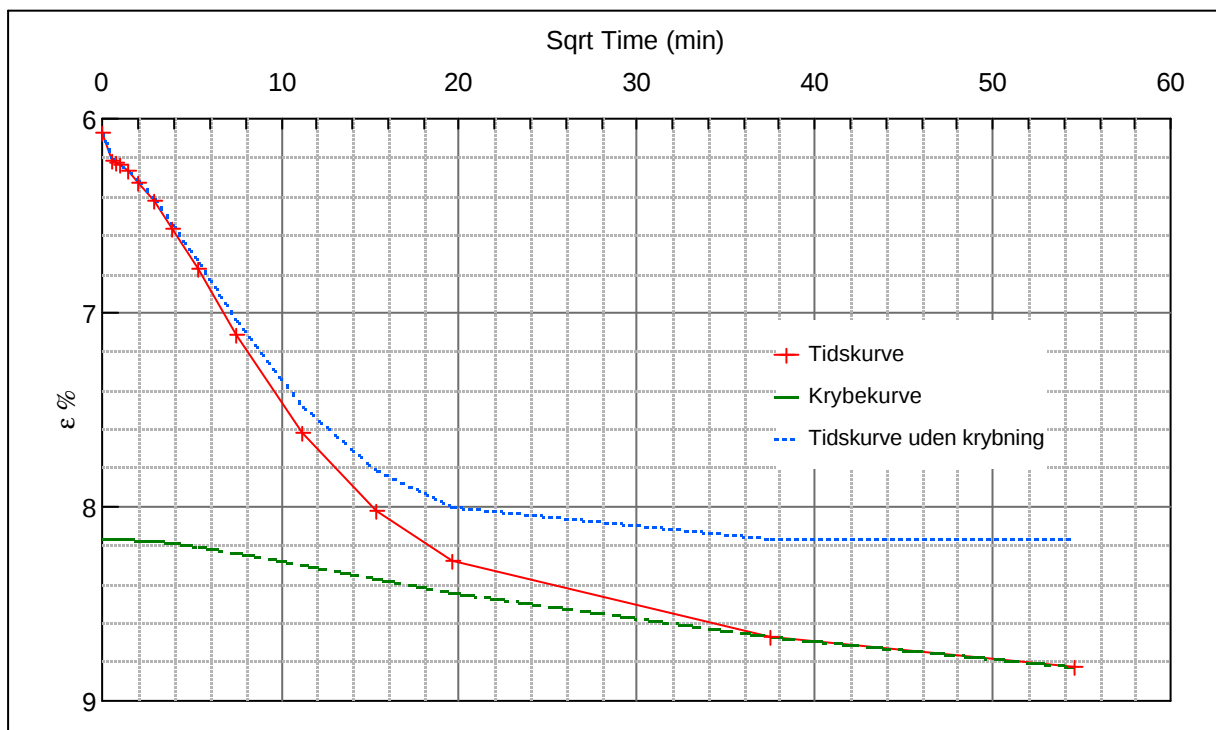
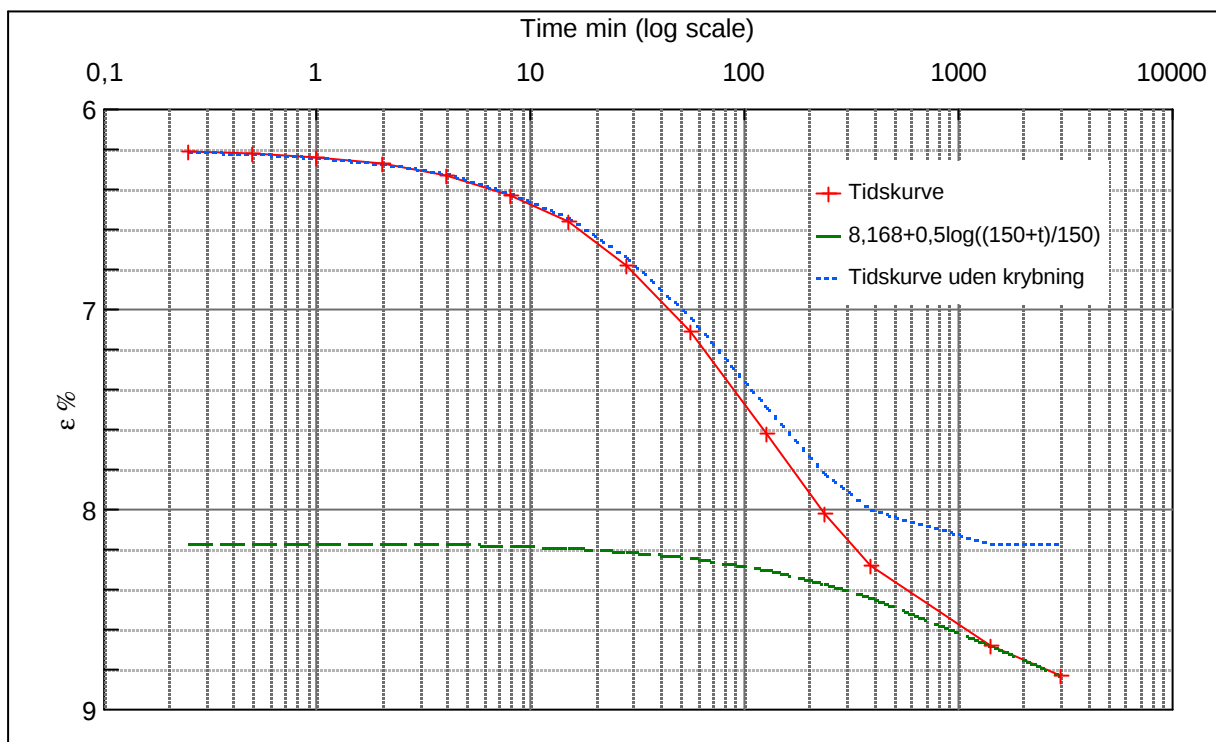
Step no 13	σ	kPa	ϵ	%	ϵ_i		tc in sec	13500
	Before	2.396,4	ϵ_0	4,54	ϵ_c %	5,80	K i kPa	83.203
	After	3.437,3	$\epsilon_{\sim\#}$	6,07	ϵ_s	0,33	k10 m/sec	8,5E-12
					ϵ_{kryb}	0,28	ck10 m ² /sec	7,18E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress.~780 kPa

Job:	Anholt	AAU
		Encl. No 3.15
Executed:	AMS/mj/gt	Check:
Approved:		

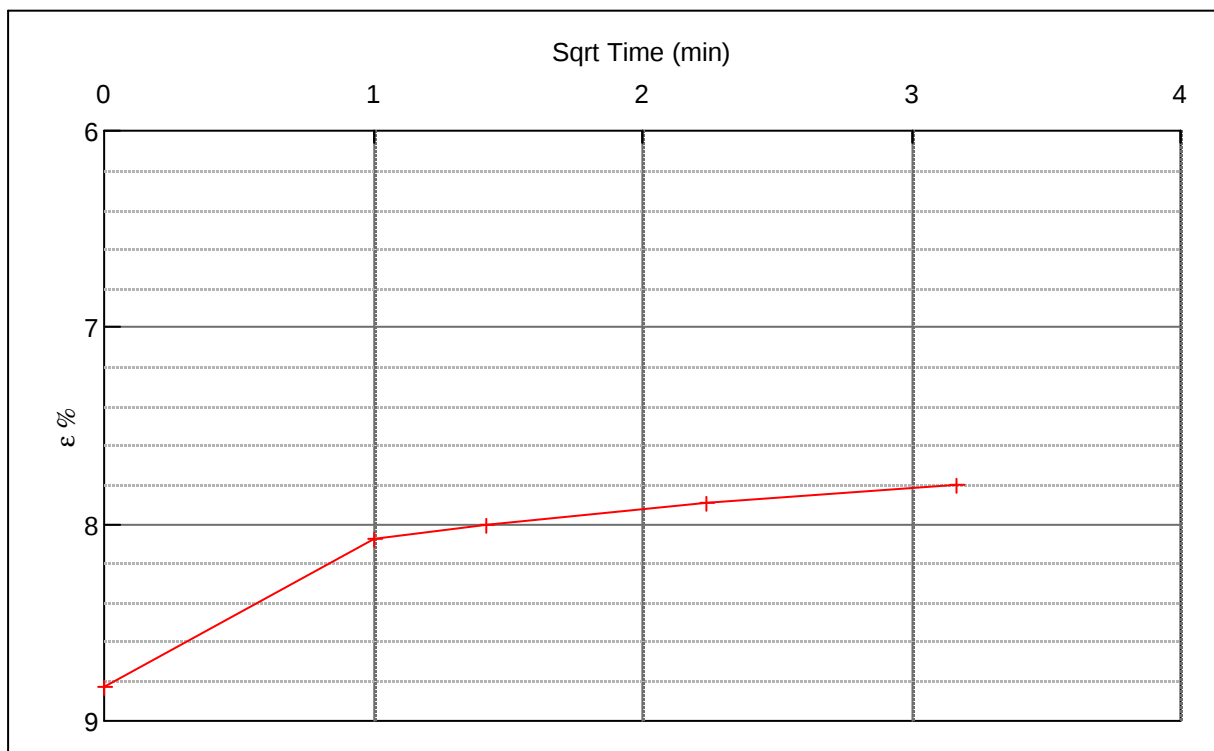
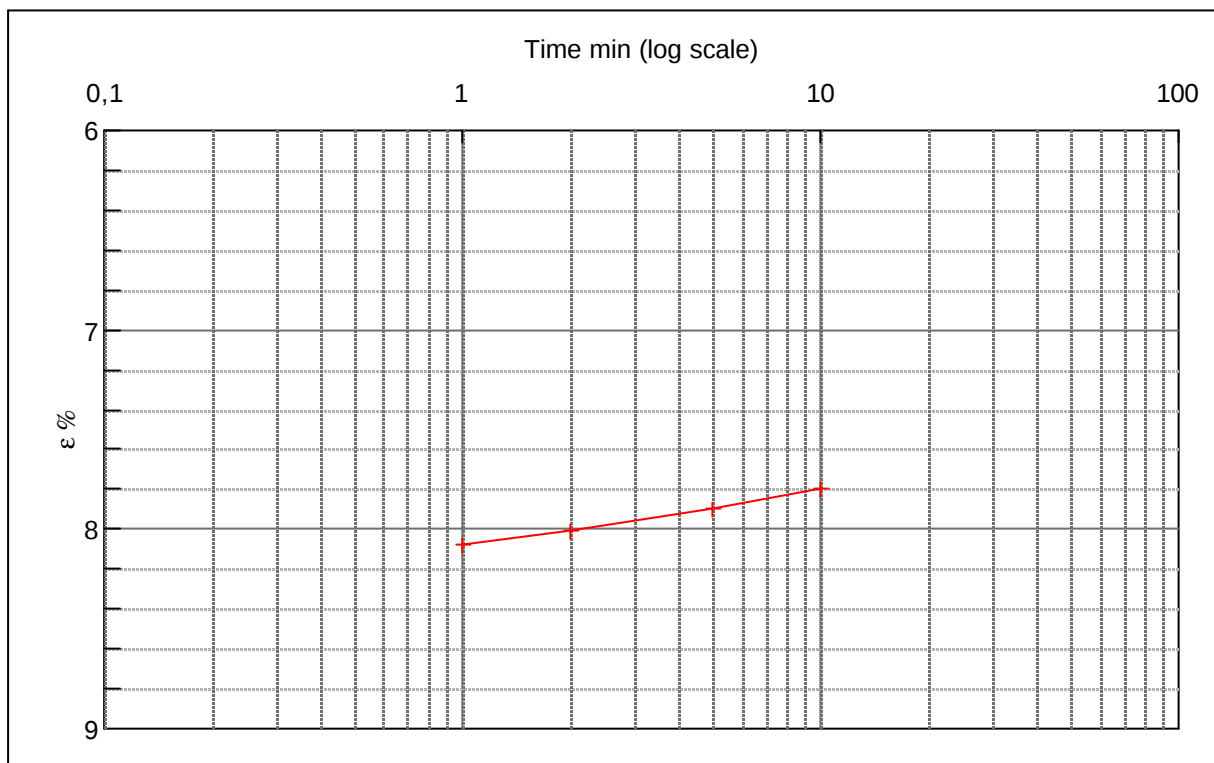
Step no 14	σ	kPa	ϵ	%	ϵ_i		tc in sec	11760
	Before	3.437,3	ϵ_0	6,07	ϵ_c %	8,17	K i kPa	99.320
	After	5.519,1	$\epsilon_{-#}$	8,83	ϵ_s	0,5	k10 m/sec	8,2E-12
					ϵ_{kryb}	0,659	ck10 m^2/sec	8,25E-08



Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.16
Executed:	AMS/mj/gt	Check:
Approved:		

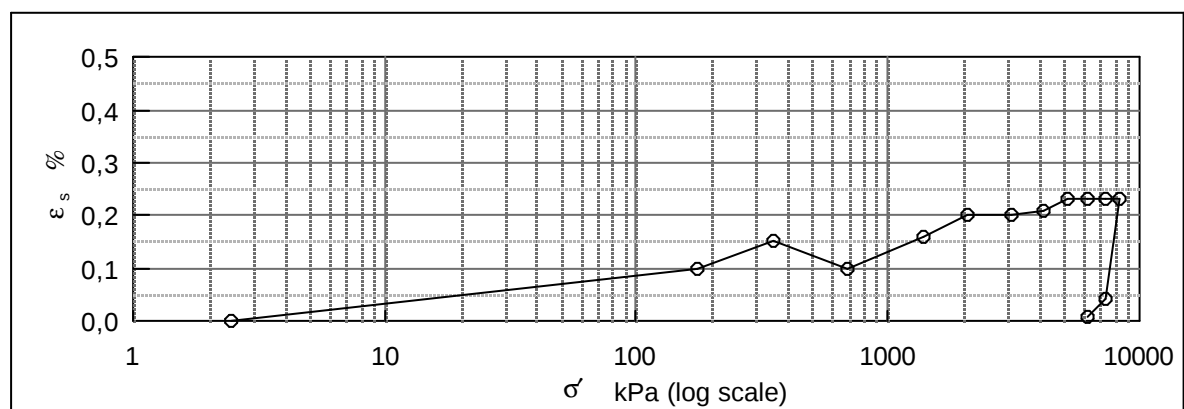
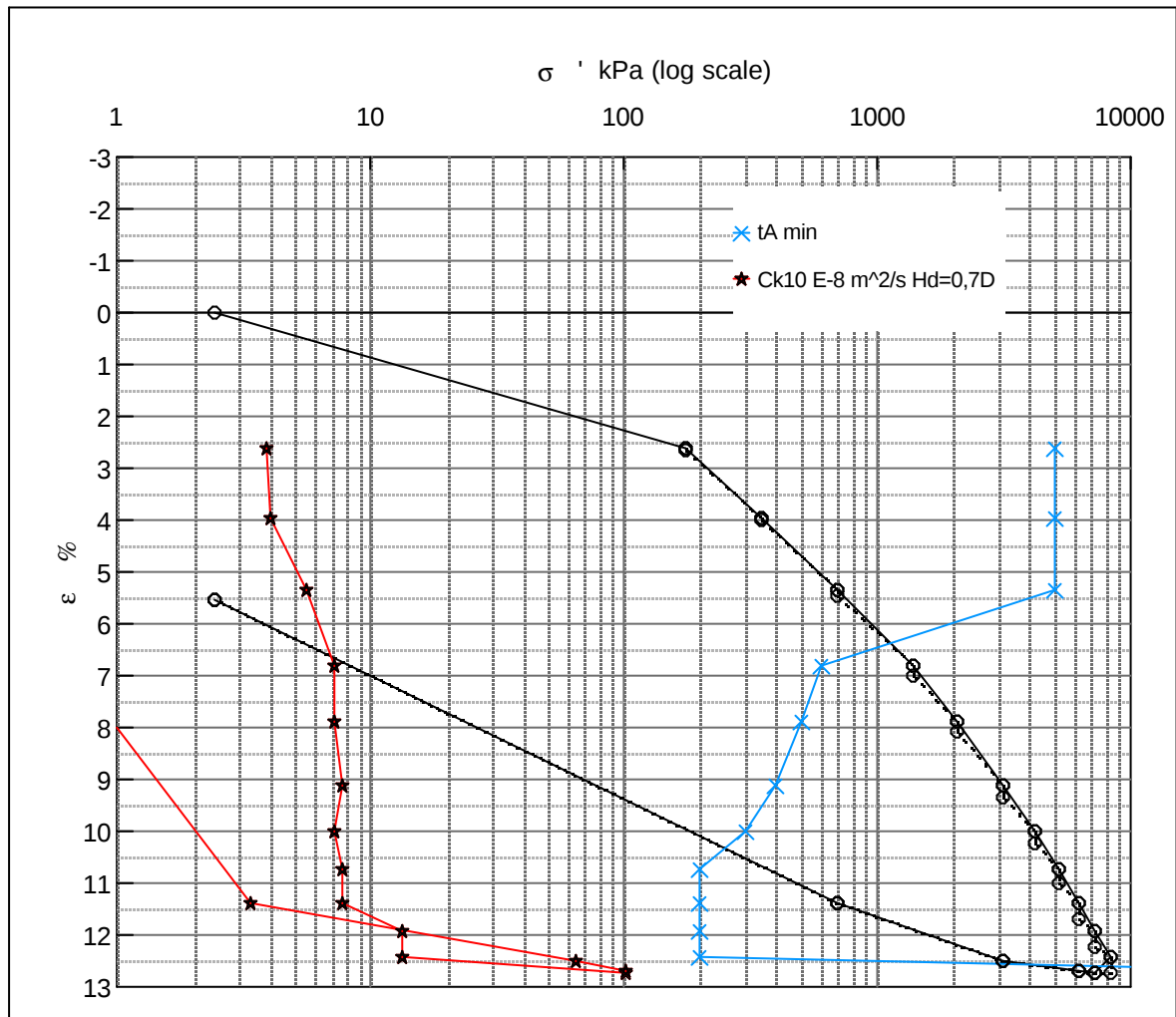
Step no 15	σ	kPa	ε	%	ε_i		tc in sec	
	Before	5.519	ε_0	8,83	ε_c %	7,8	K i kPa	536.985
	After	2,43	$\varepsilon_{-#}$	7,80	ε_s		k10 m/sec	
					ε_{kyb}		ck10 m ² /sec	



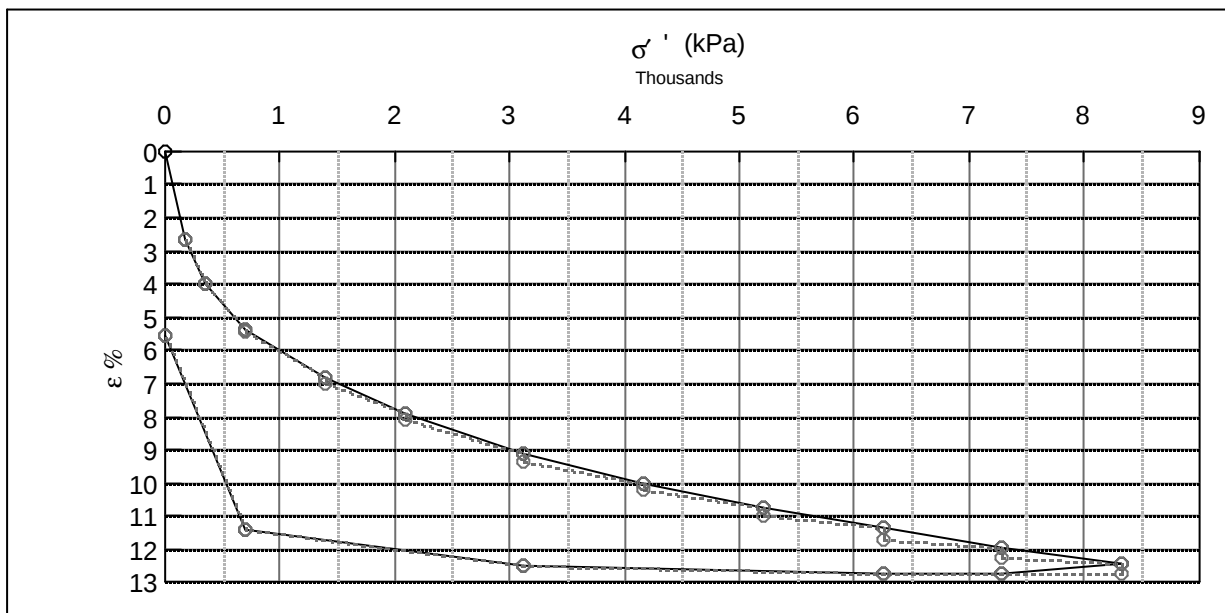
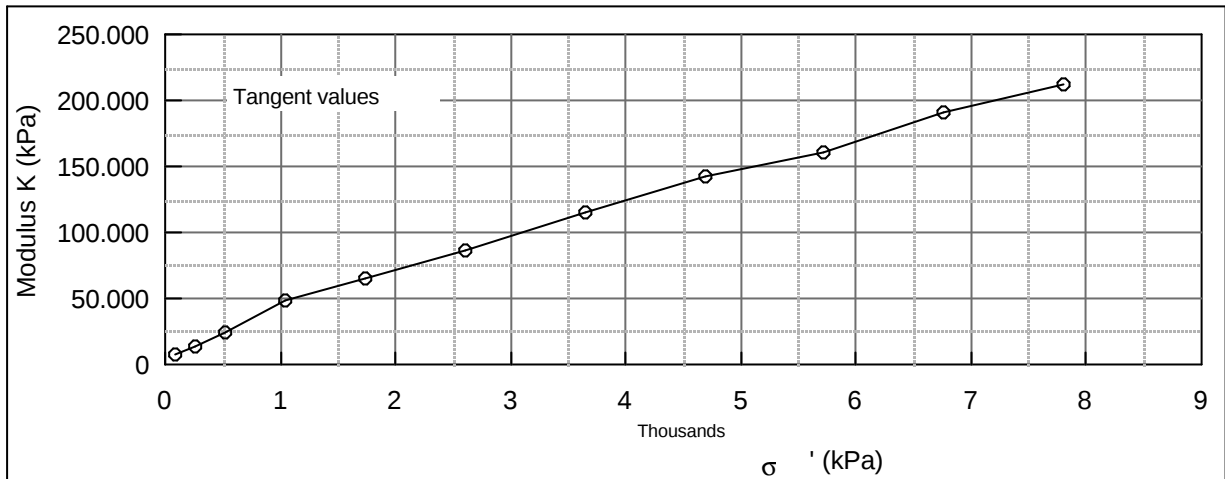
Material: Clay Eemian Glacial	
Bor no : Lab. no: P2	Depth: 76.7 m.b.s Insitu stress. ~780 kPa

Job:	Anholt	AAU
		Encl. No 3.17
Executed:	AMS/mj/gt	Check:
Approved:		

Description of soil: Clay Eemian Glacial			Water content %	Before	After
			Bulk density Mg/m ³	17,8	15,5
			Grain density Mg/m ³	2,17	2,21
			Void ratio	~2.72	0,48
Bor no :	Overburden pressure σ'_o	~800 kPa	Degr. of Saturation %	0,48	0,42
Lab. no: k12	Vane strength c_v	kPa	Dimension H x D mm	~96	~100
Level : 78 m.b.s.	CPT - value q_c	MPa		30x60	28.8x60



Job: Anholt		AAU
		Encl. No 4.1
Executed:	AMS/gt	Check:
Approved:		



Test results		σ' kPa	ϵ_c %	ϵ_s % / lct	C k10 m ² /s	σ'_m kPa	K kPa	w %
Q	~8 %	2,4	0,00	0,00	-	-	-	18,5
Qs	~0.23 %	175,9	2,64	0,10	3,8E-08	89,2	6571,2	17,1
σ'_{pc}	~5000 kPa	349,4	3,96	0,15	4,0E-08	262,6	13142,3	16,4
		696,3	5,37	0,10	5,6E-08	522,9	24606,9	15,6
		1.390,3	6,82	0,16	7,2E-08	1.043,3	47856,2	14,8
		2.084,2	7,90	0,20	7,2E-08	1.737,2	64251,4	14,2
		3.125,0	9,10	0,20	7,7E-08	2.604,6	86739,4	13,6
		4.165,9	10,00	0,21	7,2E-08	3.645,5	115652,6	13,1
		5.206,8	10,73	0,23	7,7E-08	4.686,4	142585,4	12,7
		6.247,7	11,38	0,23	7,7E-08	5.727,2	161375,7	12,3
		7.288,5	11,92	0,23	1,3E-07	6.768,1	190985,9	12,0
		8.329,4	12,41	0,23	1,3E-07	7.809,0	212423,1	11,8
		7.288,5	12,73	0,04	1,0E-06	7.809,0	-328869,9	11,6
		6.247,7	12,71	0,01	1,0E-06	6.768,1	7178436,7	11,6
		3.125,0	12,51		6,5E-07	4.686,4	1530696,1	11,7
		696,3	11,40		3,3E-08	1.910,7	219593,5	12,3
		2,4	5,54		4,2E-09	349,4	11827,4	15,5

Remark:

Job: Anholt

AAU

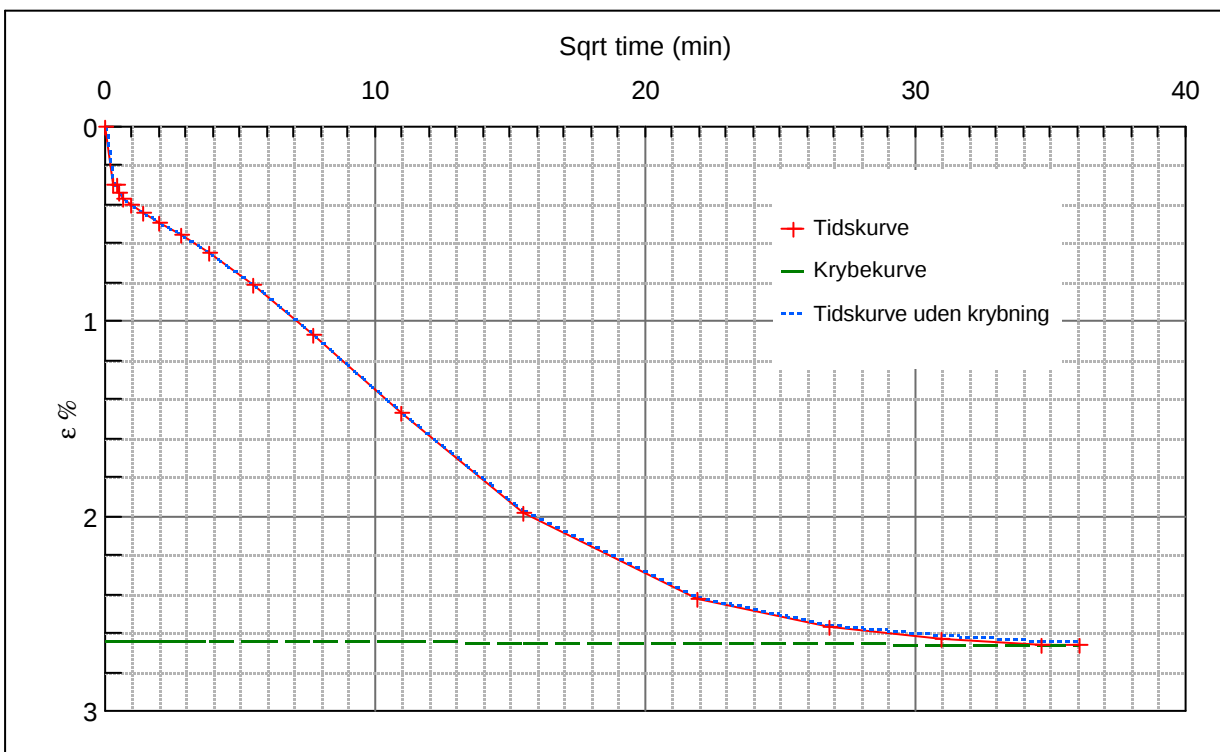
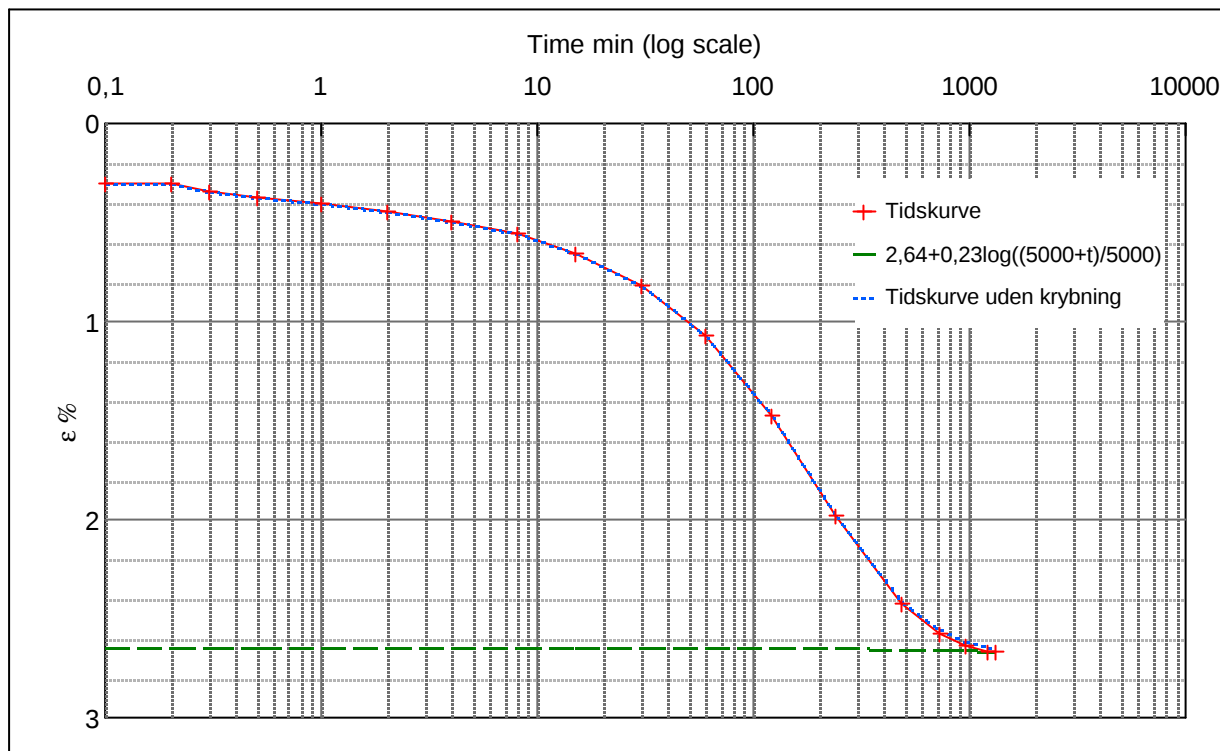
Encl. No
4.2

Executed: AMS/gt

Check:

Approved:

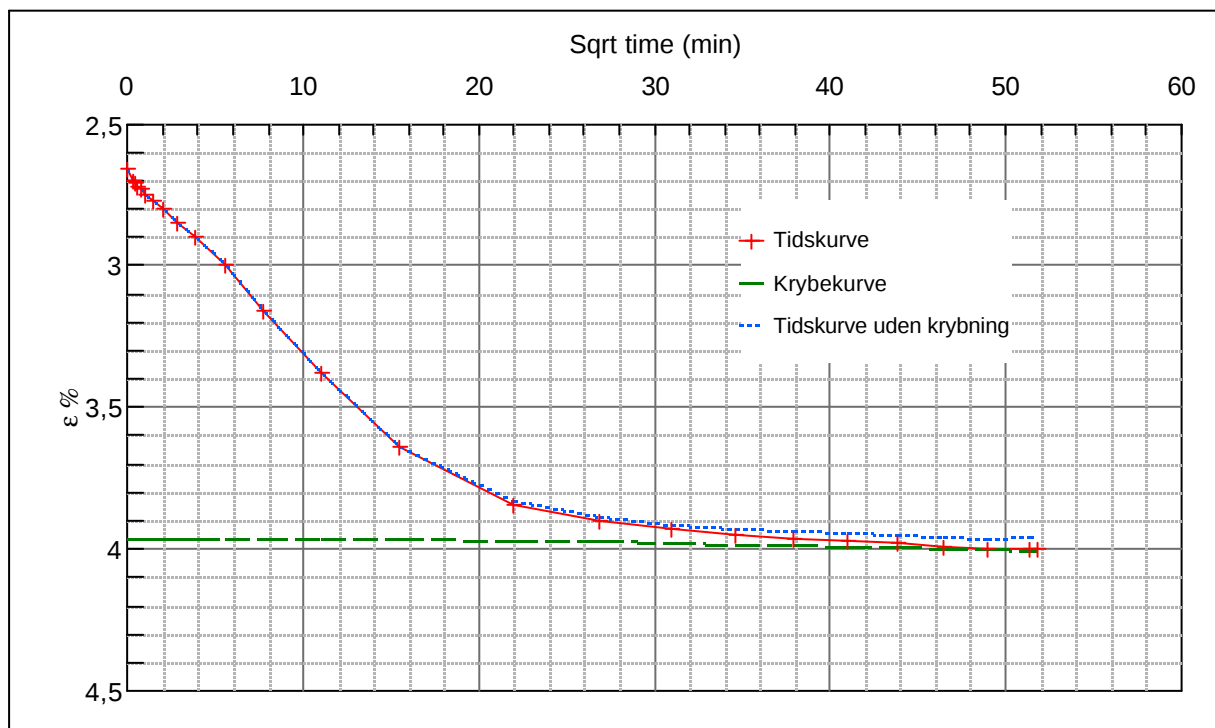
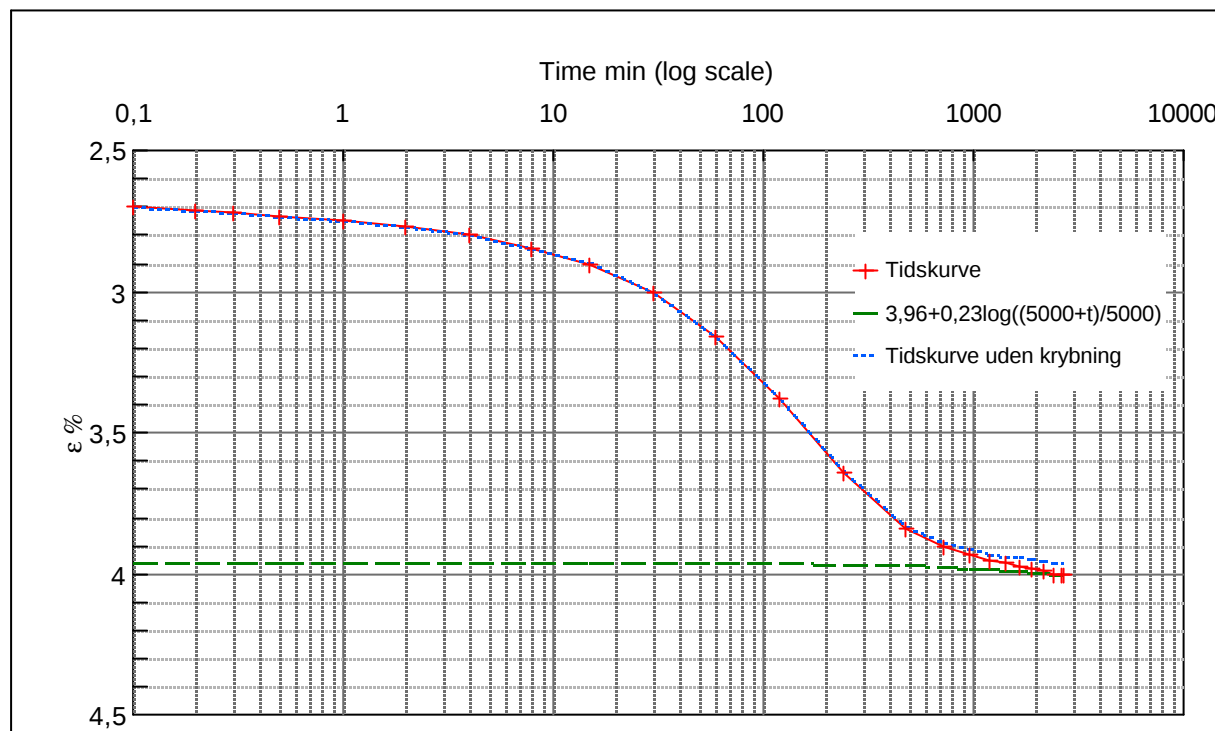
Step no 1	σ	kPa	ϵ	%	ϵ_i		tc in sec	25215
	Before	2,43	ϵ_0	0,00	ϵ_c %	2,64	K i kPa	6.571
	After	175,9	$\epsilon_{\sim\#}$	2,66	ϵ_s	0,1	k10 m/sec	5,7E-11
					ϵ_{kryb}	0,02	ck10 m ² /sec	3,85E-08



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress: ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.3
Executed:	AMS/gt	Check:
Approved:		

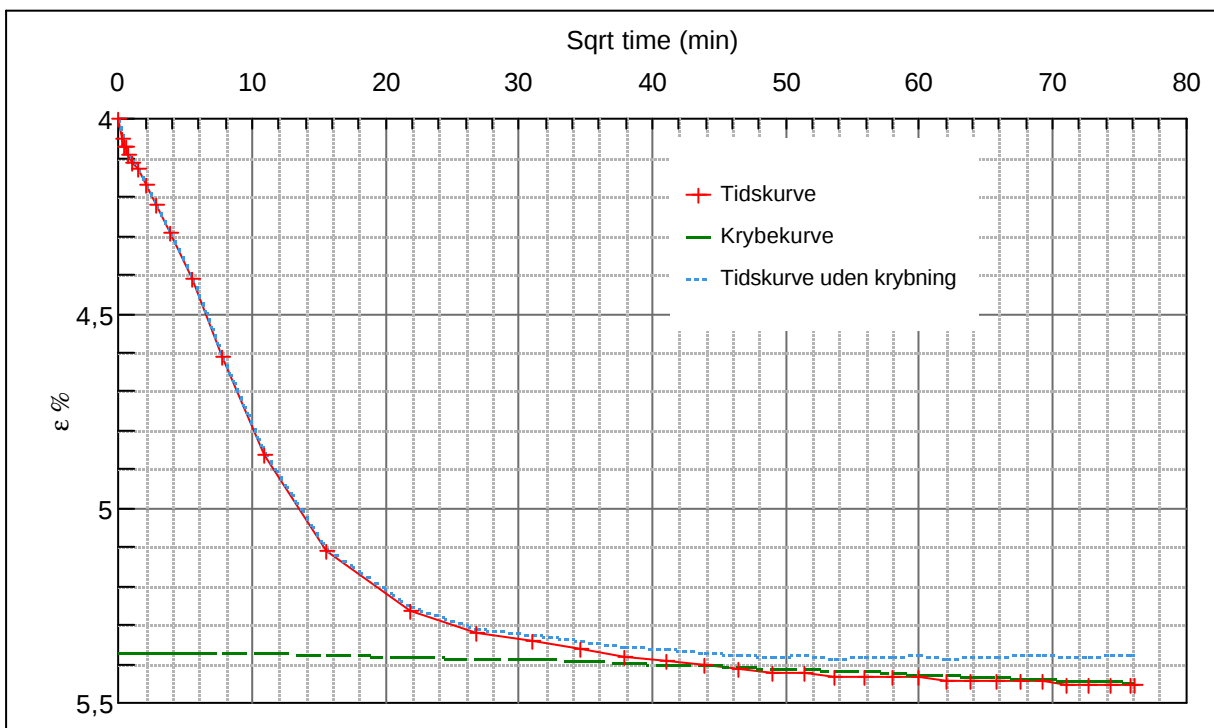
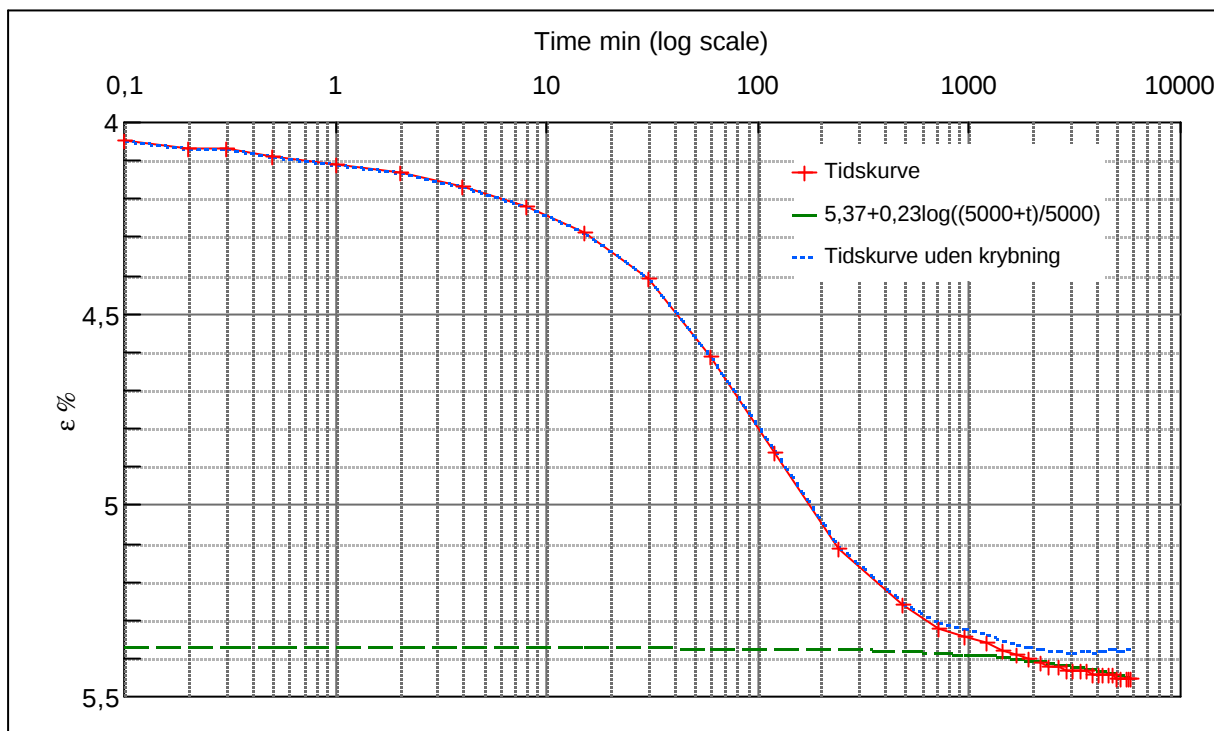
Step no 2	σ	kPa	ε	%	ε_i		tc in sec	24000
	Before	175,9	ε_0	2,66	ε_c %	3,96	K i kPa	13.345
	After	349,4	$\varepsilon_{-#}$	4,00	ε_s	0,15	k10 m/sec	3,0E-11
					ε_{kryb}	0,04	ck10 m ² /sec	4,04E-08



Material:		
	Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress: ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.4
Executed:	AMS/gt	Check:
Approved:		

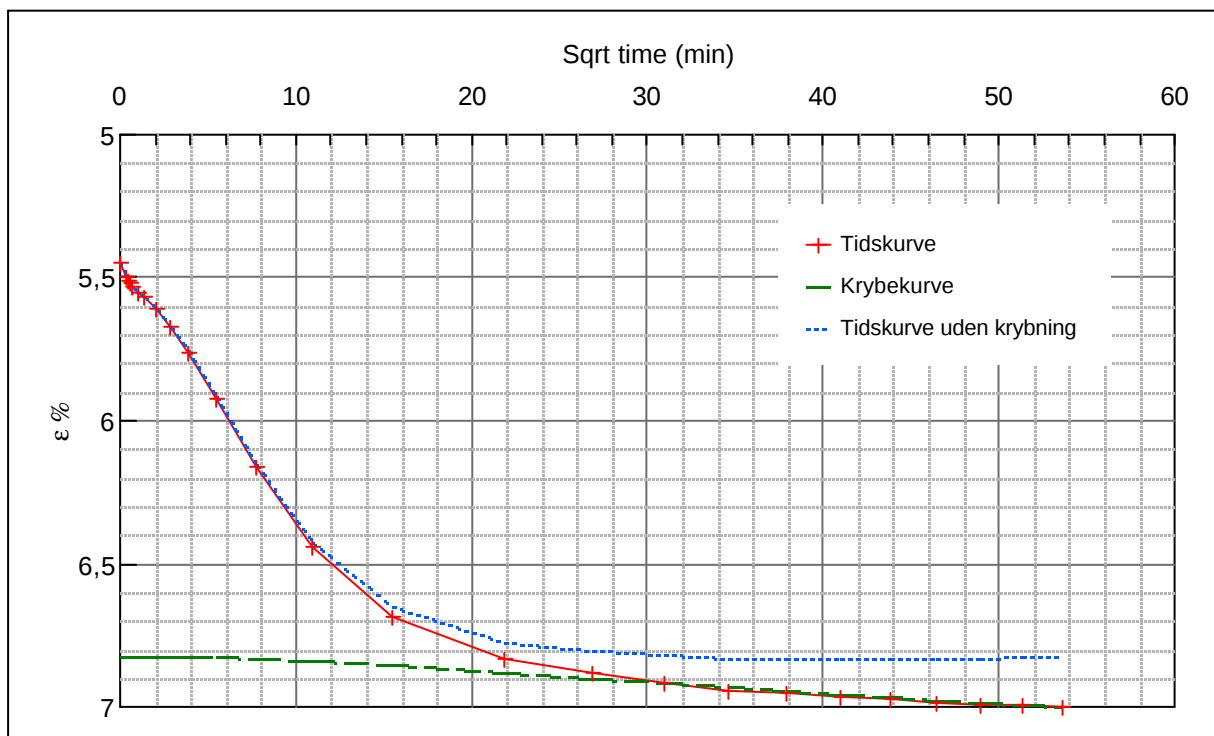
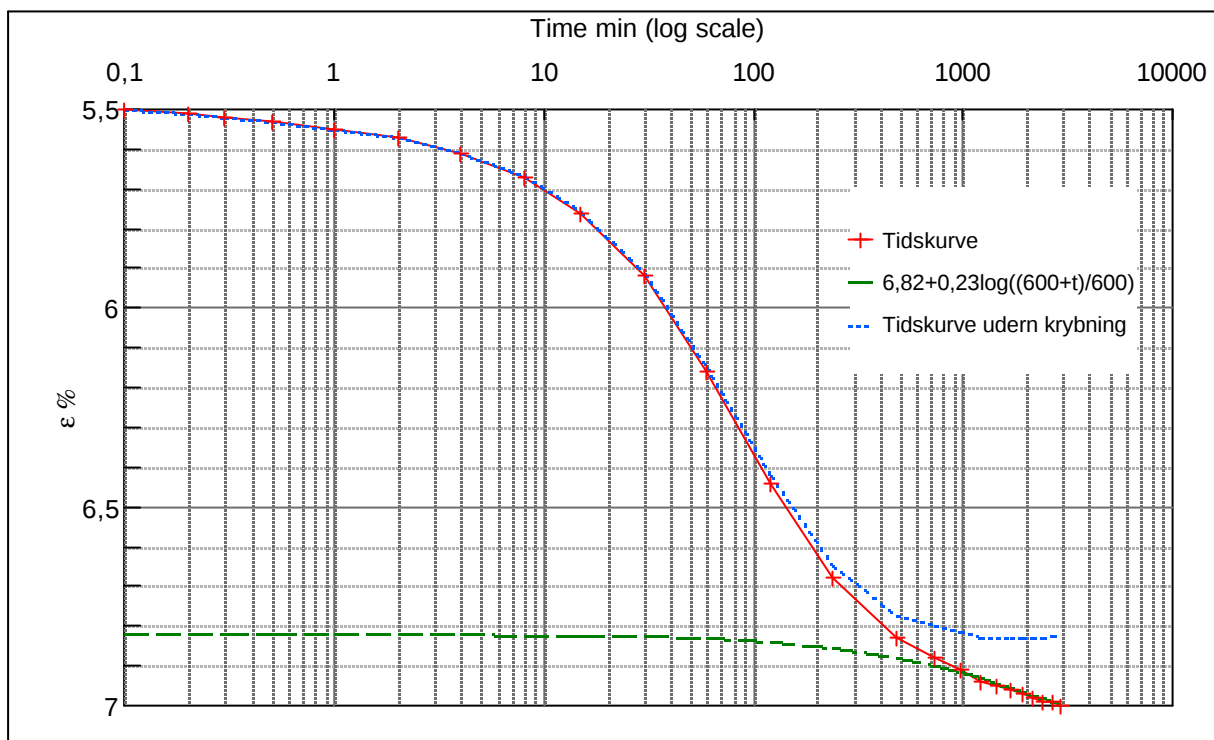
Step no 3	σ	kPa	ϵ	%	ϵ_i		tc in sec	17340
	Before	349,4	ϵ_0	4,00	ϵ_c %	5,37	K i kPa	25.325
	After	696,3	$\epsilon_{\sim\#}$	5,45	ϵ_s	0,1	k10 m/sec	2,2E-11
					ϵ_{kryb}	0,08	ck10 m ² /sec	5,59E-08



Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.5
Executed:	AMS/gt	Check:
Approved:		

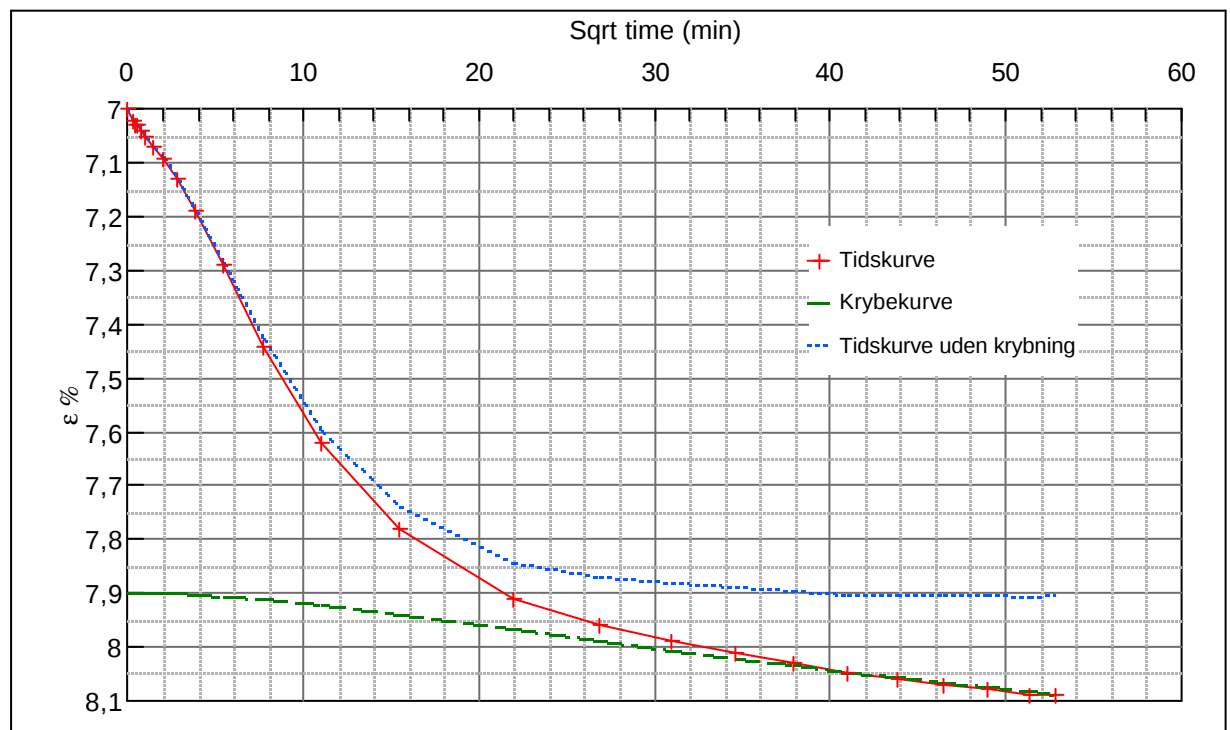
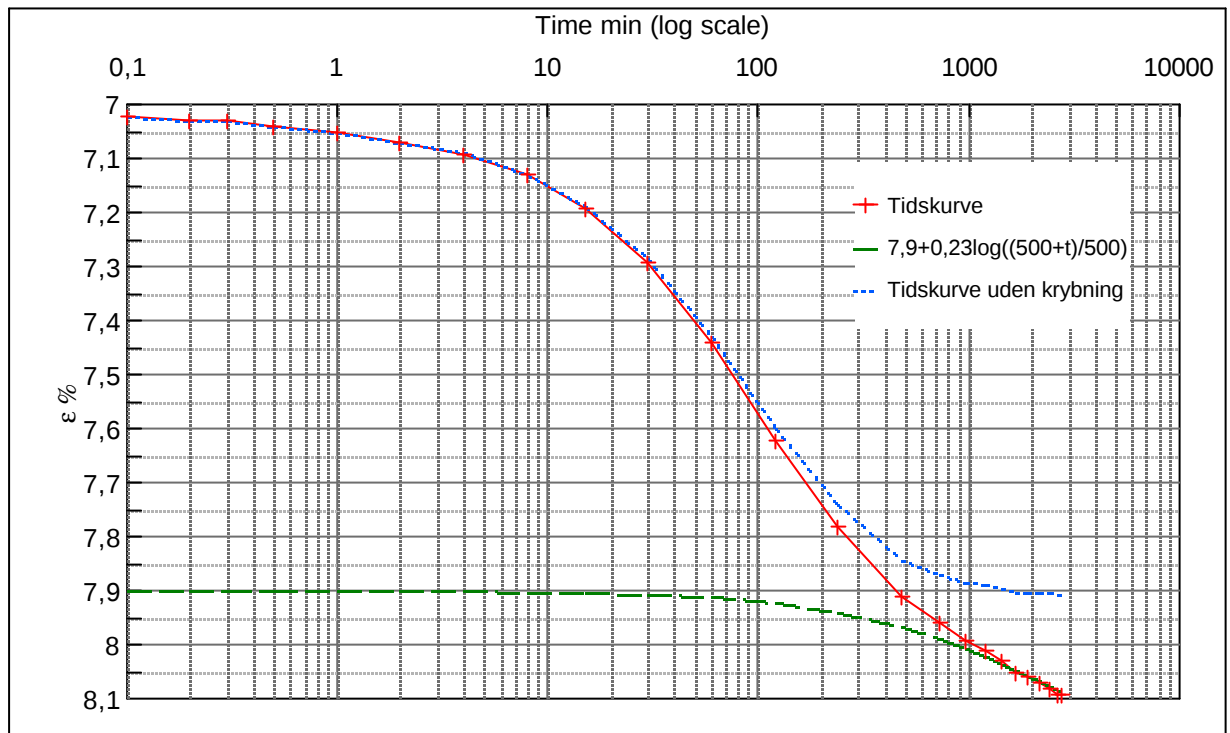
Step no 4	σ	kPa	ϵ	%	ϵ_i		tc in sec	13500
	Before	696,3	ϵ_0	5,450	ϵ_c %	6,82	K i kPa	50.651
	After	1.390,3	$\epsilon_{-#}$	7,00	ϵ_s	0,16	k10 m/sec	1,4E-11
					ϵ_{kryb}	0,18	ck10 m ² /sec	7,18E-08



Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.6
Executed:	AMS/gt	Check:
Approved:		

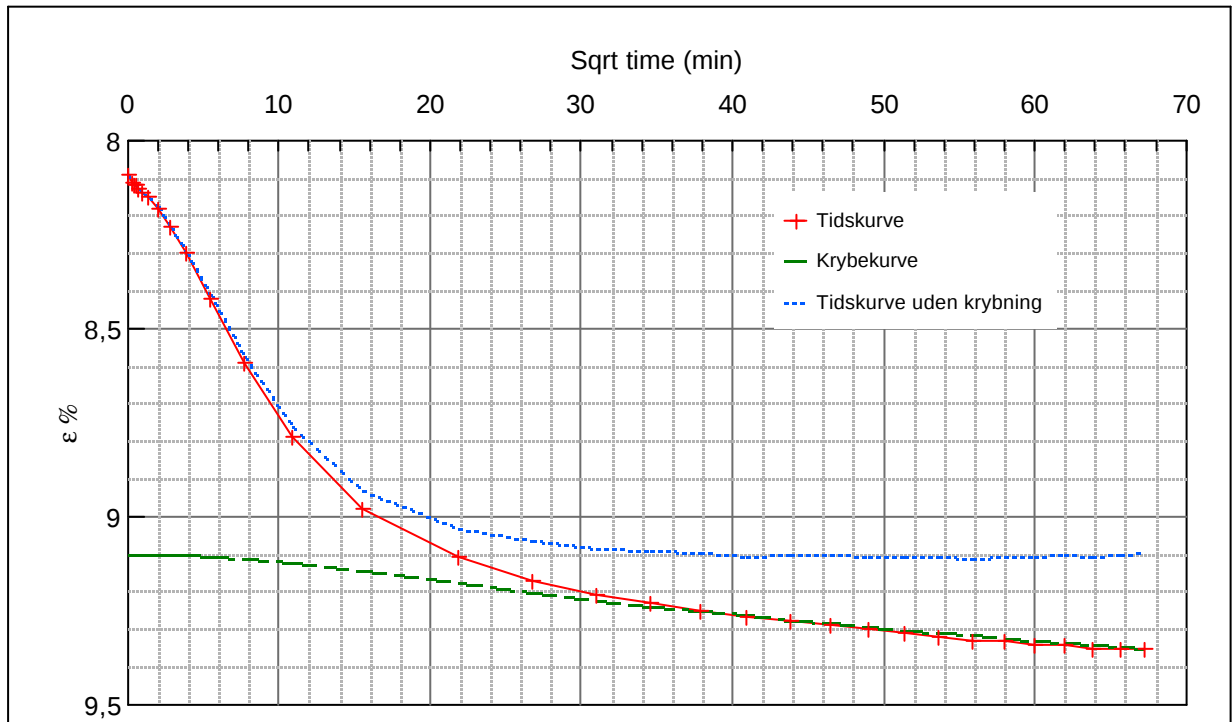
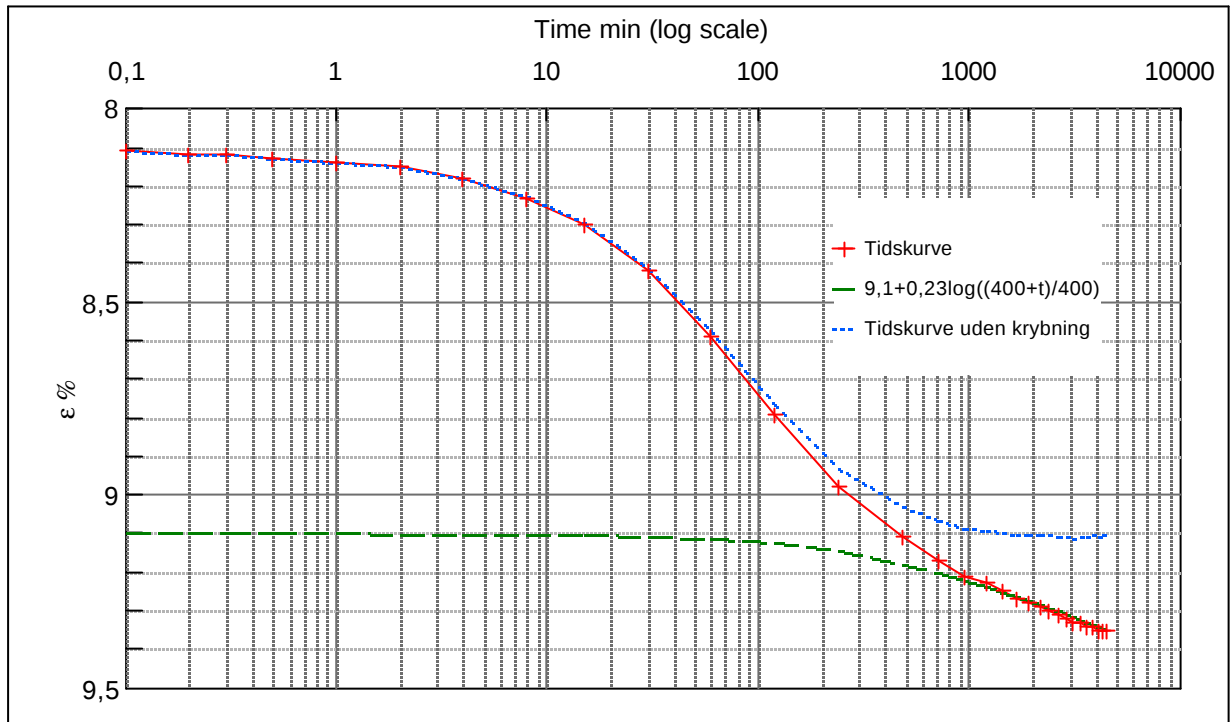
Step no 5	σ	kPa	ϵ	%	ϵ_i		tc in sec	13500
	Before	1.390,3	ϵ_0	7,00	ϵ_c %	7,9	K i kPa	77.102
	After	2.084,2	$\epsilon_{-#}$	8,09	ϵ_s	0,2	k10 m/sec	9,1E-12
					ϵ_{kryb}	0,19	ck10 m^2/sec	7,18E-08



Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.7
Executed:	AMS/gt	Check:
Approved:		

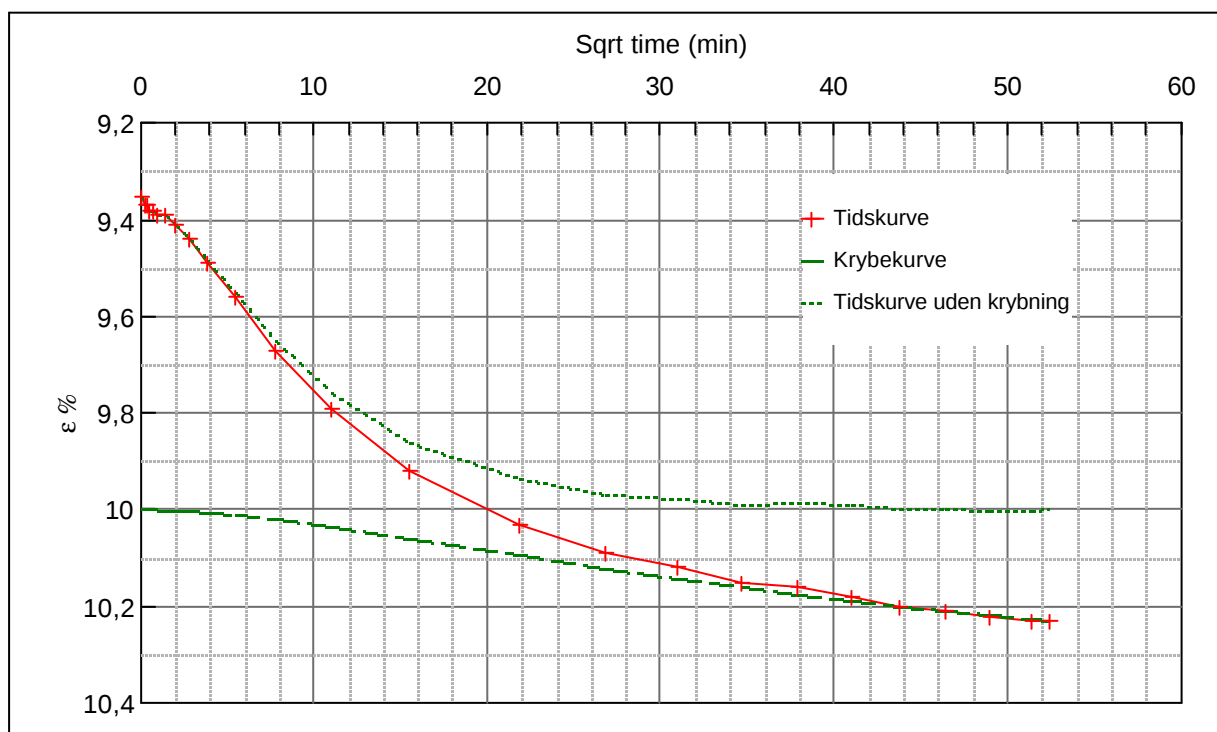
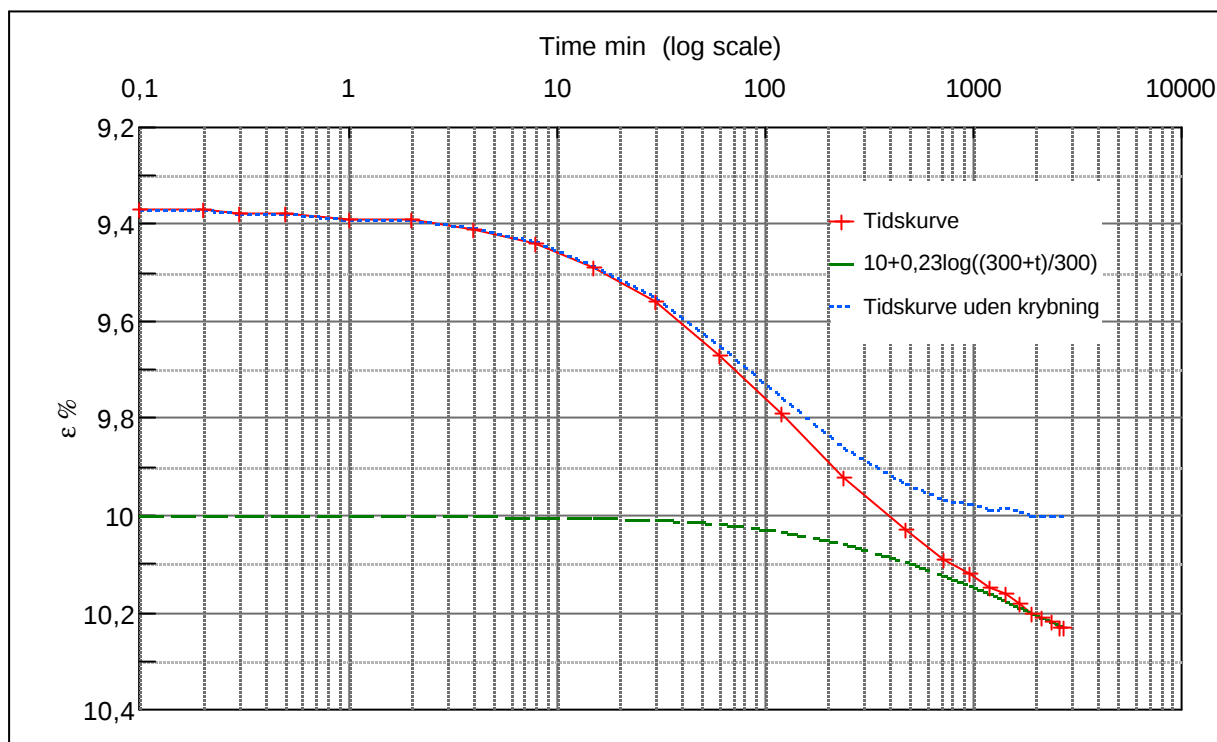
Step no 6	σ	kPa	ϵ	%	ϵ_i		tc in sec	12615
	Before	2.084,2	ϵ_0	8,09	ϵ_c %	9,1	K i kPa	103.057
	After	3.125,0	$\epsilon_{\sim\#}$	9,35	ϵ_s	0,2	k10 m/sec	7,3E-12
					ϵ_{kryb}	0,25	ck10 m ² /sec	7,69E-08



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.8
Executed:	AMS/gt	Check:
Approved:		

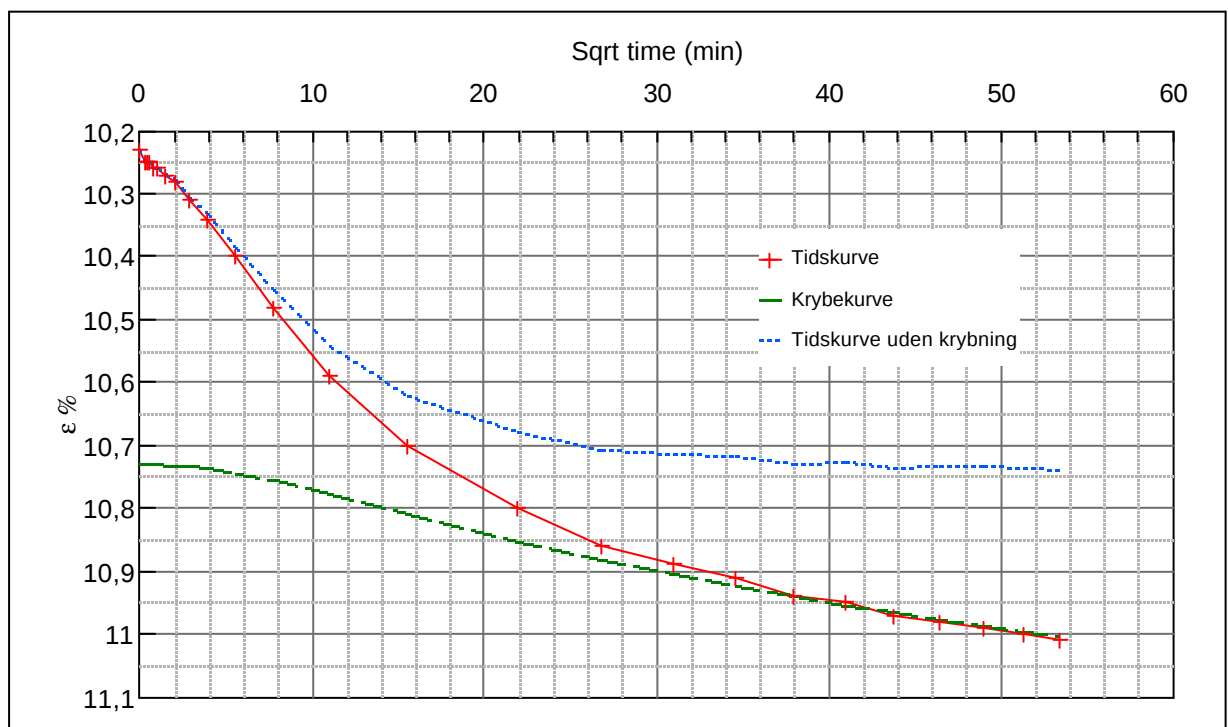
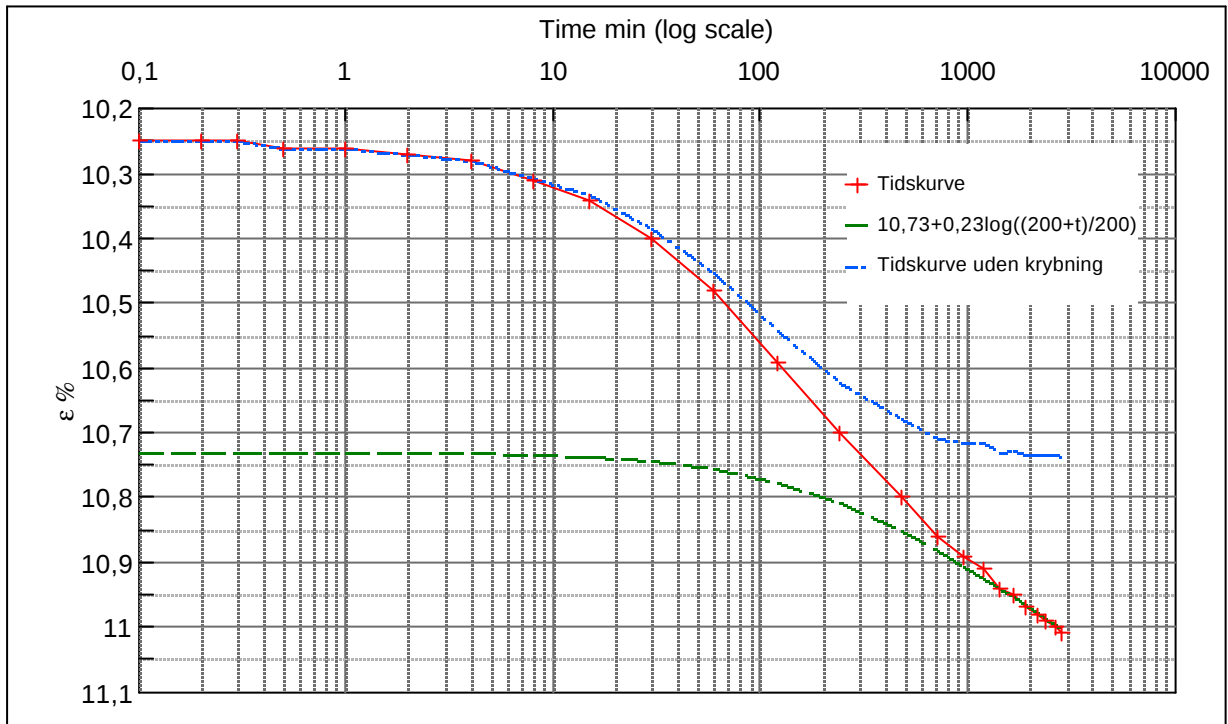
Step no 7	σ	kPa	ϵ	%	ϵ_i		tc in sec	13500
	Before	3.125,0	ϵ_0	9,35	ϵ_c %	10	K i kPa	160.134
	After	4.165,9	$\epsilon_{-#}$	10,23	ϵ_s	0,21	k10 m/sec	4,4E-12
					ϵ_{kryb}	0,23	ck10 m^2/sec	7,18E-08



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress: ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.9
Executed:	AMS/gt	Check:
Approved:		

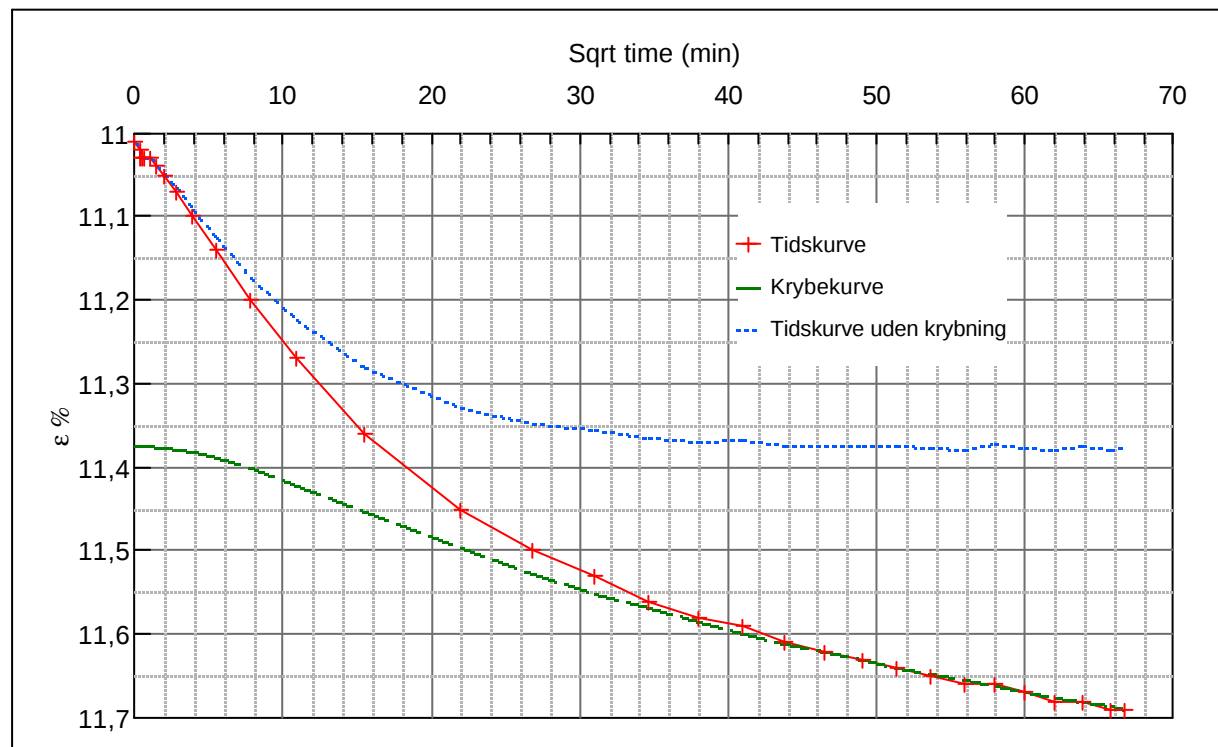
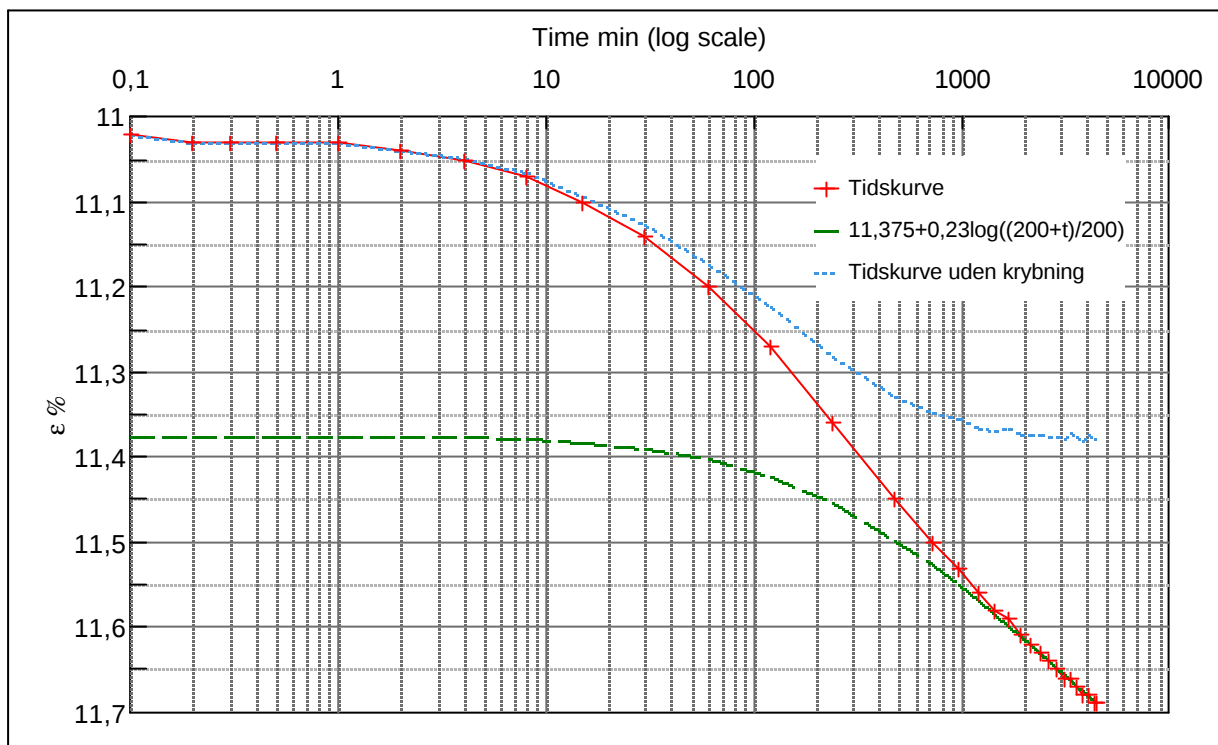
Step no 8	σ	kPa	ϵ	%	ϵ_i		tc in sec	12615
	Before	4.165,92	ϵ_0	10,23	ϵ_c %	10,73	K i kPa	208.175
	After	5.206,80	$\epsilon_{\sim\#}$	11,01	ϵ_s	0,23	k10 m/sec	3,6E-12
					ϵ_{kryb}	0,28	ck10 m ² /sec	7,69E-08



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.10
Executed:	AMS/gt	Check:
Approved:		

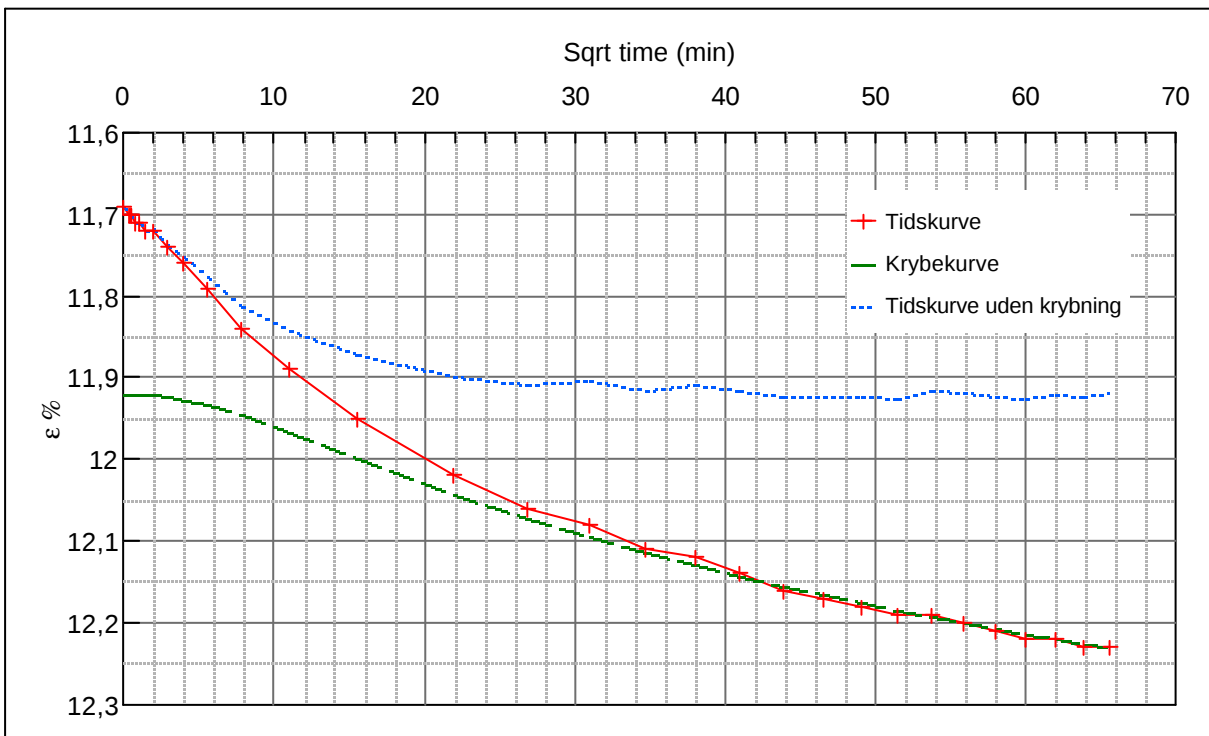
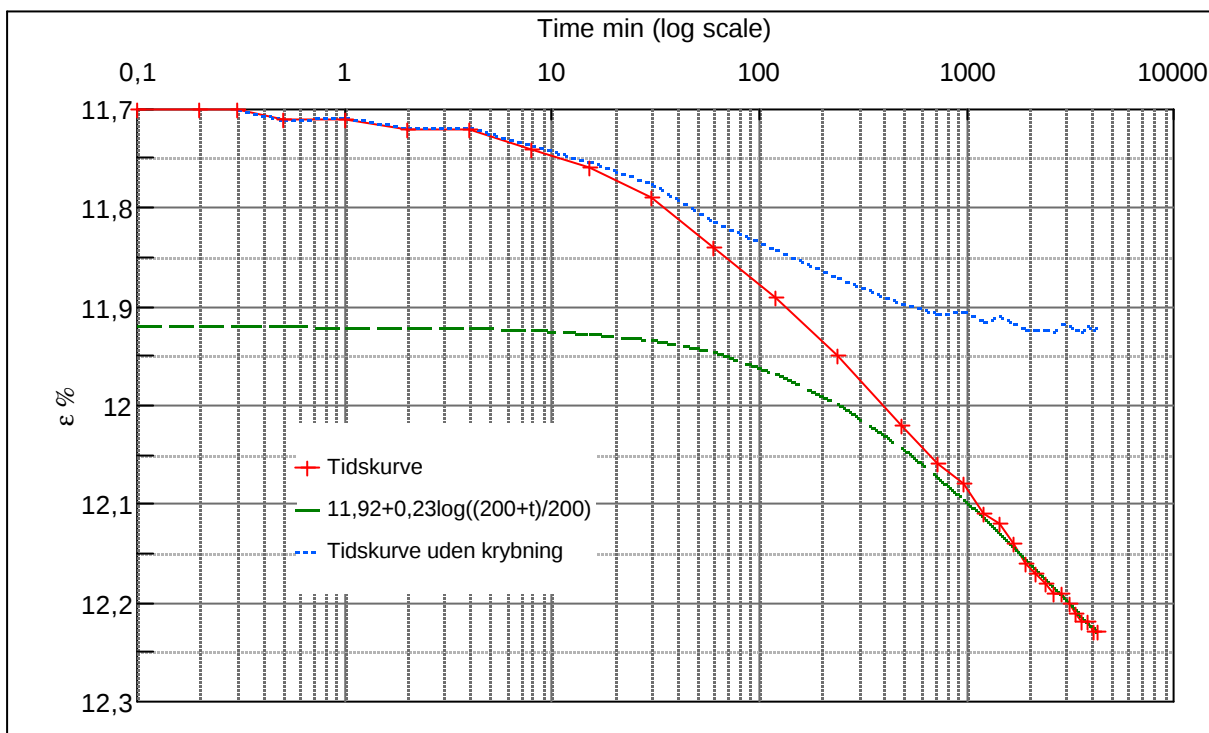
Step no 9	σ	kPa	ϵ	%	ϵ_i		tc in sec	12615
	Before	5.206,8	ϵ_0	11,01	ϵ_c %	11,38	K i kPa	285.171
	After	6.247,7	$\epsilon_{\sim\#}$	11,69	ϵ_s	0,23	k10 m/sec	2,6E-12
					ϵ_{kryb}	0,315	ck10 m^2 /sec	7,69E-08



Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.11
Executed:	AMS/gt	Check:
Approved:		

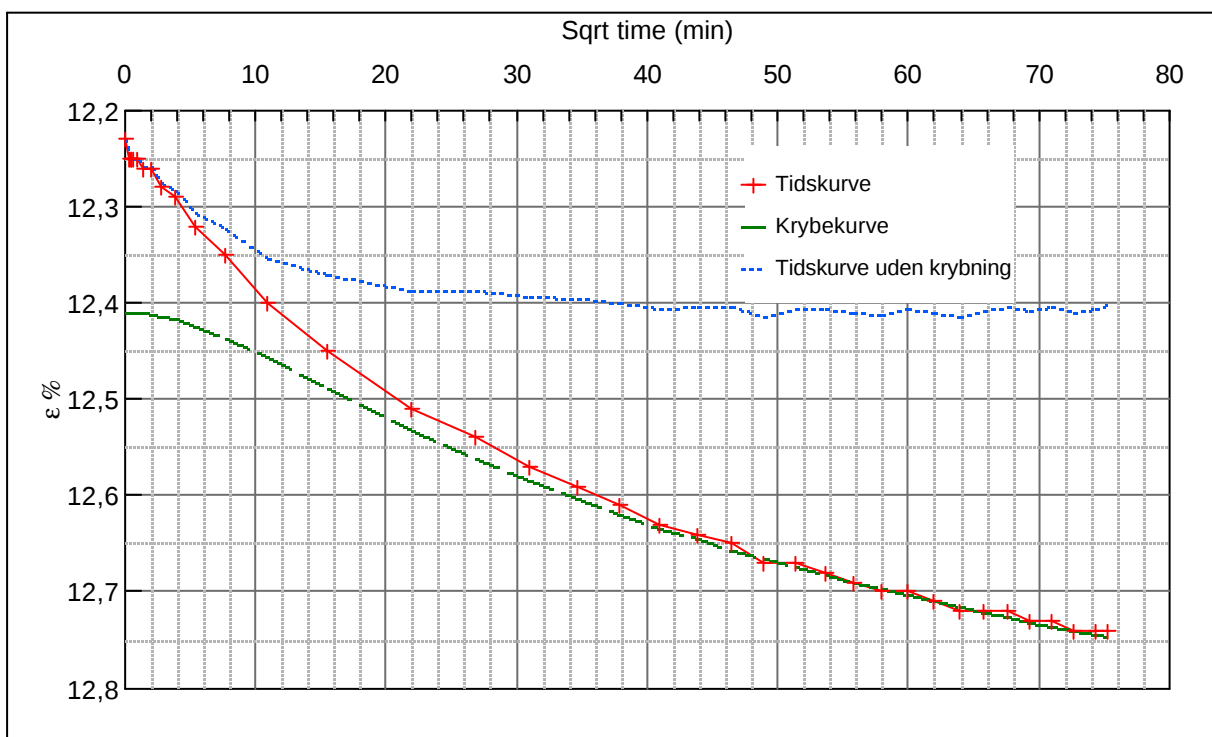
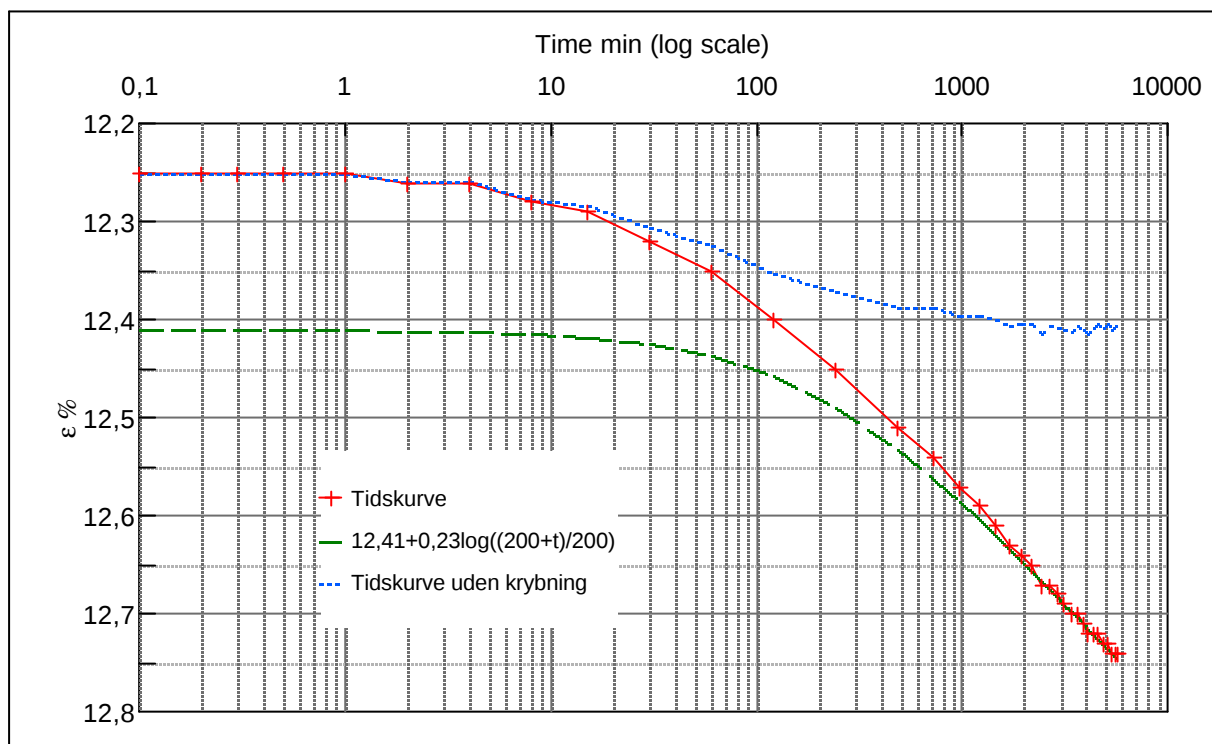
Step no 10	σ	kPa	ϵ	%	ϵ_i		tc in sec	7260
	Before	6.247,7	ϵ_0	11,69	ϵ_c %	11,92	K i kPa	452.554
	After	7.288,5	$\epsilon_{\sim\#}$	12,23	ϵ_s	0,23	k10 m/sec	2,9E-12
					ϵ_{kryb}	0,31	ck10 m ² /sec	1,34E-07



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress: ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.12
Executed:	AMS/gt	Check:
Approved:		

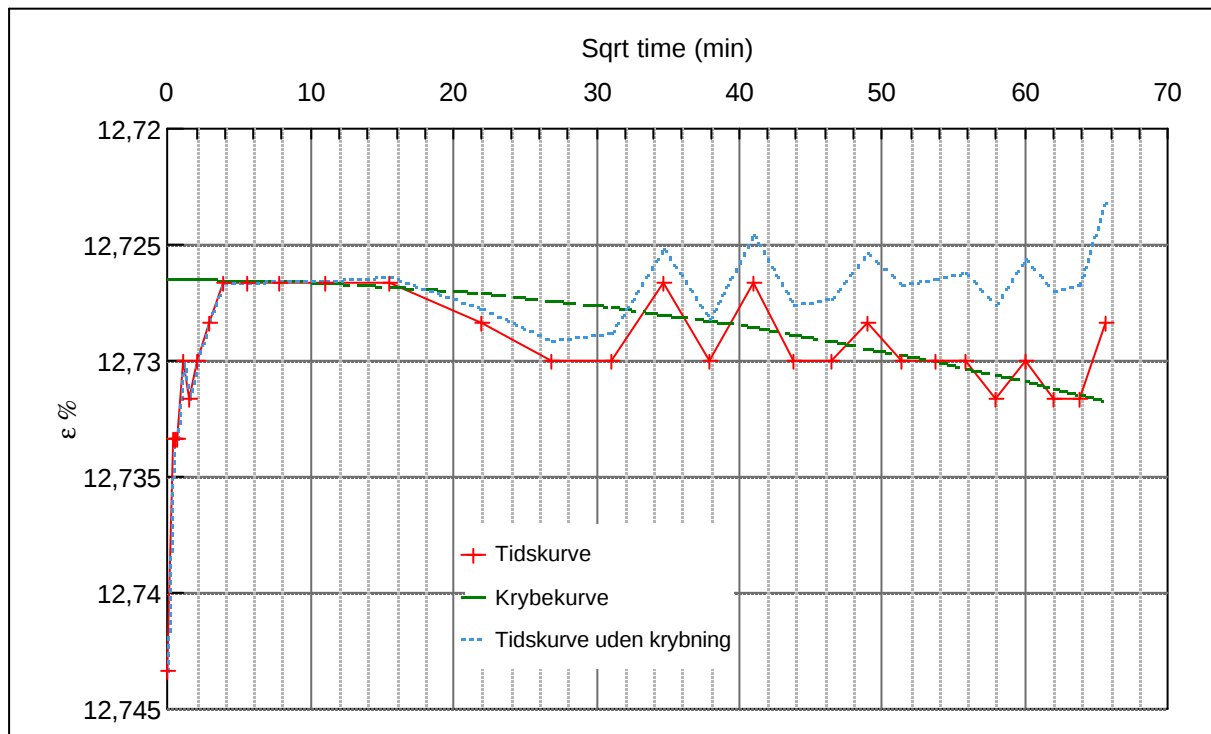
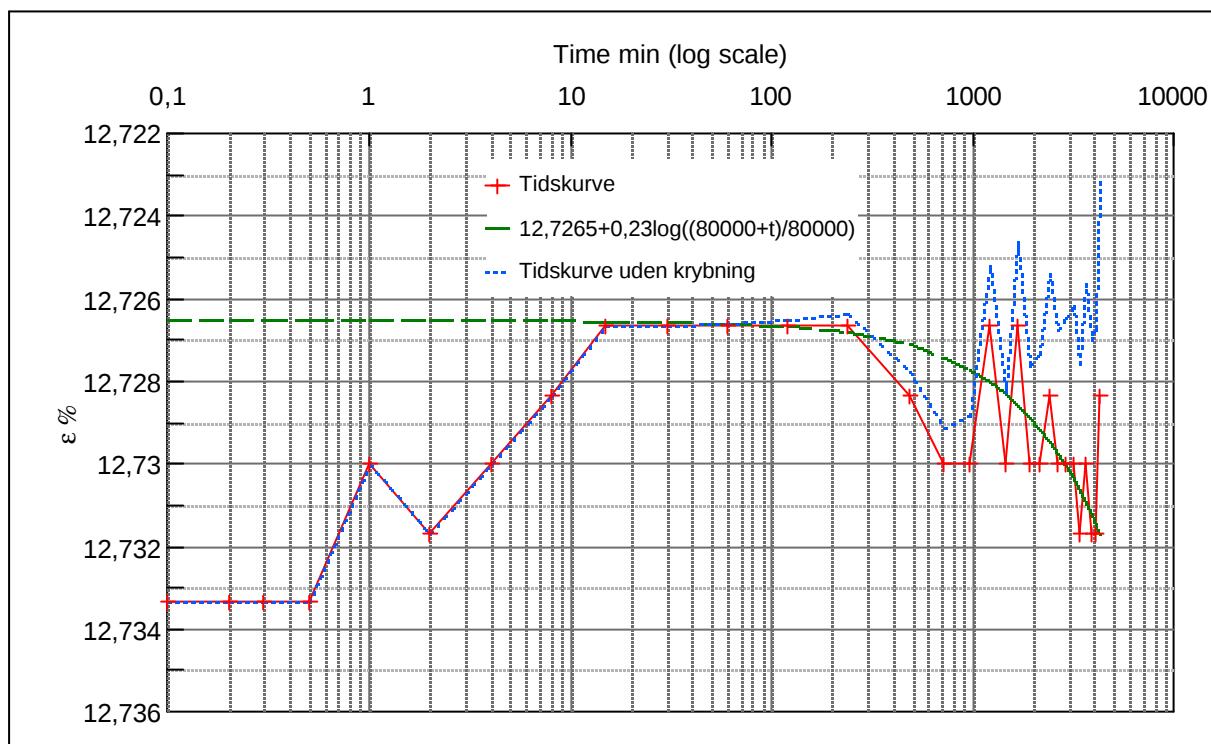
Step no 11	σ	kPa	ϵ	%	ϵ_i		tc in sec	7260
	Before	7.288,5	ϵ_0	12,23	ϵ_c %	12,41	K i kPa	578.263
	After	8.329,4	$\epsilon_{-#}$	12,74	ϵ_s	0,23	k10 m/sec	2,3E-12
					ϵ_{kryb}	0,33	ck10 m ² /sec	1,34E-07



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress: ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.13
Executed:	AMS/gt	Check:
Approved:		

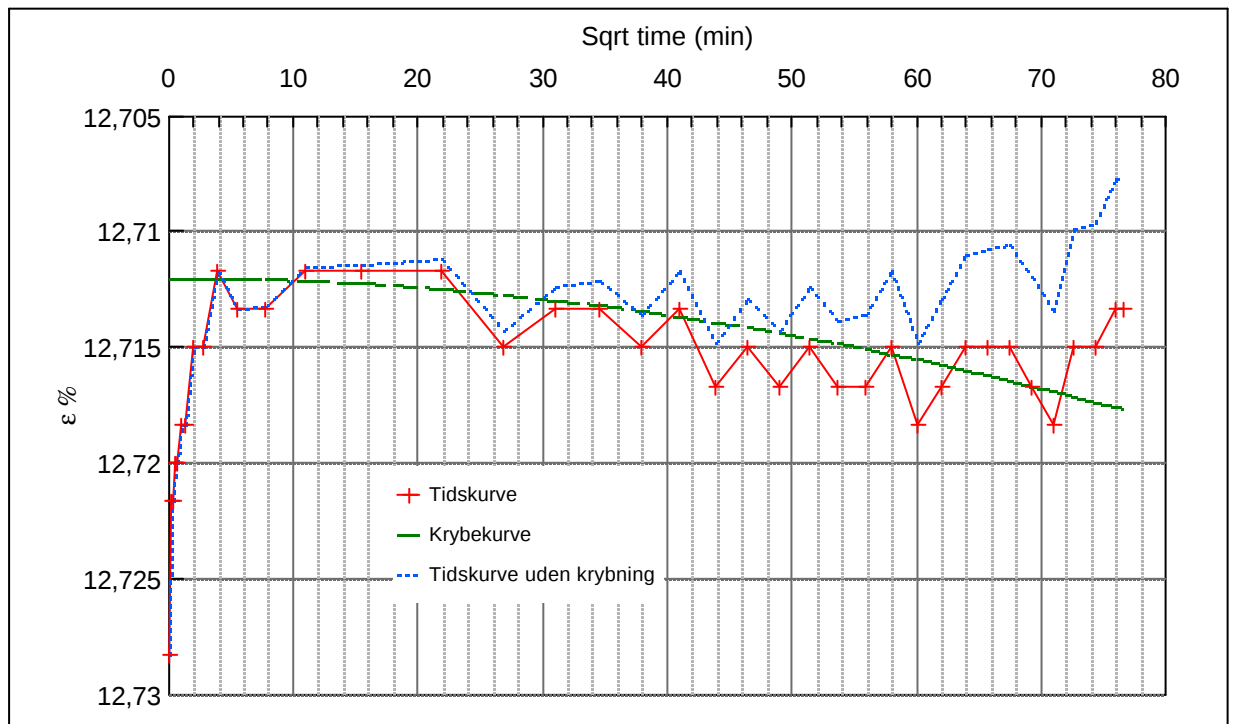
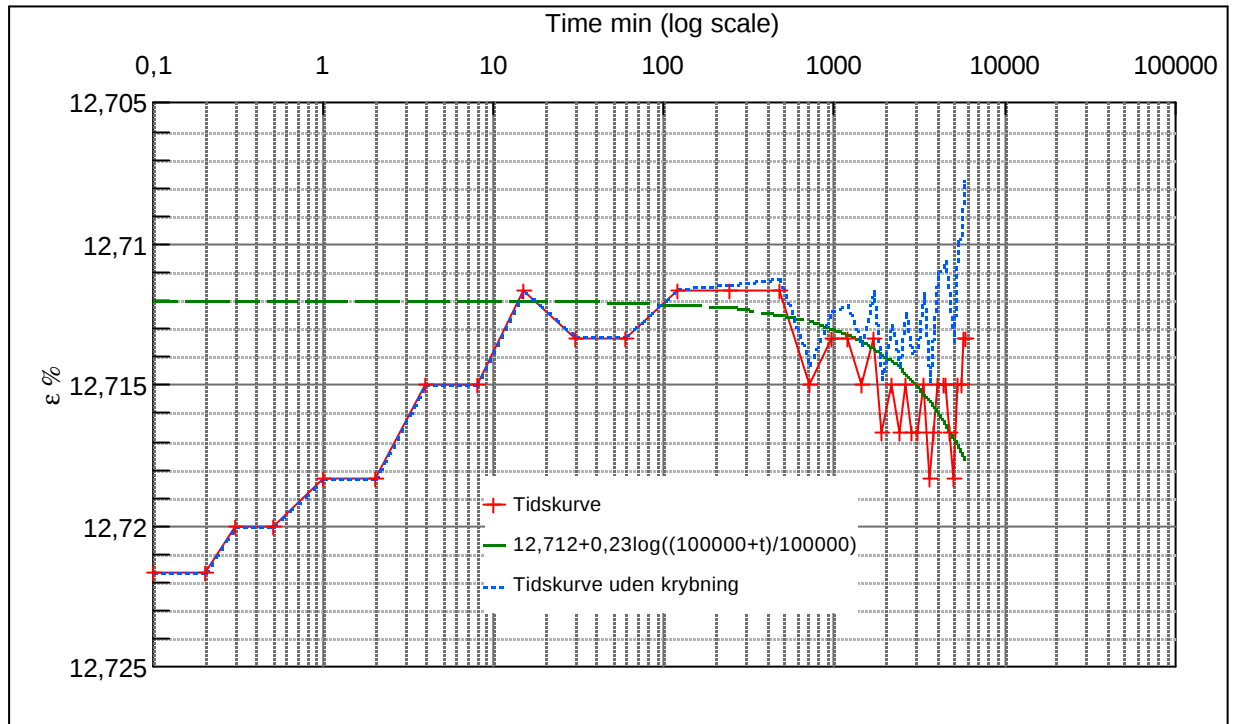
Step no 12	σ	kPa	ϵ	%	ϵ_i		tc in sec	960
	Before	8.329,4	ϵ_0	12,74	ϵ_c %	12,73	K i kPa	6.183.406
	After	7.288,5	$\epsilon_{-#}$	12,73	ϵ_s	0,04	k10 m/sec	1,6E-12
					ϵ_{kryb}	0,0015	ck10 m^2/sec	1,01E-06



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress:~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.14
Executed:	AMS/gt	Check:
Approved:		

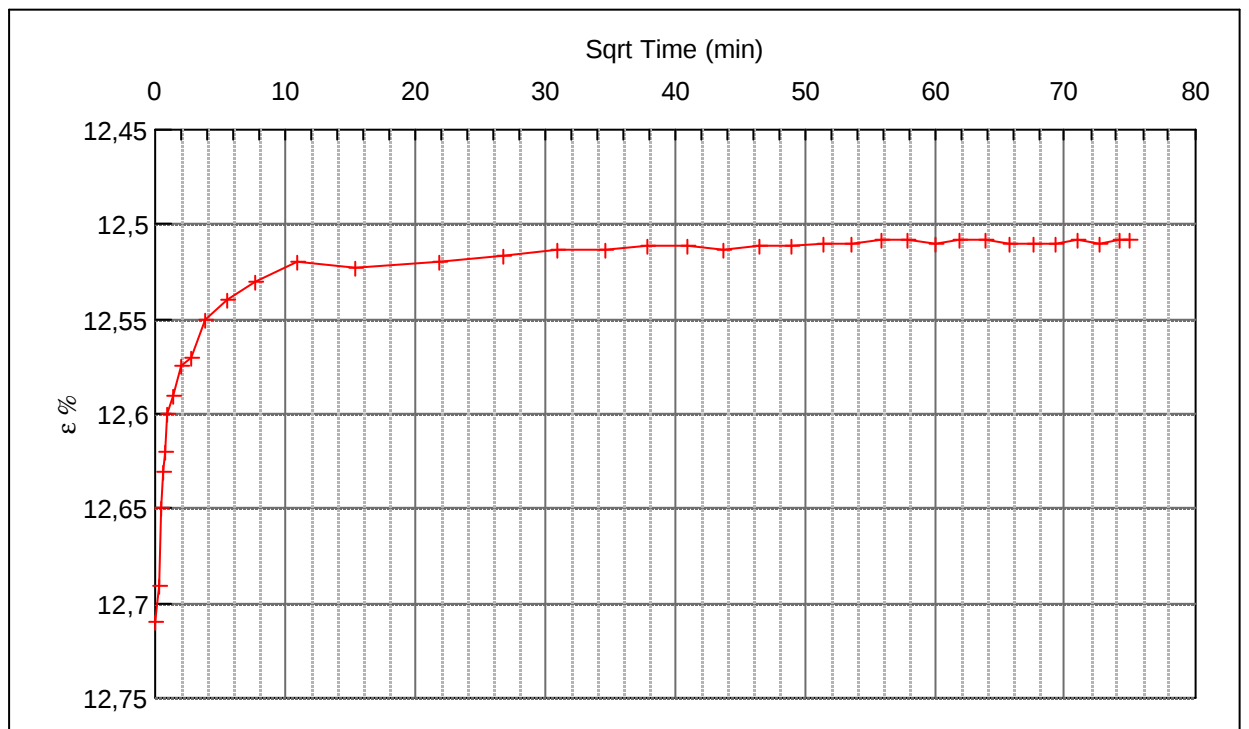
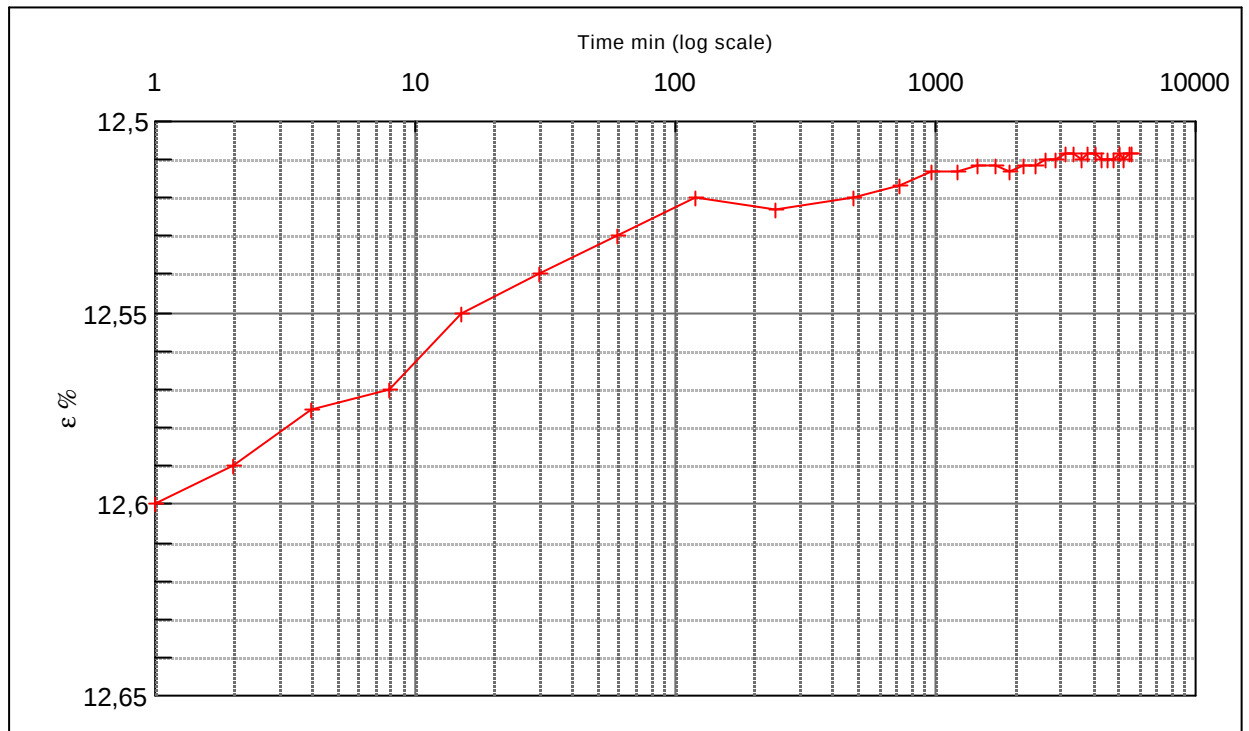
Step no 13	σ	kPa	ϵ	%	ϵ_i		tc in sec	960
	Before	7.288,5	ϵ_0	12,73	ϵ_c %	12,71	K i kPa	6.372.694
	After	6.247,7	$\epsilon_{\sim\#}$	12,71	ϵ_s	0,006	k10 m/sec	1,6E-12
					ϵ_{kryb}	0,001	ck10 m ² /sec	1,01E-06



Material:		
Clay	Eemian	Glacial
Bor no :	Depth: 78 m.b.s.	
Lab. no: k12	Insitu stress ~800 kPa	

Job:	Anholt	AAU
		Encl. No 4.15
Executed:	AMS/gt	Check:
Approved:		

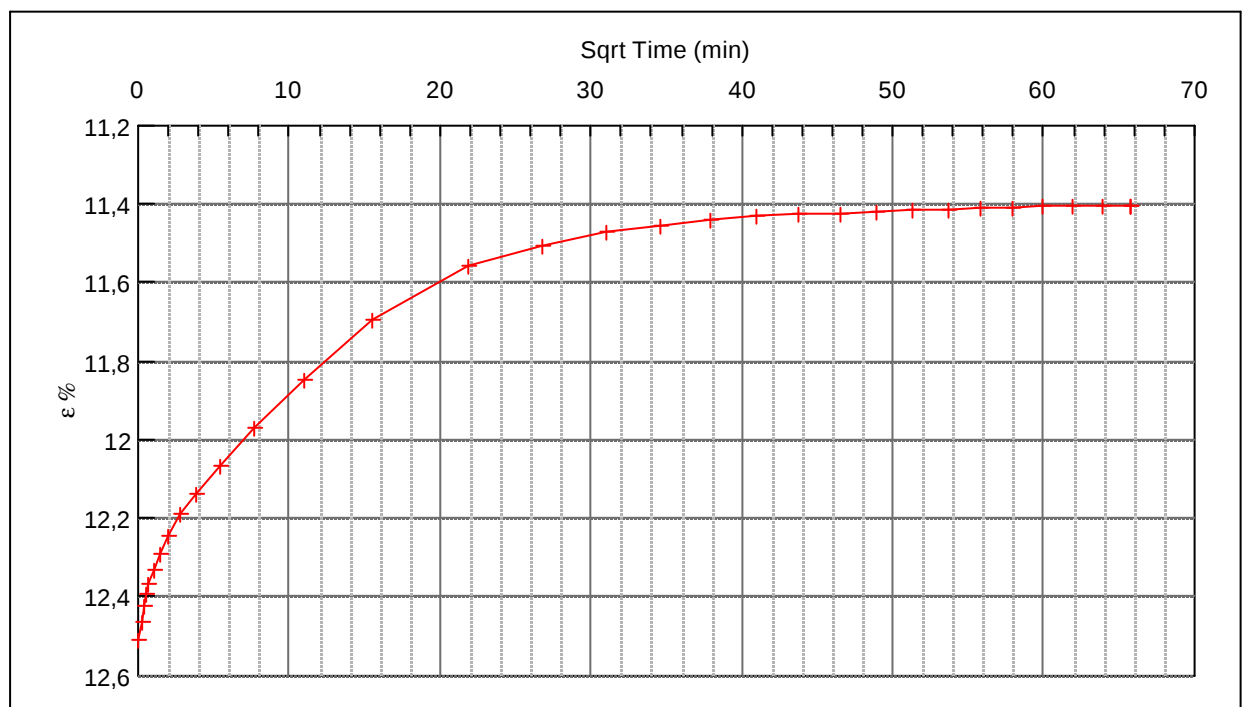
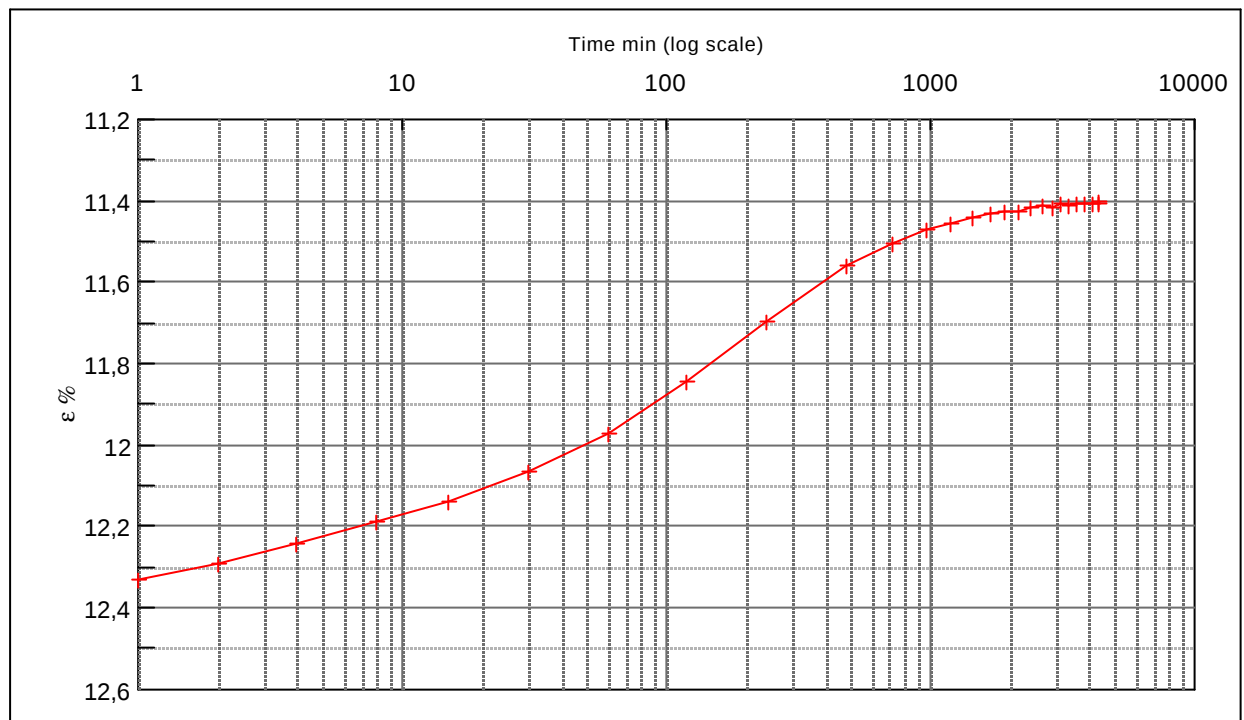
Step no 14	σ	kPa	ϵ	%	ϵ_i		tc in sec	1500
	Before	6.247,7	ϵ_0	12,71	ϵ_c %	12,5	K i kPa	1.545.851
	After	3.125,0	$\epsilon_{\sim\#}$	12,51	ϵ_s		k10 m/sec	4,1E-12
					ϵ_{kyb}		ck10 m^2 /sec	6,47E-07



Material:		
	Clay	Eemian Glacial
Bor no :	78 m.b.s.	
Lab. no:	k12	Insitu stress ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.16
Executed:	AMS/gt	Check:
Approved:		

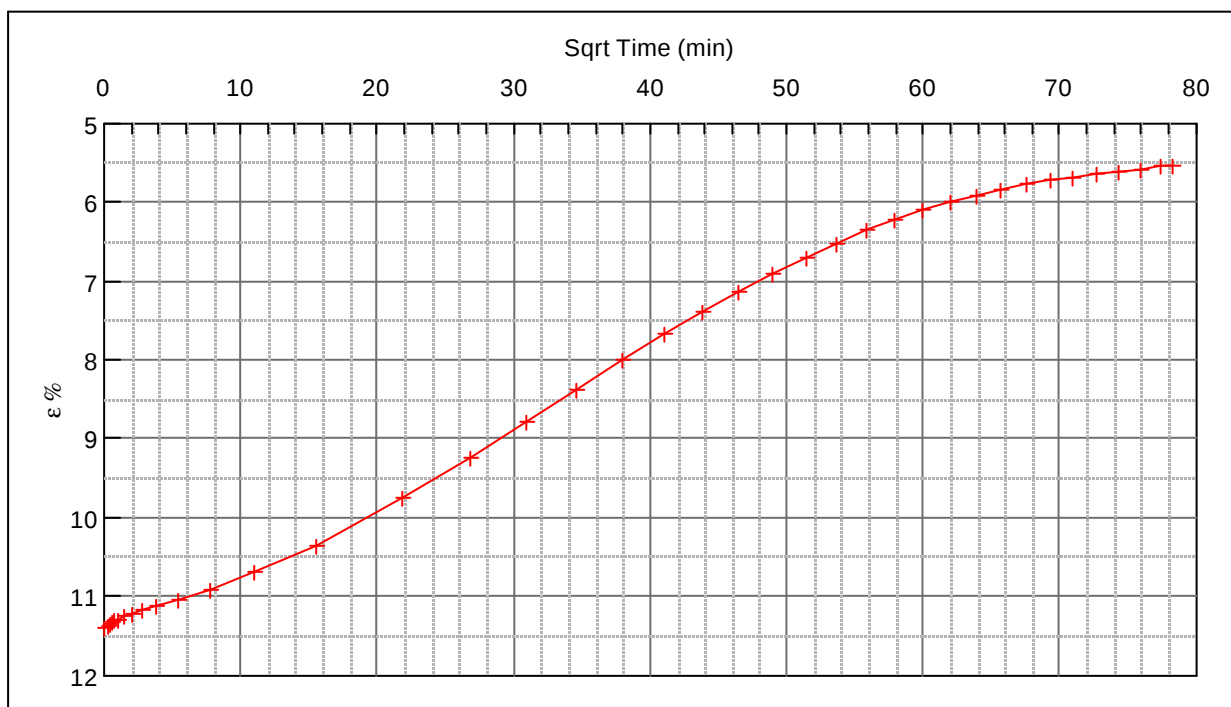
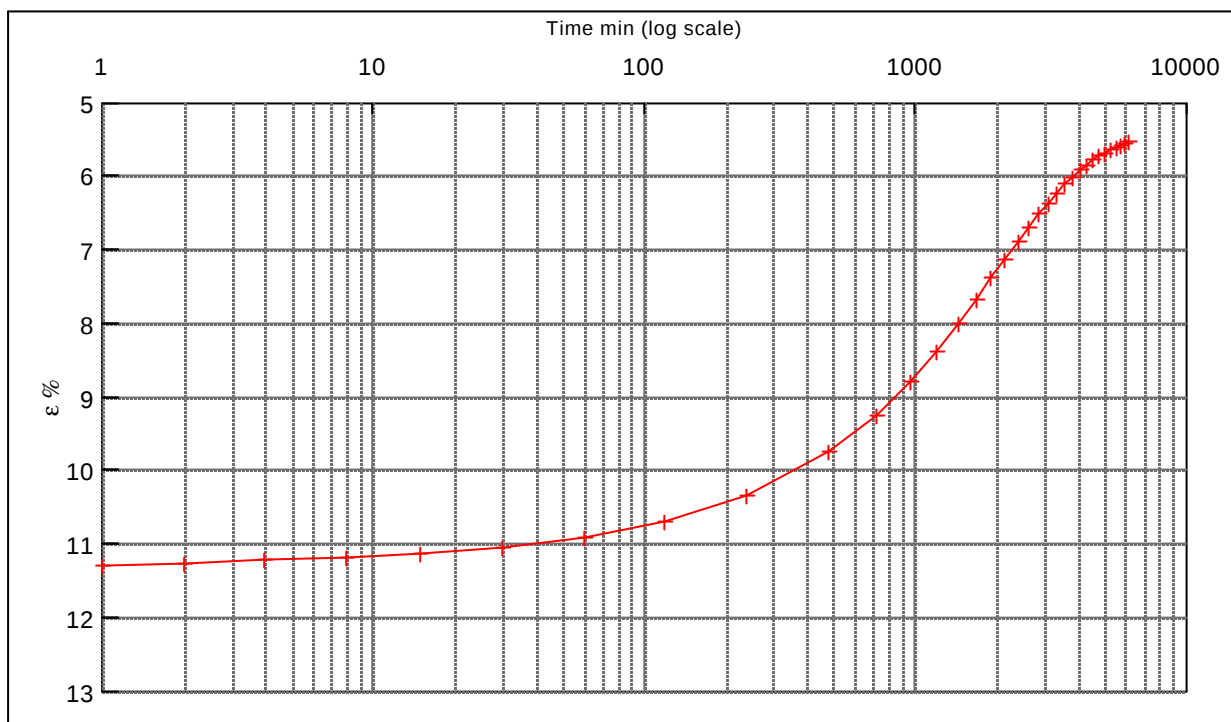
Step no 15	σ	kPa	ϵ	%	ϵ_i		tc in sec	29040
	Before	3.125,0	ϵ_0	12,51	ϵ_c %	11,4	K i kPa	219.527
	After	696,3	$\epsilon_{-#}$	11,40	ϵ_s		k10 m/sec	1,5E-12
					ϵ_{kyb}		ck10 m ² /sec	3,34E-08



Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.17
Executed:	AMS/gt	Check:
Approved:		

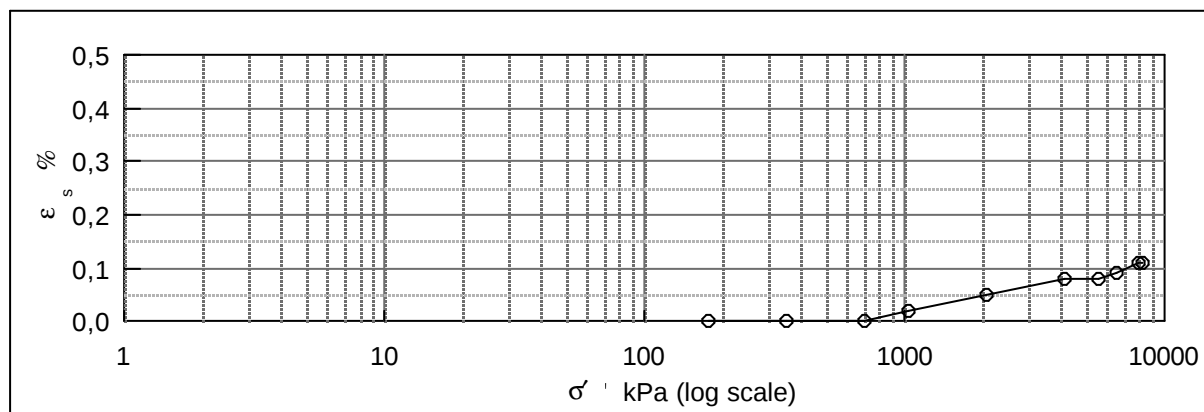
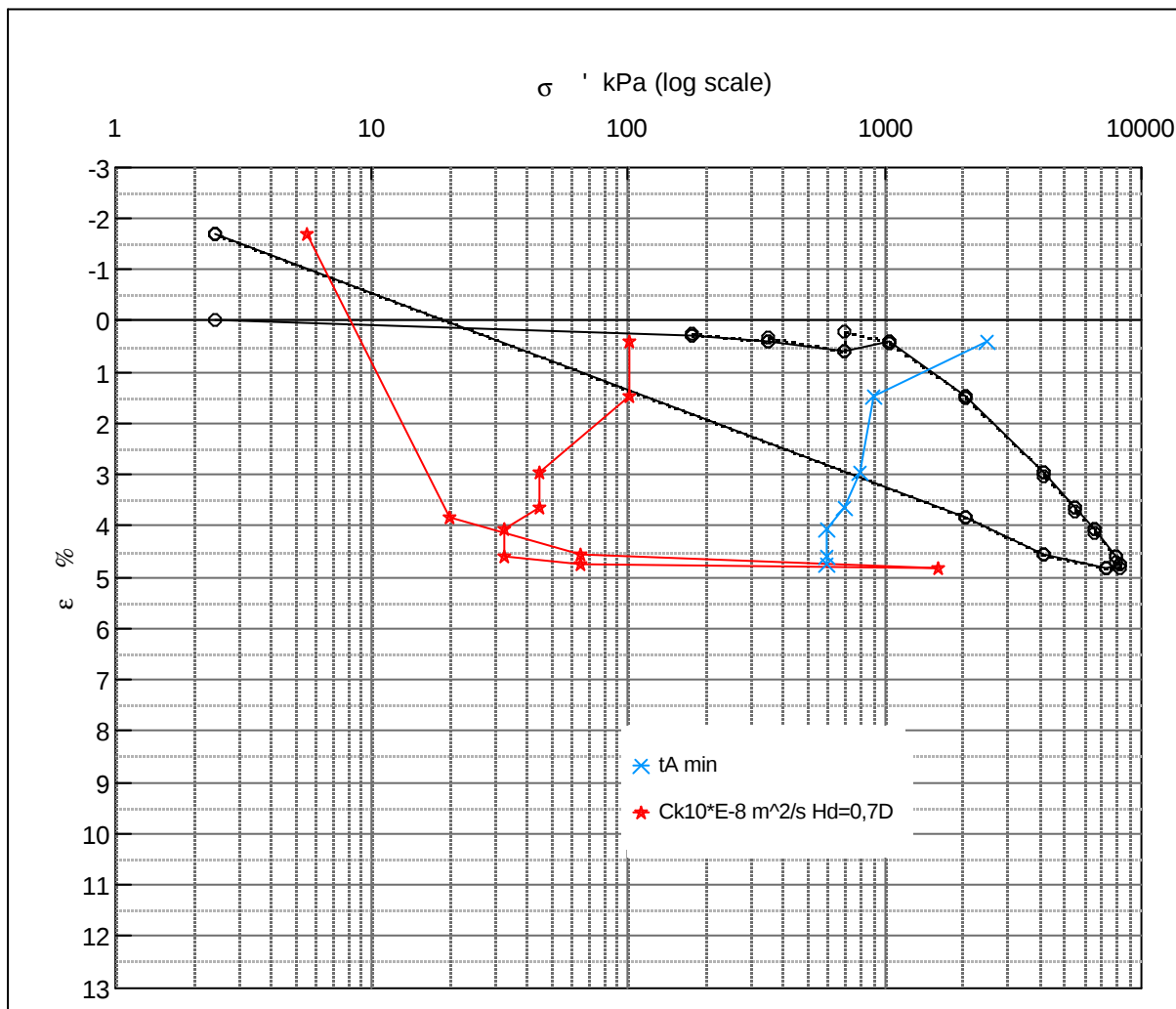
Step no 16	σ	kPa	ϵ	%	ϵ_i	tc in sec	230640
	Before	696,3	ϵ_0	11,40	ϵ_c %	K i kPa	11.831
	After	2,43	$\epsilon_{-#}$	5,54	ϵ_s	k10 m/sec	3,5E-12
					ϵ_{kyb}	ck10 m ² /sec	4,20E-09



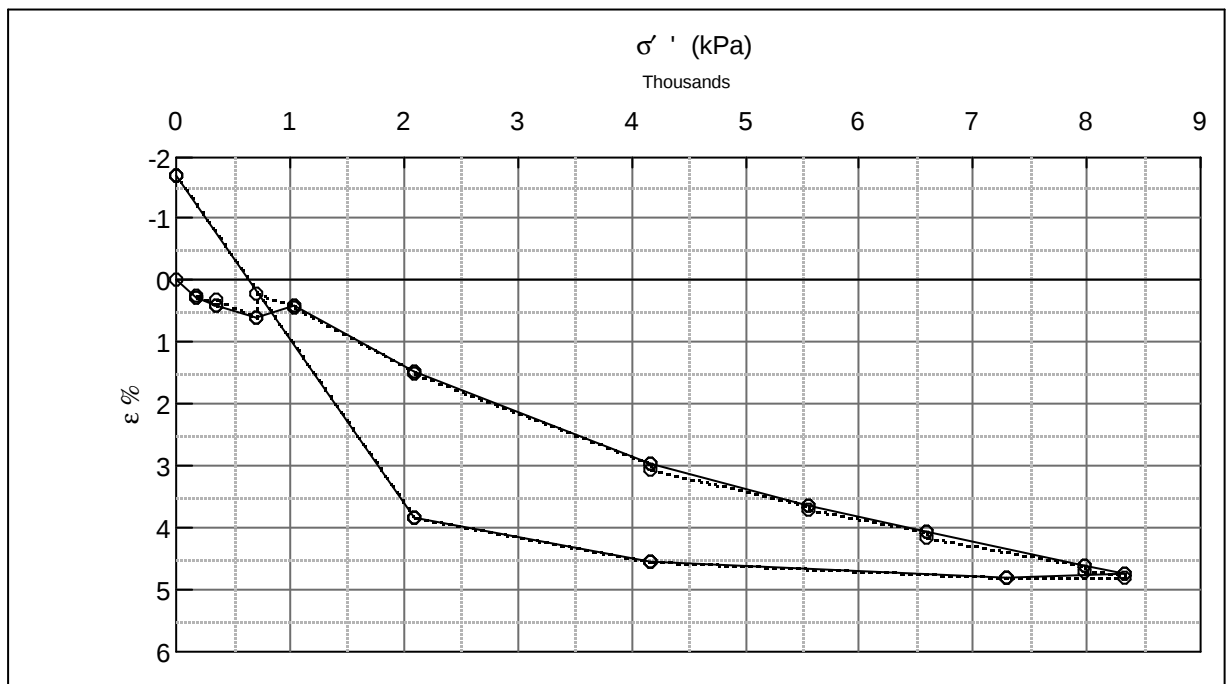
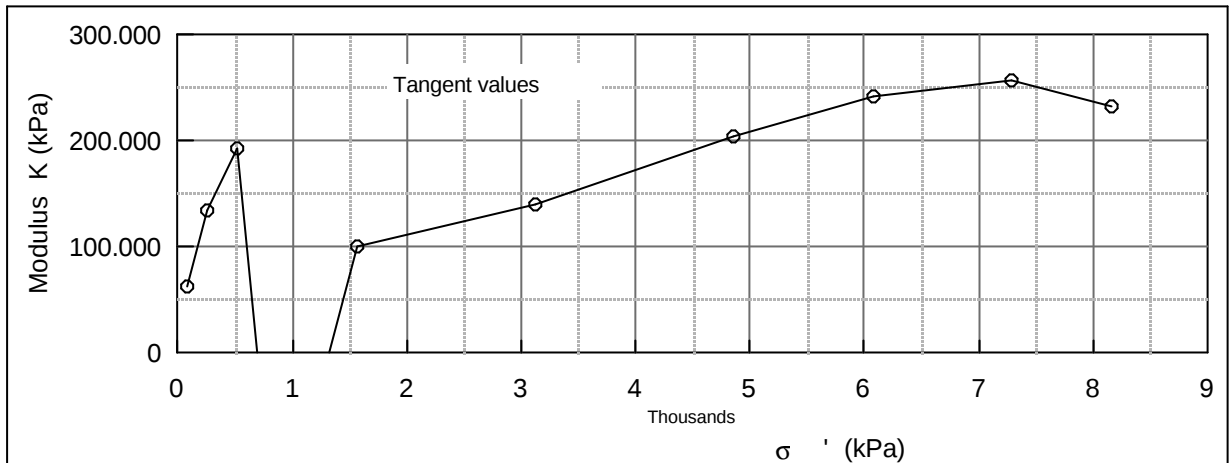
Material:	
Clay	Eemian Glacial
Bor no :	Depth: 78 m.b.s.
Lab. no: k12	Insitu stress: ~800 kPa

Job:	Anholt	AAU
		Encl. No 4.18
Executed:	AMS/gt	Check:
Approved:		

Description of soil: Clay middle jura			Water content %	Before	After
			Bulk density Mg/m ³	12,3	18,4
			Grain density Mg/m ³	2,07	2,15
				~2.69	
Bor no : A III	Overburden pressure σ'_o	~1620 kPa	Void ratio	0,47	0,49
Lab. no: k 26	Vane strength c_v	kPa	Degr. of Saturation %	75	100
Level : 162 m.b.s	CPT - value q_c	MPa	Dimension H x D mm	30x60	30.5x60



Job: Anholt	AAU	
	Encl. No 5.1	
Executed:	AMS/gt	Check:



Test results		σ kPa	ε_c %	ε_s % / lct	C k10 m ² /s	σ_m kPa	K kPa	w %
Q	~ 6 % ?	2,4	0,00					17,5
QS	0.11 %	175,9	0,28			89,2	61956,7	17,3
σ_{pc}	~8000 kPa	349,4	0,41			262,6	133445,3	17,3
		696,3	0,59			522,9	192754,3	17,2
		1.043,3	0,41	0,02	1,0E-06	869,8	-187544,7	17,3
		2.084,2	1,46	0,05	1,0E-06	1.563,7	98661,0	16,7
		4.165,9	2,95	0,08	4,5E-07	3.125,0	139714,5	15,9
		5.553,8	3,63	0,08	4,5E-07	4.859,8	204092,8	15,5
		6.594,6	4,06	0,09	3,3E-07	6.074,2	242063,6	15,3
		7.982,5	4,60	0,11	3,3E-07	7.288,5	257005,8	15,0
		8.329,4	4,75	0,11	6,5E-07	8.155,9	231305,2	14,9
		7.288,5	4,81		1,6E-05	7.809,0	-1892497,0	14,9
		4.165,9	4,55		6,5E-07	5.727,2	1210317,8	15,0
		2.084,2	3,85		2,0E-07	3.125,0	296545,1	15,4
		2,4	(1,69)		5,6E-08	1.043,3	37590,2	18,4

Remark:
" Genbelastningsgren"
Normalkonsolideret tilstand næppe nået

Job: Anholt

AAU

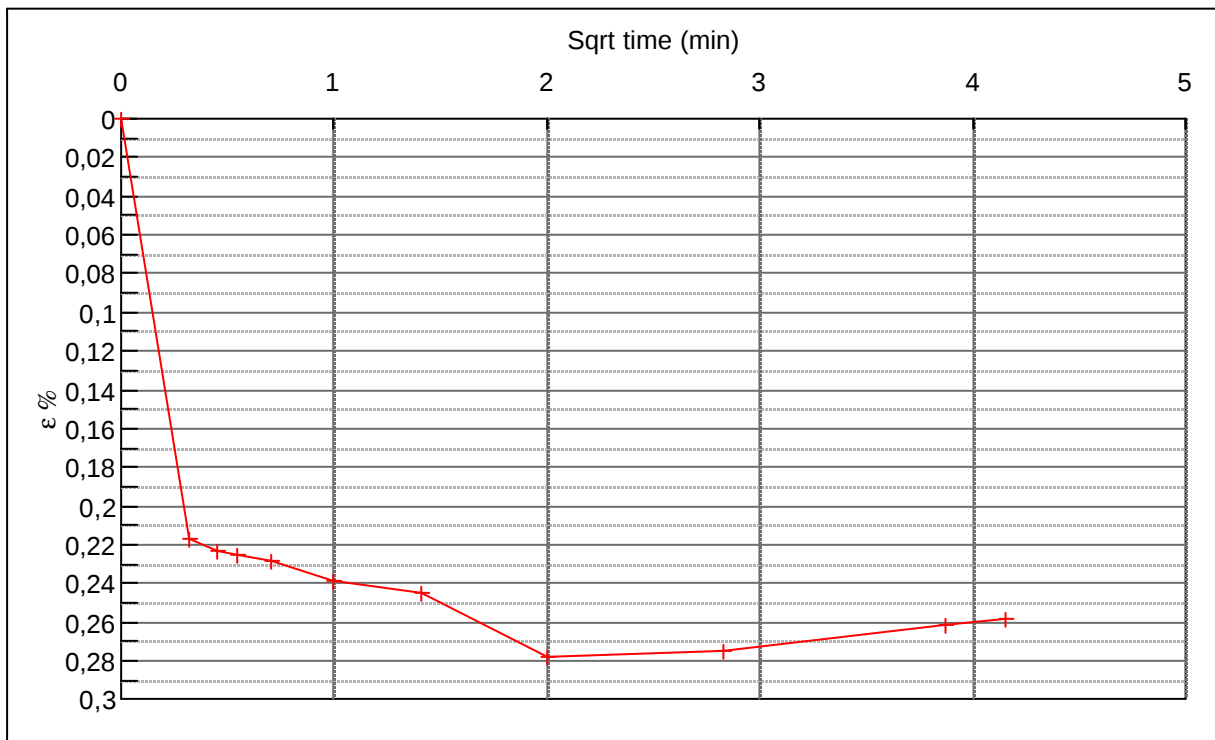
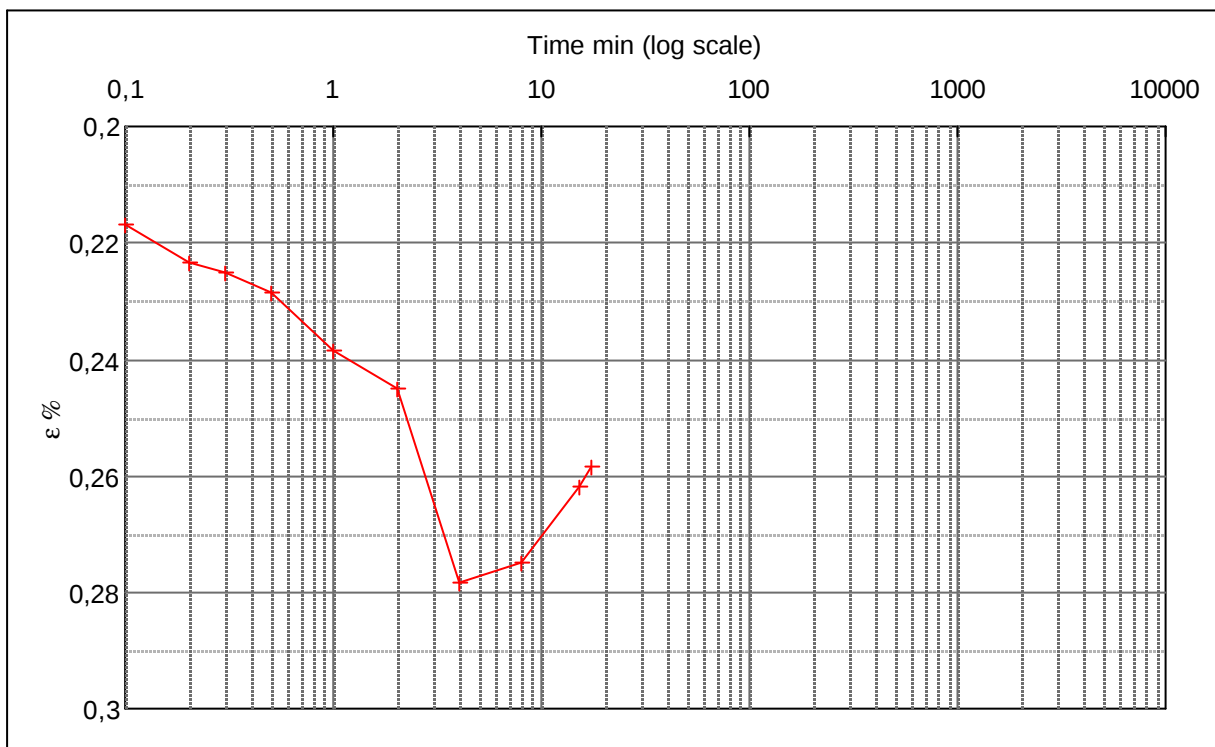
Encl. No
5.2

Executed: AMS/gt

Check:

Approved:

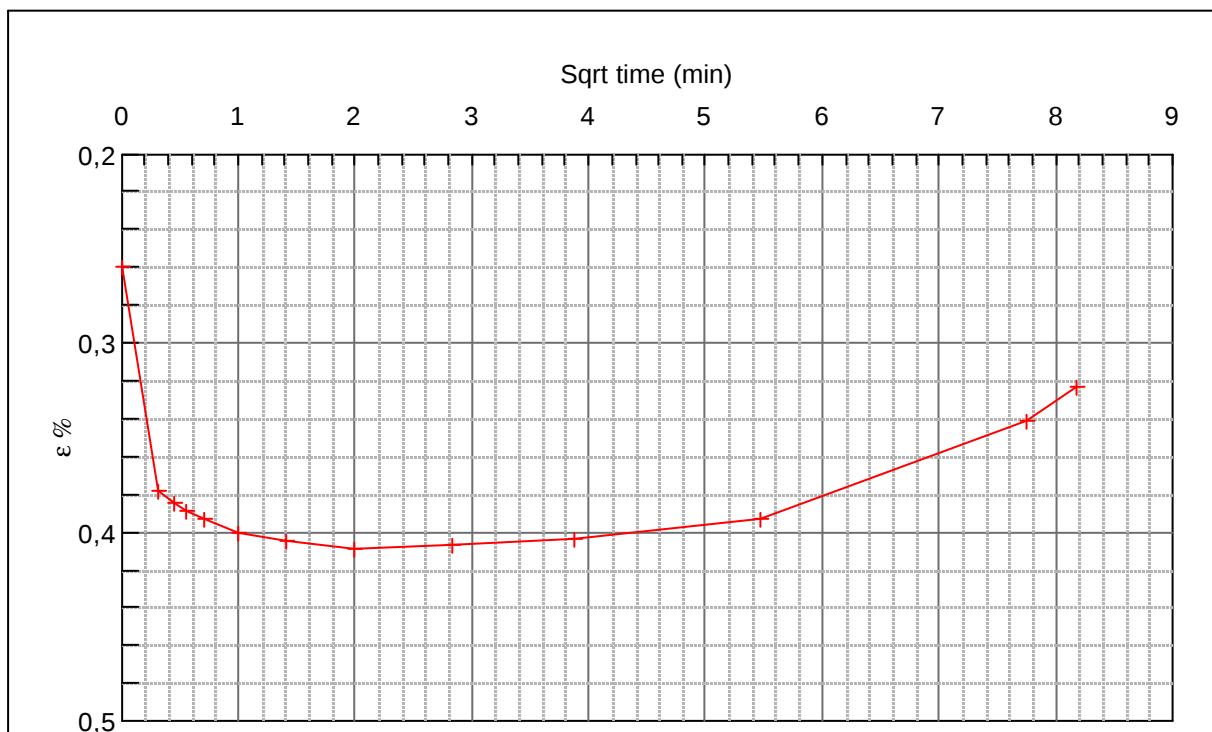
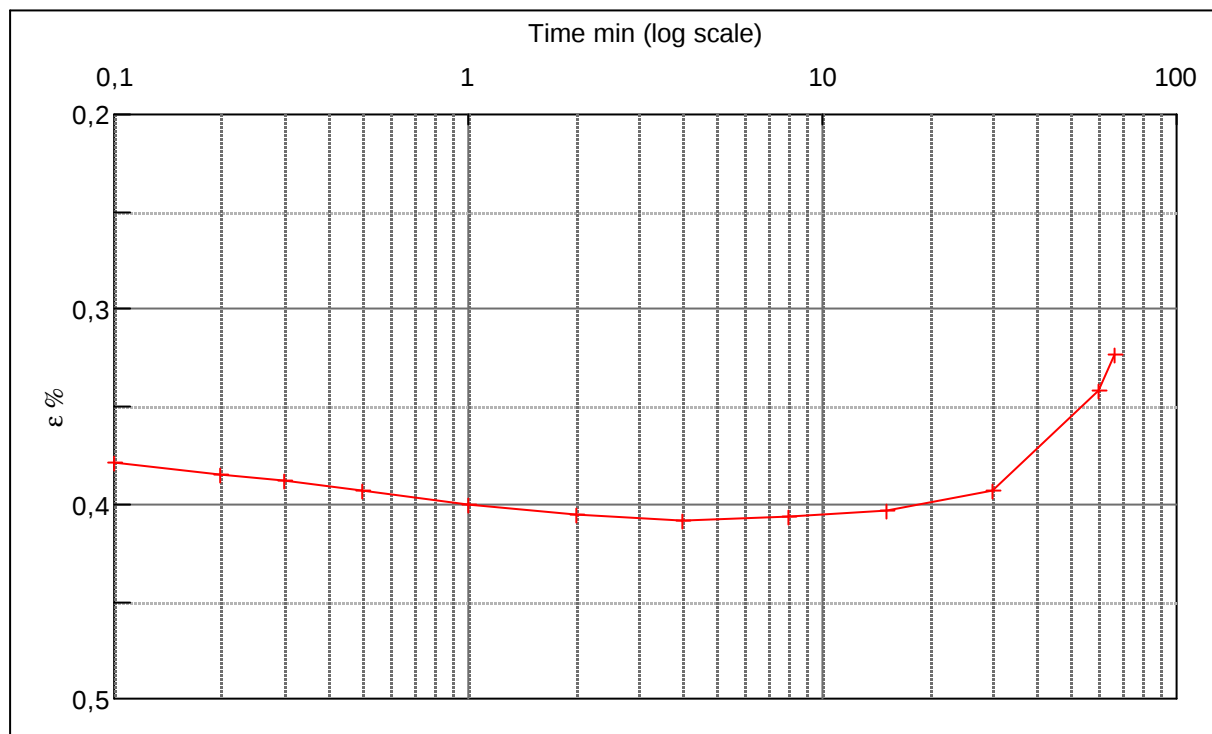
Step no	σ	kPa	ϵ	%	ϵ_i		tc in sec
1	Before	2,43	ϵ_0	0,00	ϵ_c %	0,28	K i kPa
	After	175,9	$\epsilon_{\sim\#}$	0,26	ϵ_s		k10 m/sec
					ϵ_{kylb}		ck10 m^2 /sec



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.3
Executed:	AMS/gt	Check:
Approved:		

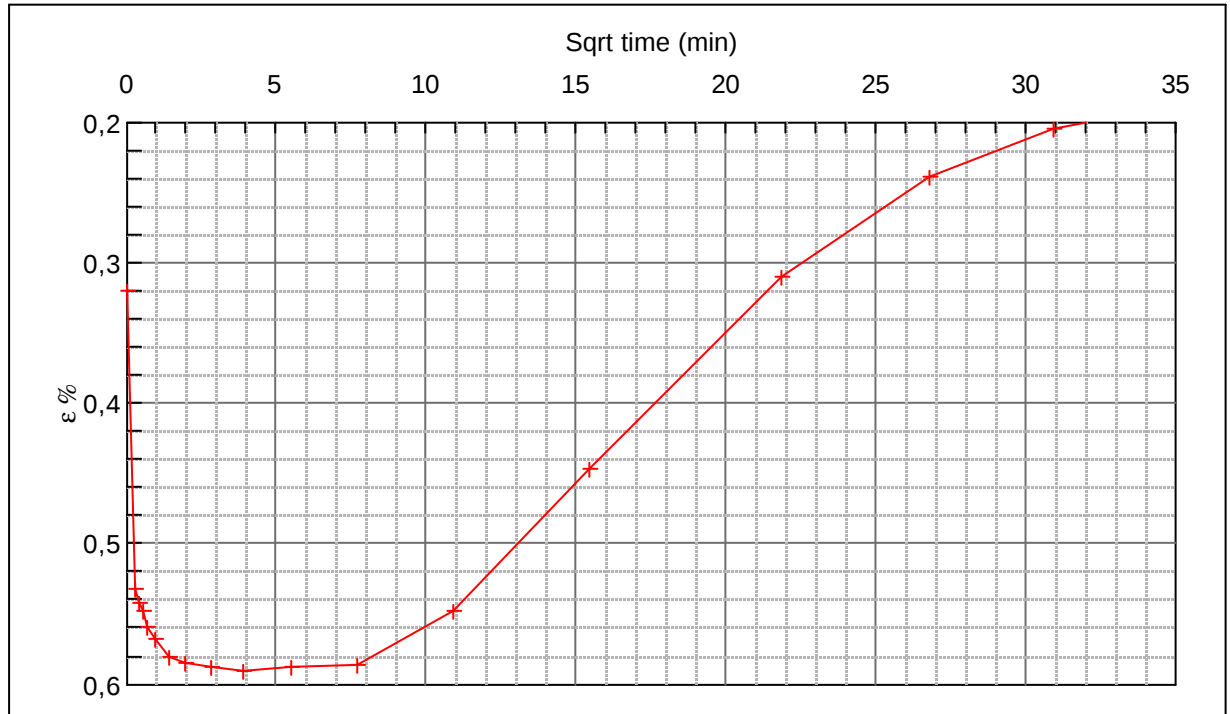
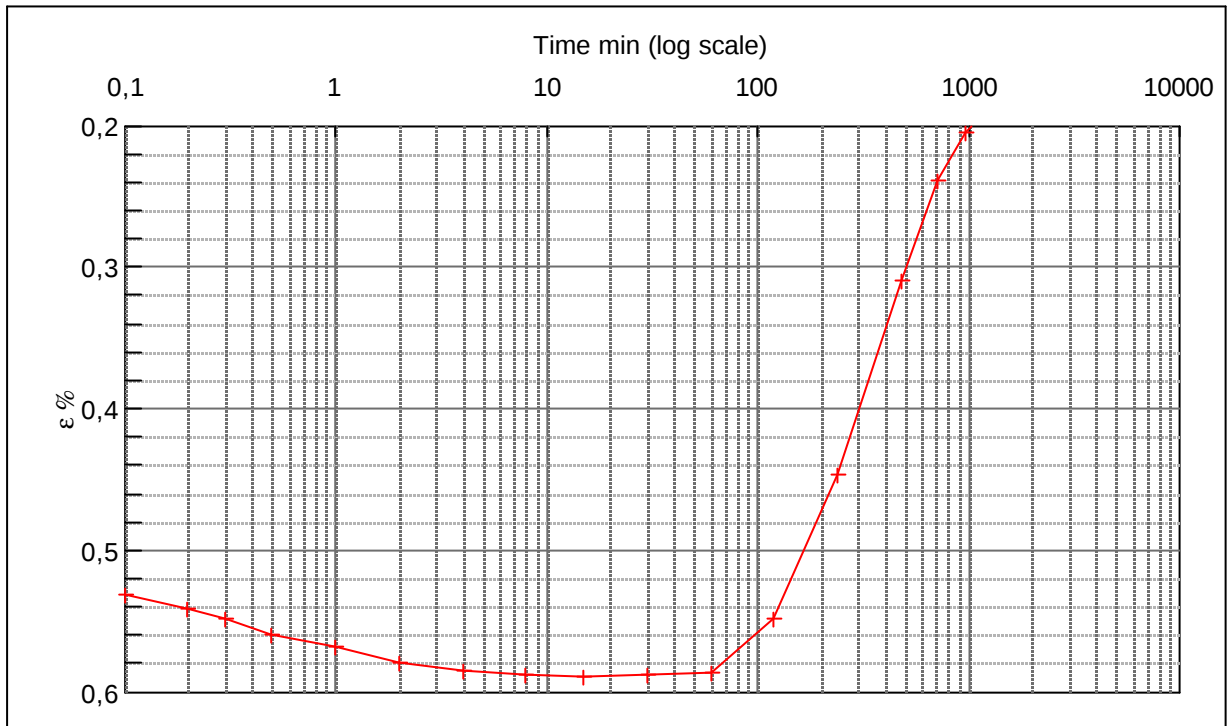
Step no 2	σ	kPa	ϵ	%	ϵ_i	tc in sec K i kPa k10 m/sec ck10 m^2 /sec	
	Before	175,9	ϵ_0	0,26	ϵ_c %		
	After	349,4	$\epsilon_{-#}$	0,32	ϵ_s		
					ϵ_{kryb}		



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.4
Executed:	AMS/gt	Check:
Approved:		

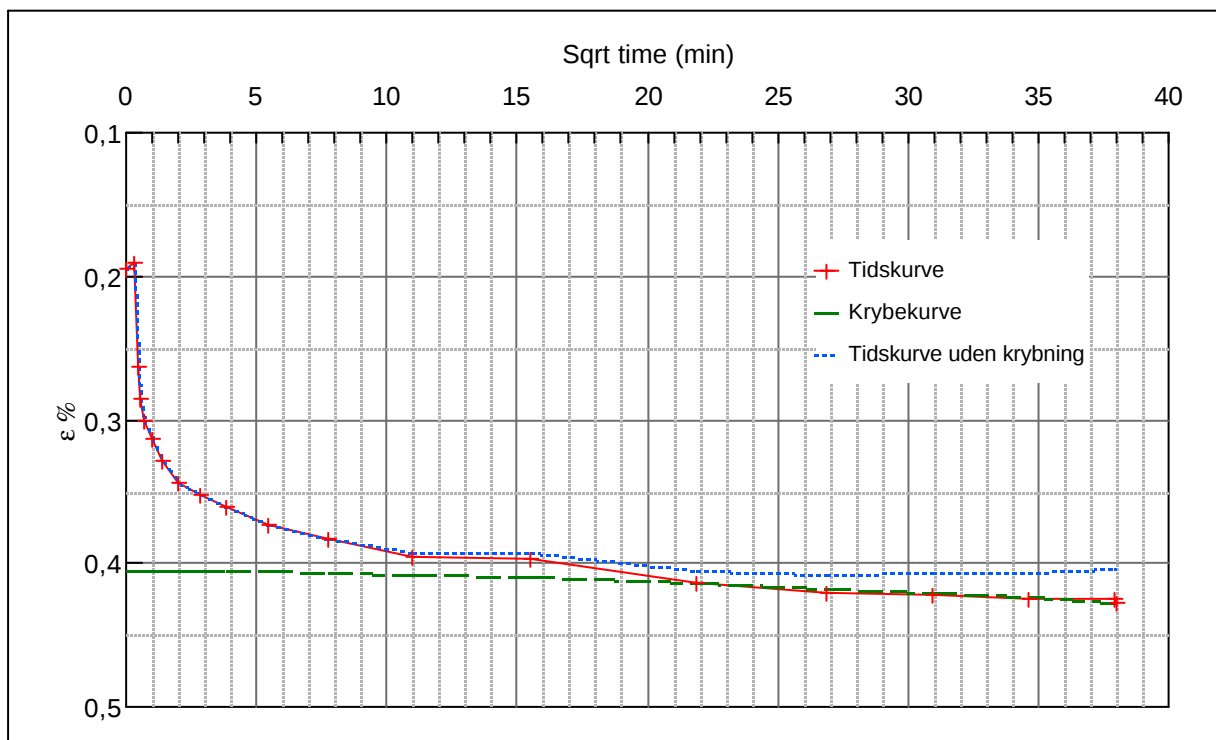
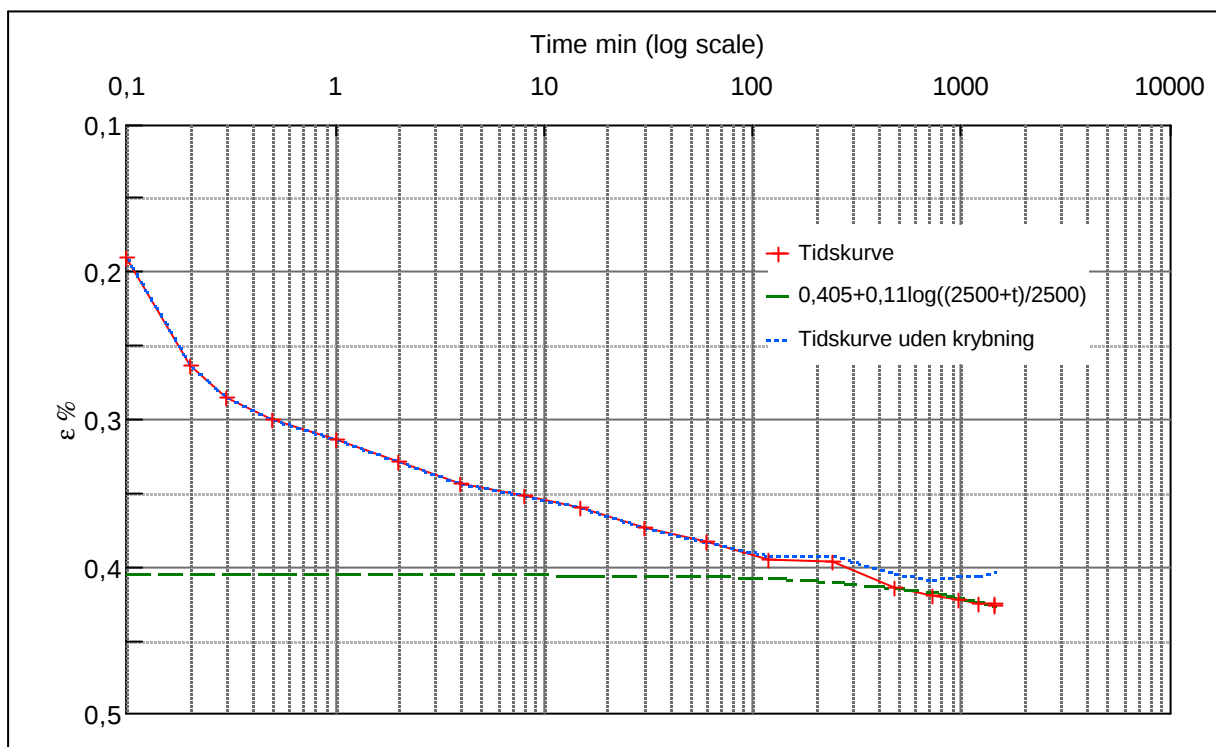
Step no 3	σ	kPa	ϵ	%	ϵ_i	tc in sec K i kPa k10 m/sec ck10 m ² /sec	
	Before	349,4	ϵ_0	0,32	ϵ_c %		
	After	696,3	$\epsilon_{\sim\#}$	0,20	ϵ_s		
					ϵ_{kyb}		



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.5
Executed:	AMS/gt	Check:
Approved:		

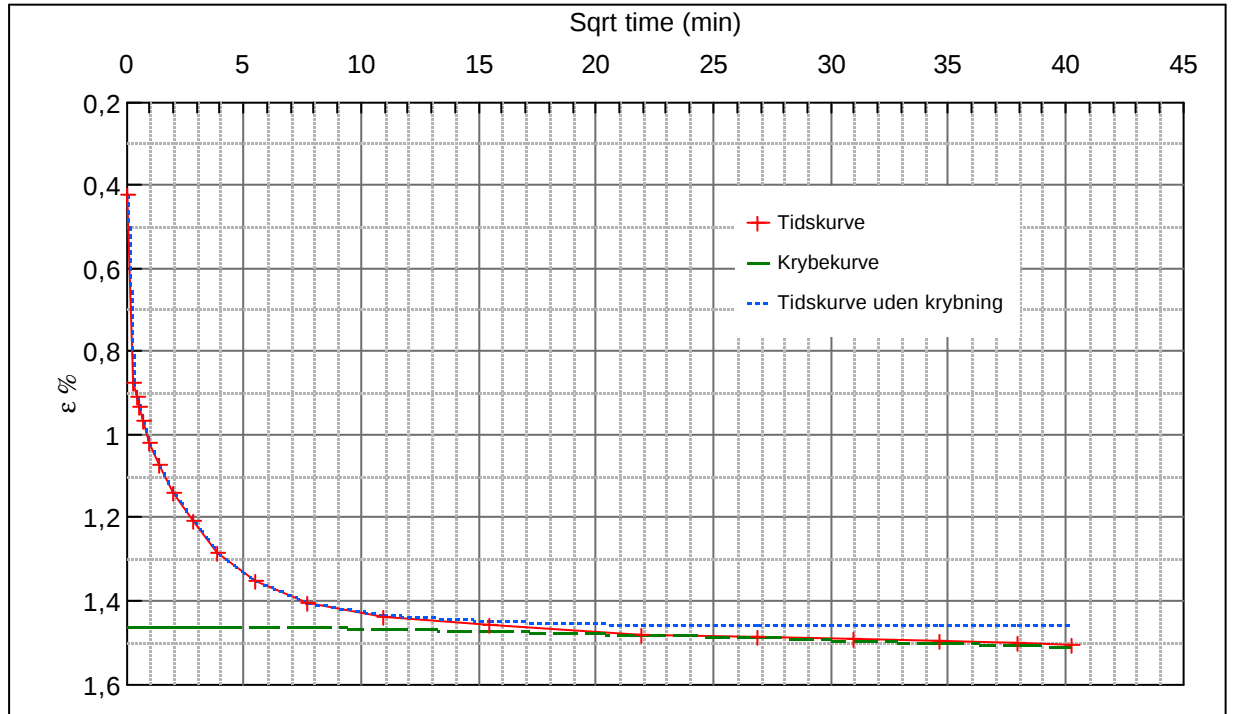
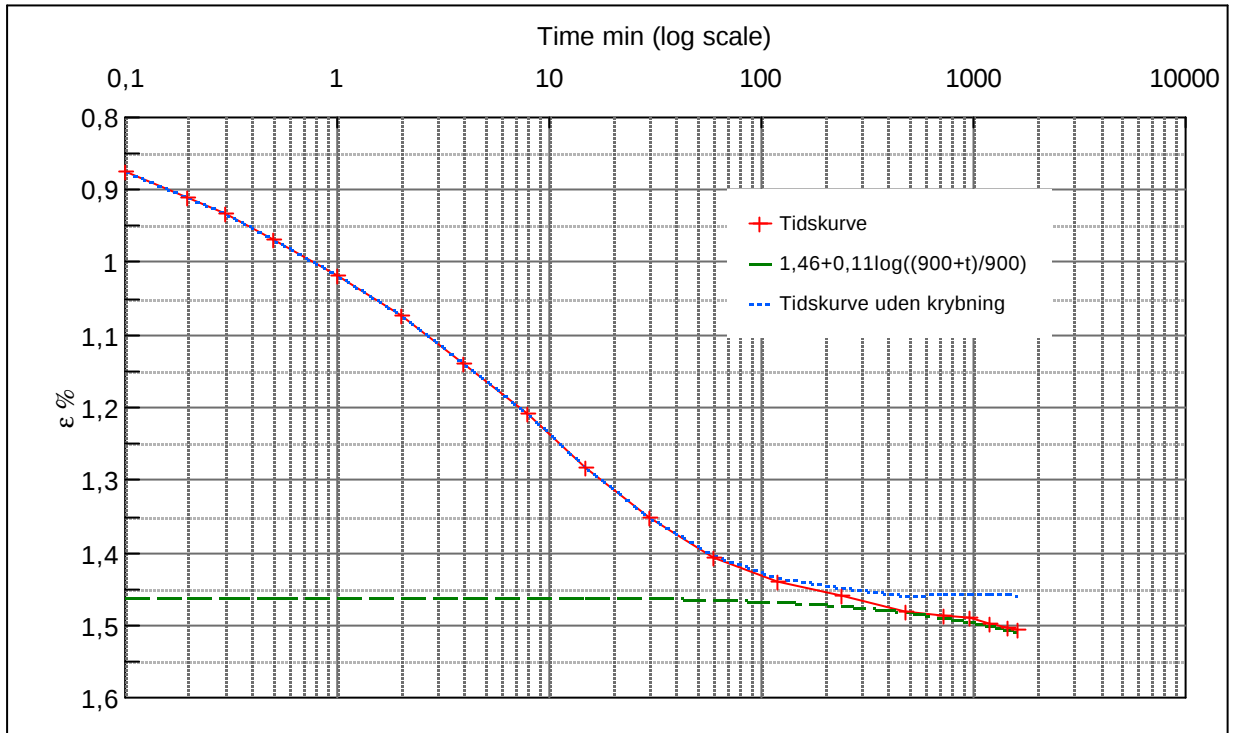
Step no 4	σ	kPa	ϵ	%	ϵ_i		tc in sec	960
	Before	696,3	ϵ_0	0,195	ϵ_c %	0,405	K i kPa	165.218
	After	1.043,3	$\epsilon_{\sim\#}$	0,427	ϵ_s	0,02	k10 m/sec	6,0E-11
					ϵ_{kryb}	0,02	ck10 m ² /sec	1,01E-06



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.6
Executed:	AMS/gt	Check:
Approved:		

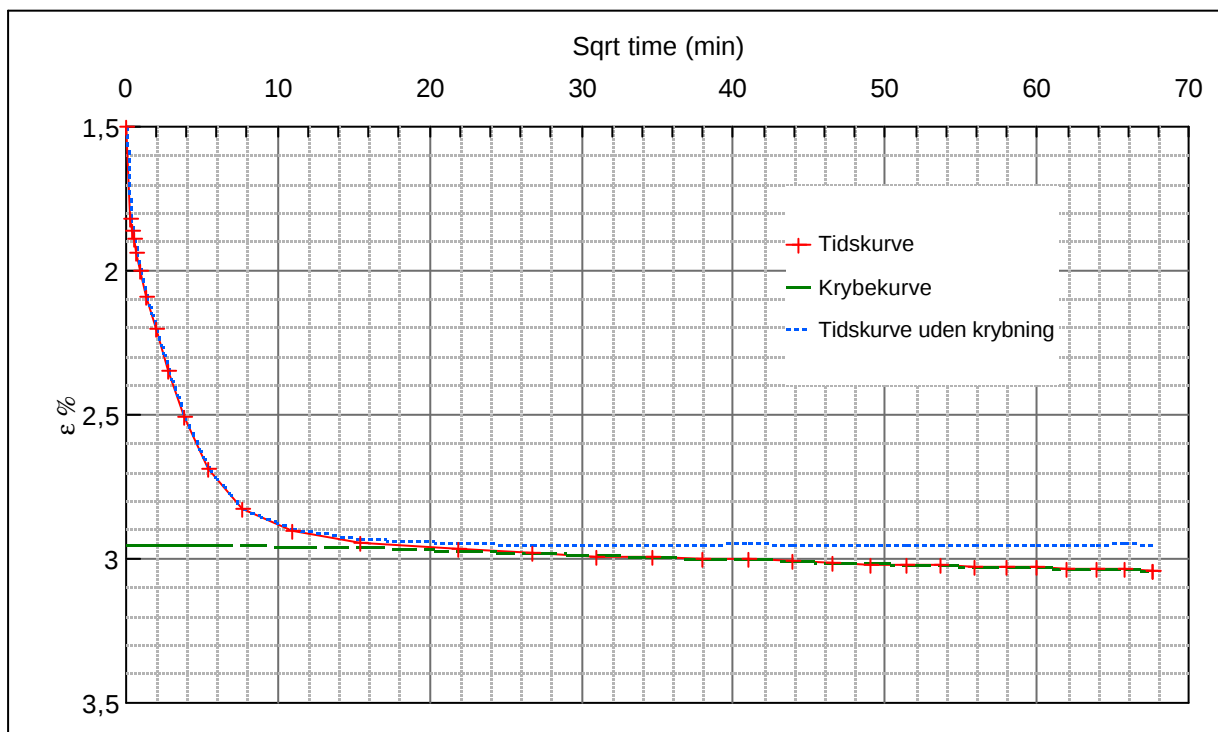
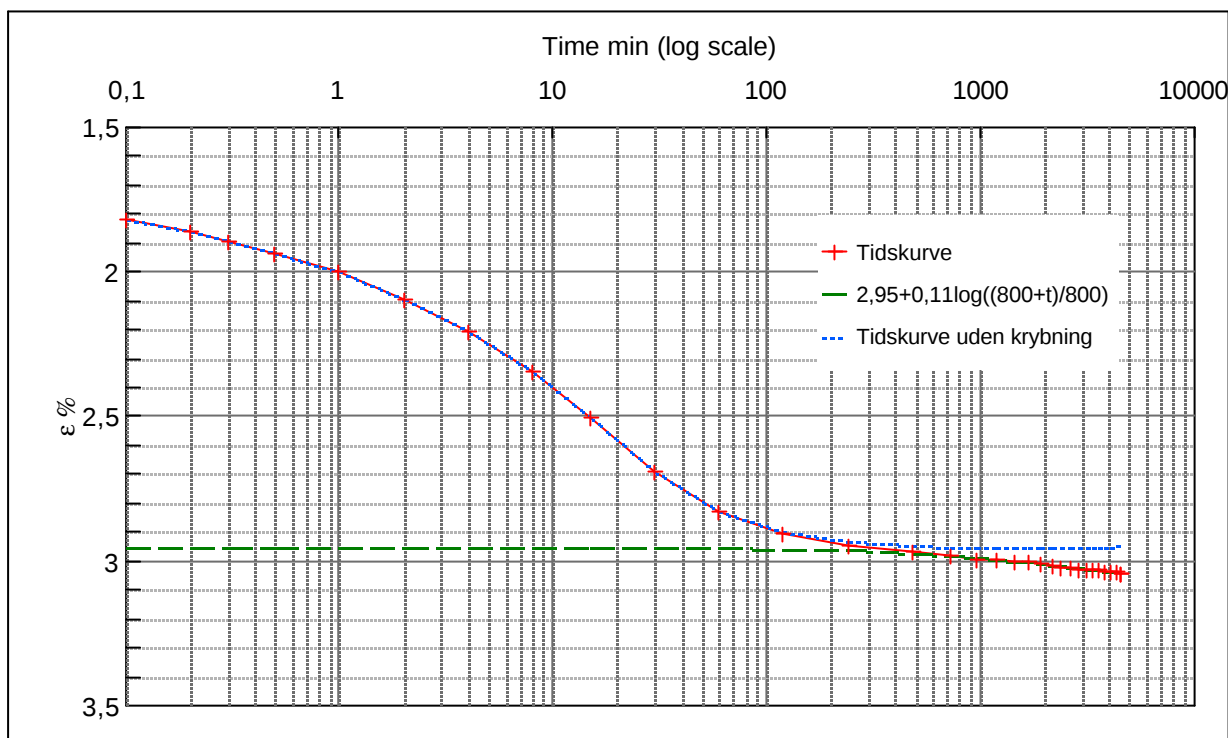
Step no 5	σ	kPa	ϵ	%	ϵ_i		tc in sec	960
	Before	1.043,3	ϵ_0	0,42	ϵ_c %	1,46	K i kPa	100.406
	After	2.084,2	$\epsilon_{\sim\#}$	1,51	ϵ_s	0,05	k10 m/sec	9,9E-11
					ϵ_{kryb}	0,05	ck10 m^2 /sec	1,01E-06



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.7
Executed:	AMS/gt	Check:
Approved:		

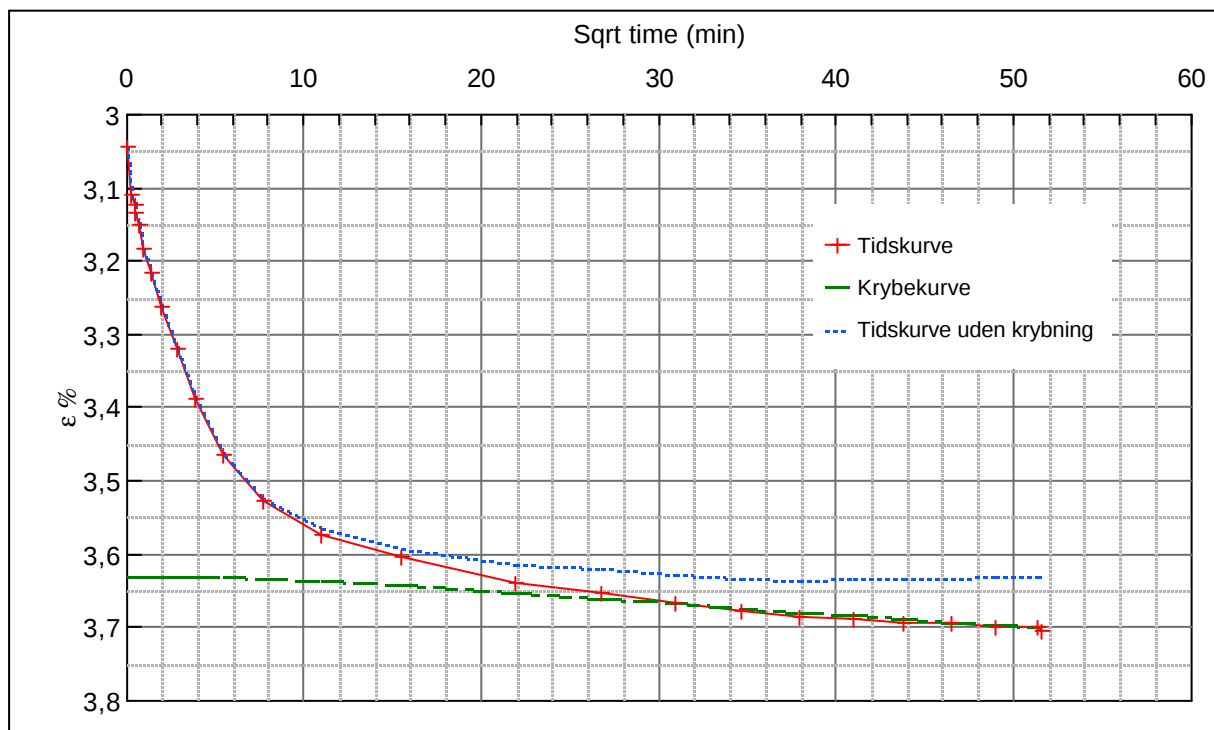
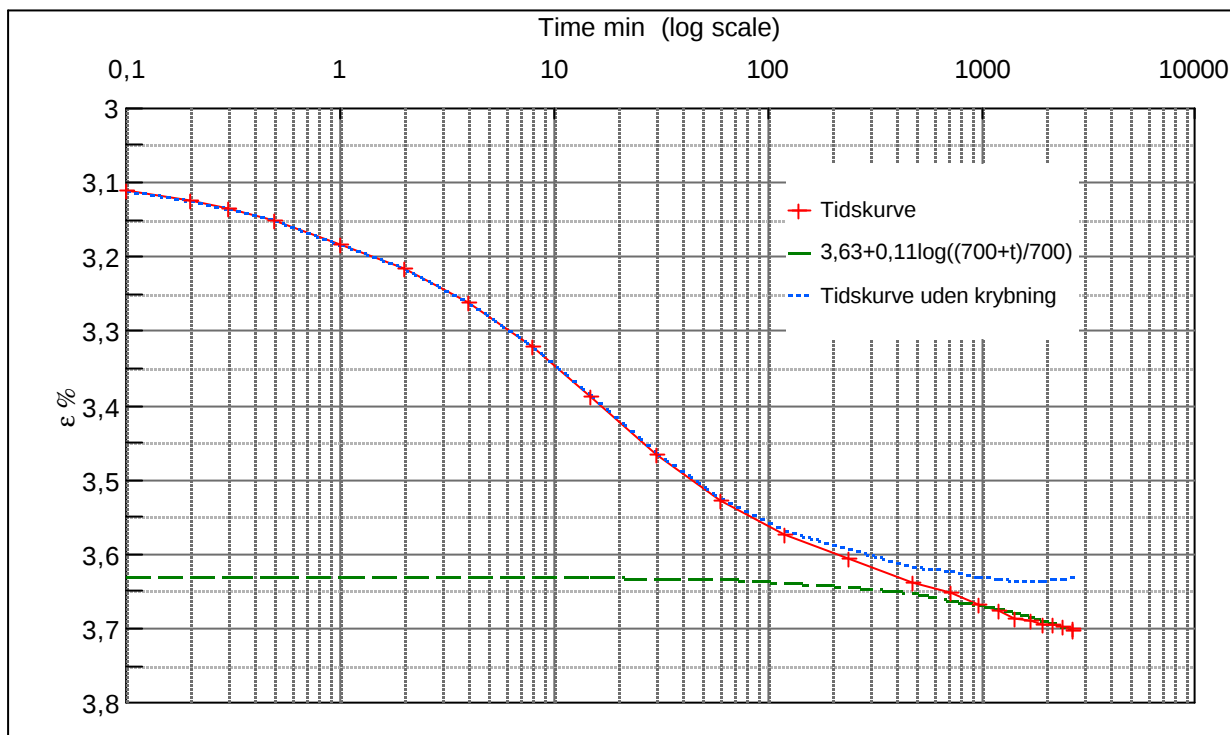
Step no 6	σ	kPa	ϵ	%	ϵ_i		tc in sec	2160
	Before	2.084,2	ϵ_0	1,50	ϵ_c %	2,95	K i kPa	143.900
	After	4.165,9	$\epsilon_{-#}$	3,04	ϵ_s	0,08	k10 m/sec	3,1E-11
					ϵ_{kryb}	0,09	ck10 m ² /sec	4,49E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.8
Executed:	AMS/gt	Check:
Approved:		

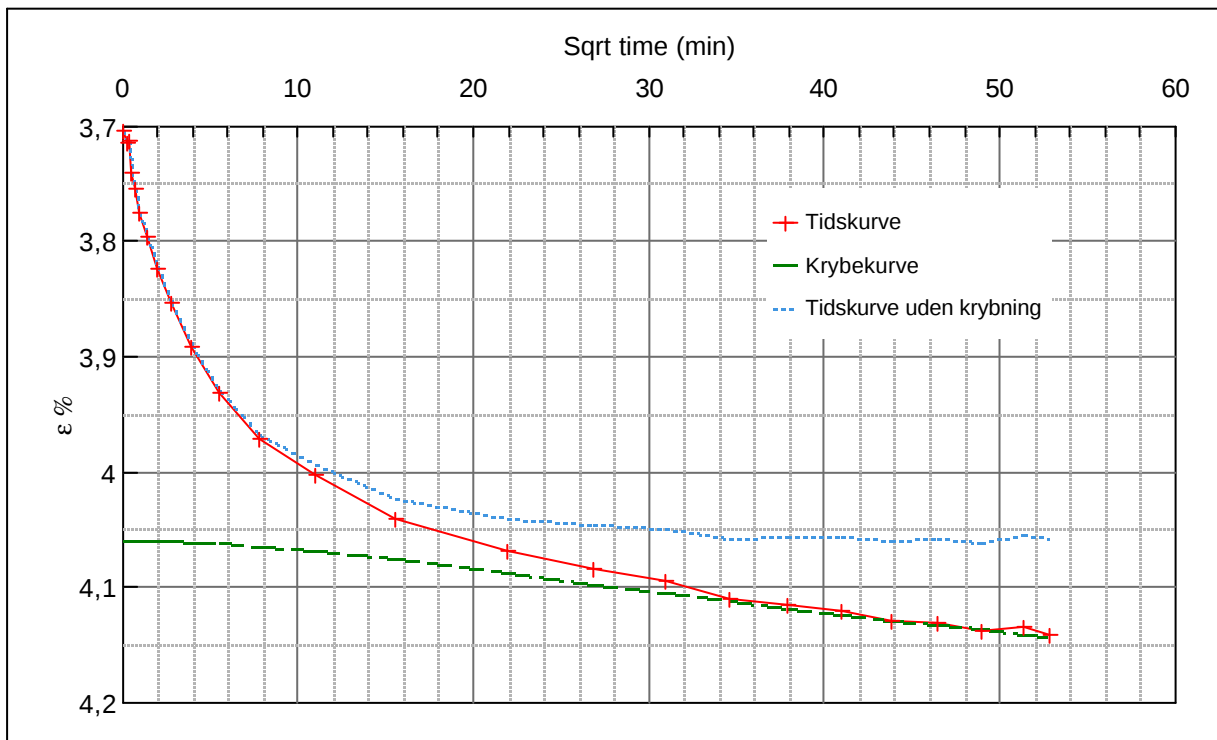
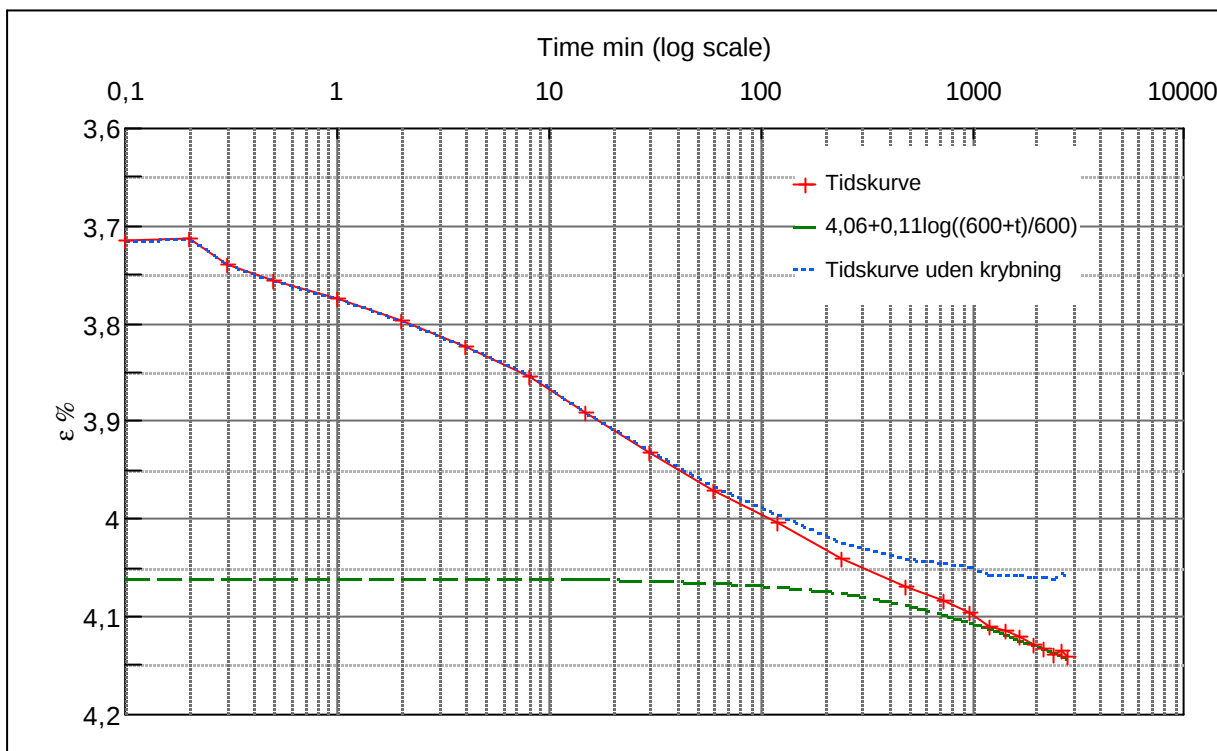
Step no 7	σ	kPa	ϵ	%	ϵ_i		tc in sec	2160
	Before	4.165,9	ϵ_0	3,04	ϵ_c %	3,63	K i kPa	236.562
	After	5.553,8	$\epsilon_{-#}$	3,70	ϵ_s	0,08	k10 m/sec	1,9E-11
					ϵ_{kryb}	0,07	ck10 m ² /sec	4,49E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.9
Executed:	AMS/gt	Check:
Approved:		

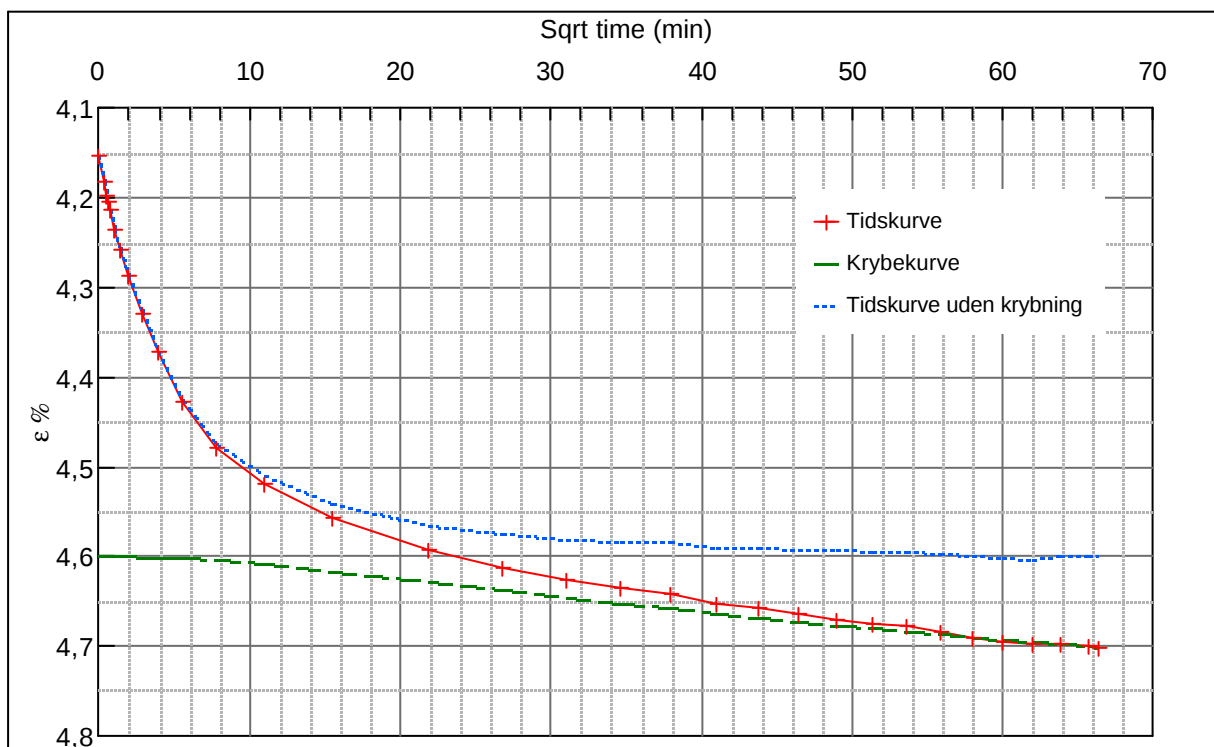
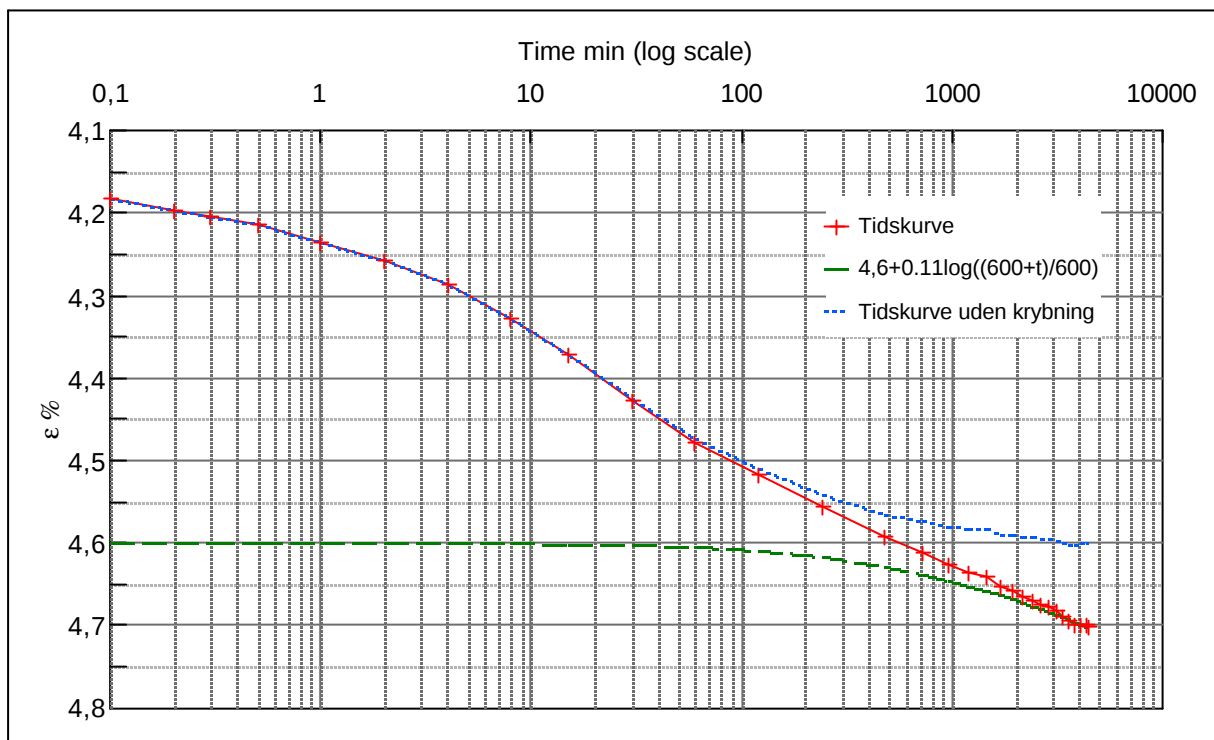
Step no 8	σ	kPa	ϵ	%	ϵ_i		tc in sec	2940
	Before	5.553,8	ϵ_0	3,70	ϵ_c %	4,06	K i kPa	291.834
	After	6.594,6	$\epsilon_{\sim\#}$	4,14	ϵ_s	0,09	k10 m/sec	1,1E-11
					ϵ_{kryb}	0,08	ck10 m ² /sec	3,30E-07



Material: Clay middle jura		
Bor no :	A III	Depth: 162 m.b.s
Lab. no:	k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.10
Executed:	AMS/gt	Check:
Approved:		

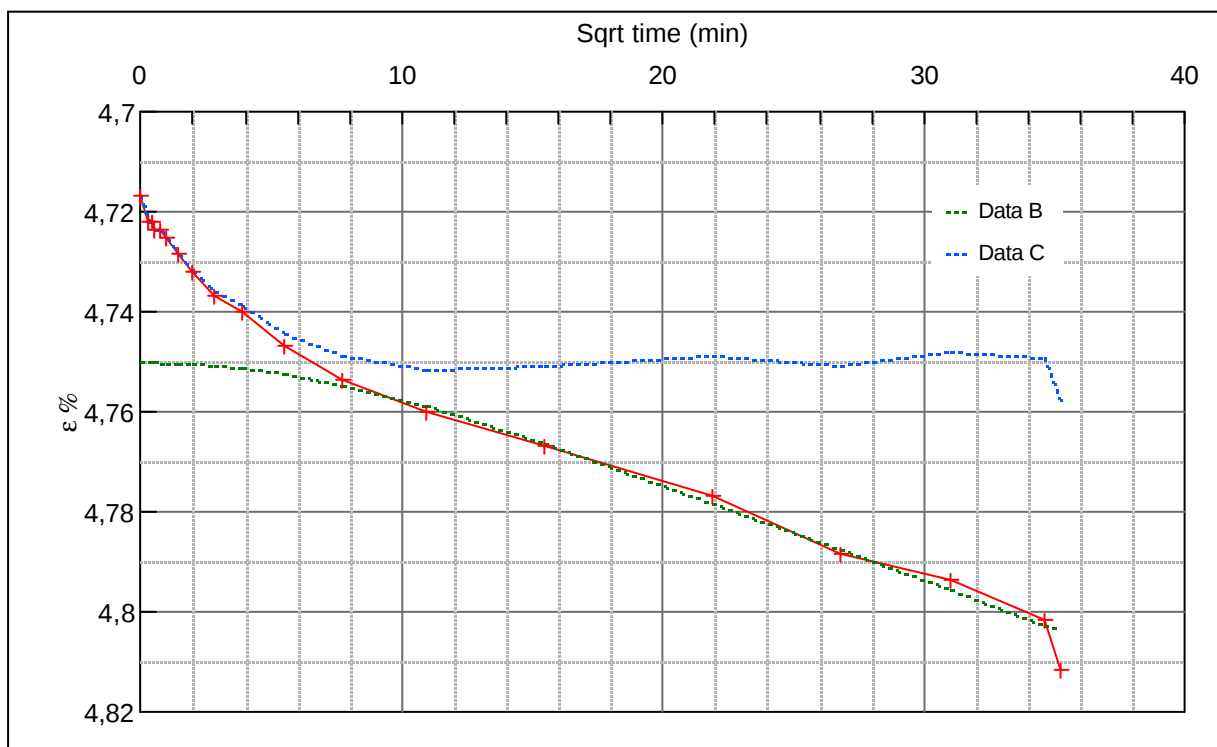
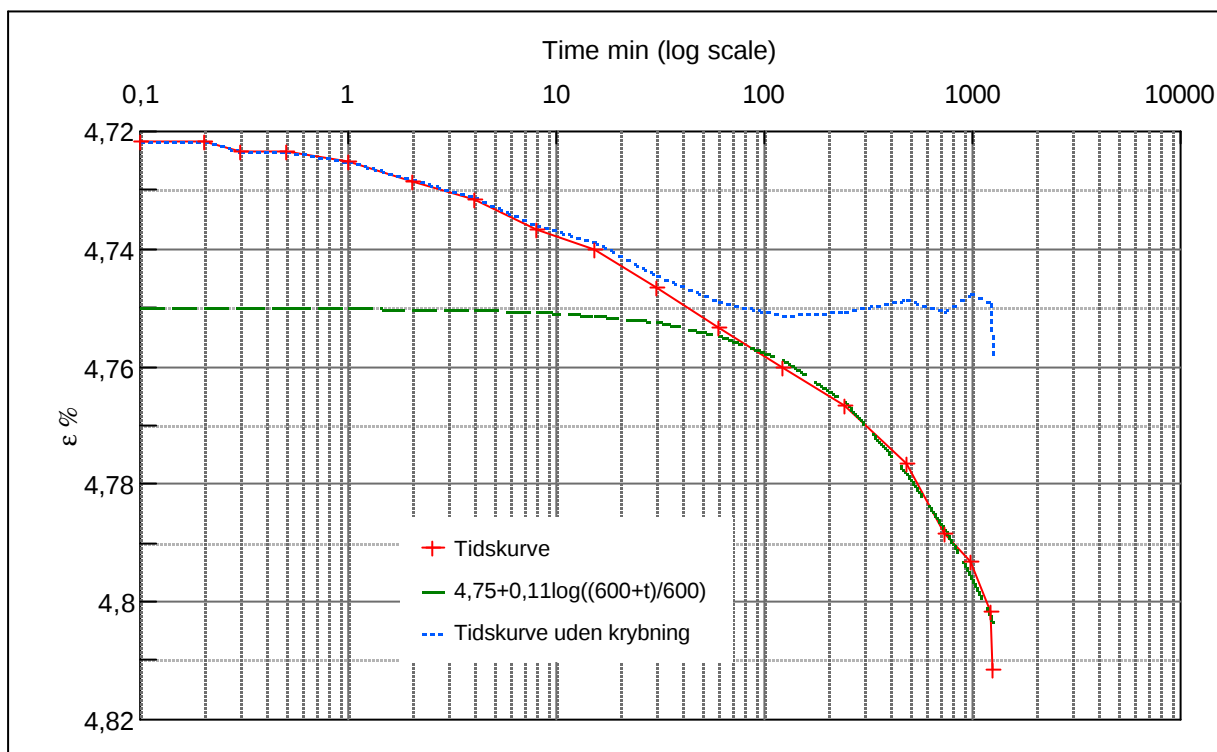
Step no 9	σ	kPa	ε	%	ε_i		tc in sec	2940
	Before	6.594,6	ε_0	4,15	ε_c %	4,6	K i kPa	310.708
	After	7.982,5	$\varepsilon_{\sim\#}$	4,70	ε_s	0,11	k10 m/sec	1,0E-11
					ε_{kryb}	0,10	ck10 m^2/sec	3,30E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.11
Executed:	AMS/gt	Check:
Approved:		

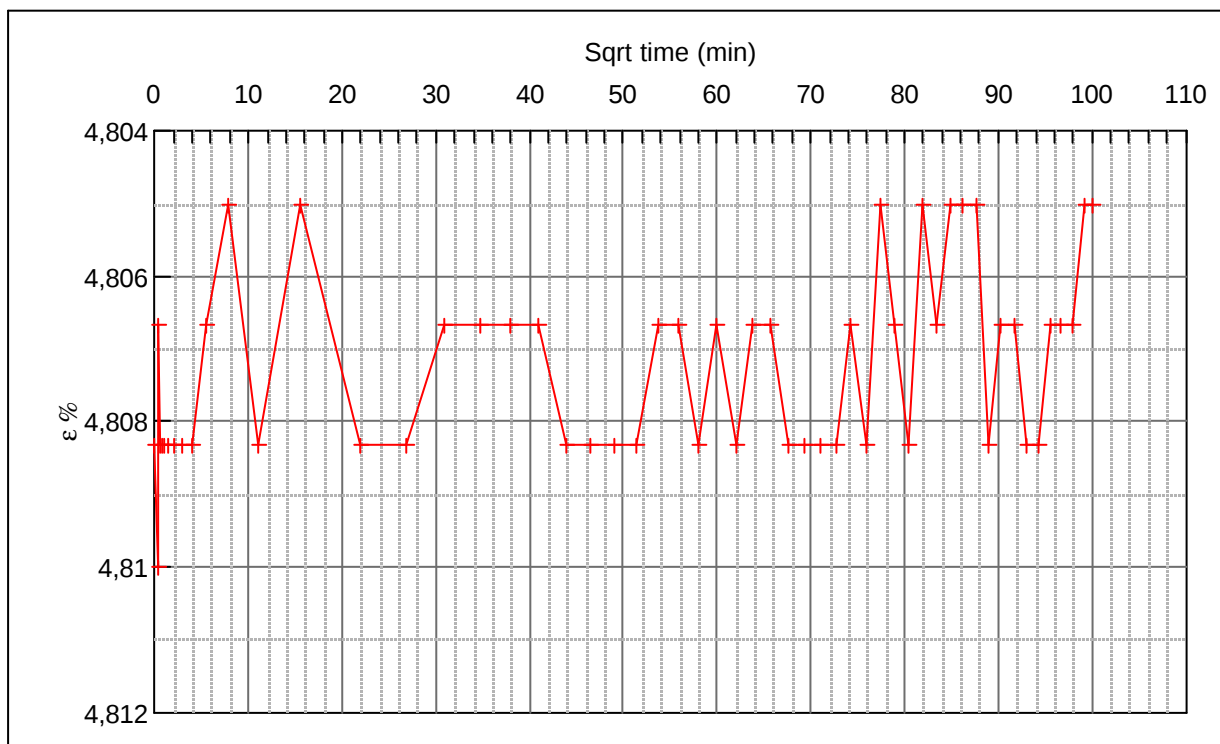
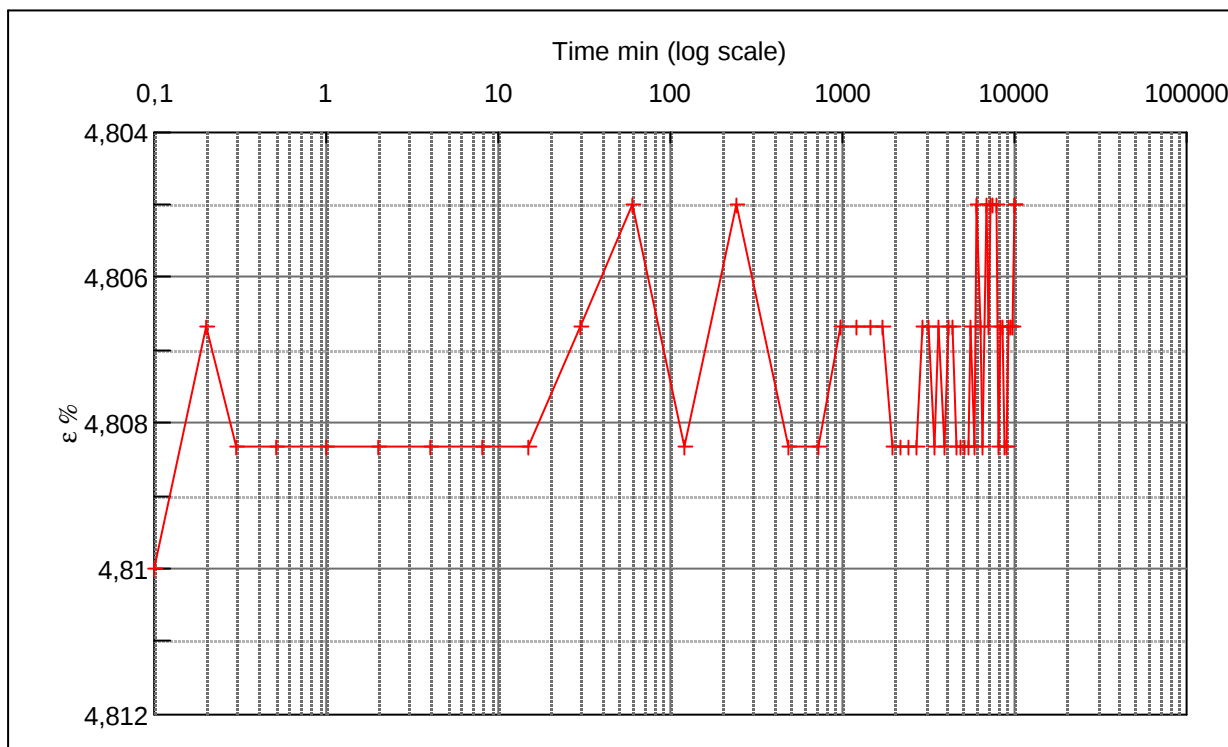
Step no 10	σ	kPa	ϵ	%	ϵ_i		tc in sec	1500
	Before	7.982,5	ϵ_0	4,72	ϵ_c %	4,75	K i kPa	1.040.873
	After	8.329,4	$\epsilon_{\sim\#}$	4,81	ϵ_s	0,11	k10 m/sec	6,1E-12
					ϵ_{kryb}	0,06	ck10 m^2 /sec	6,47E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.12
Executed:	AMS/gt	Check:
Approved:		

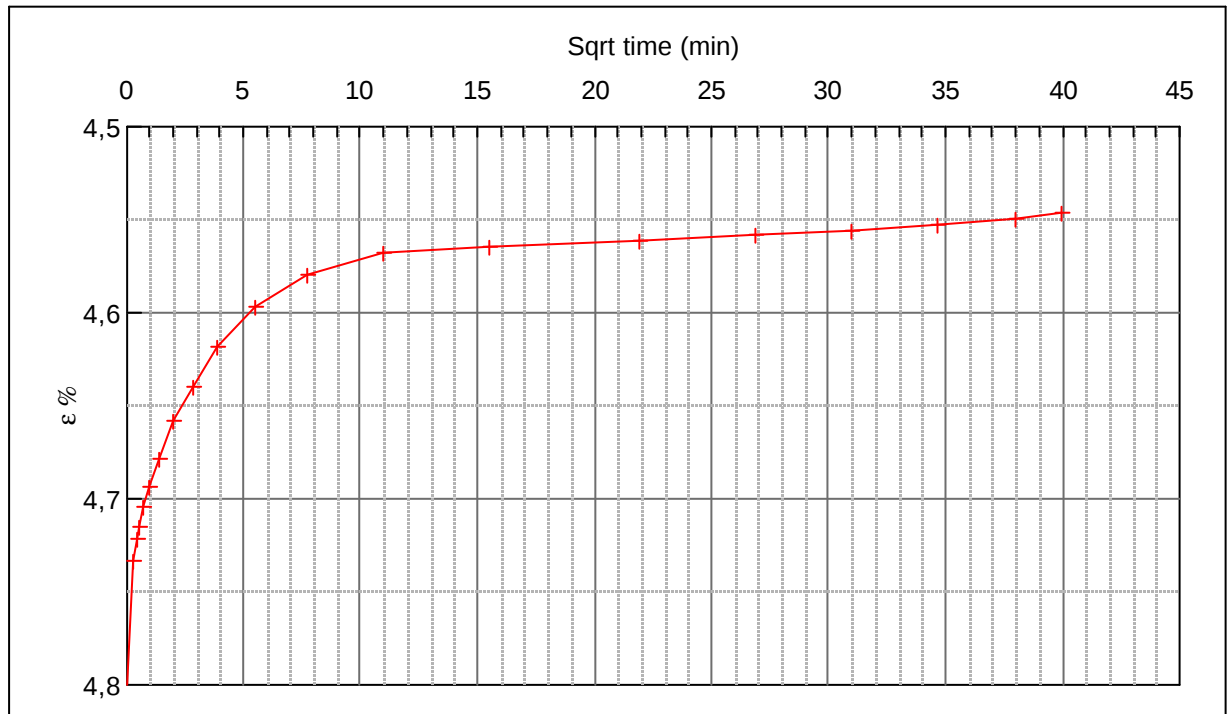
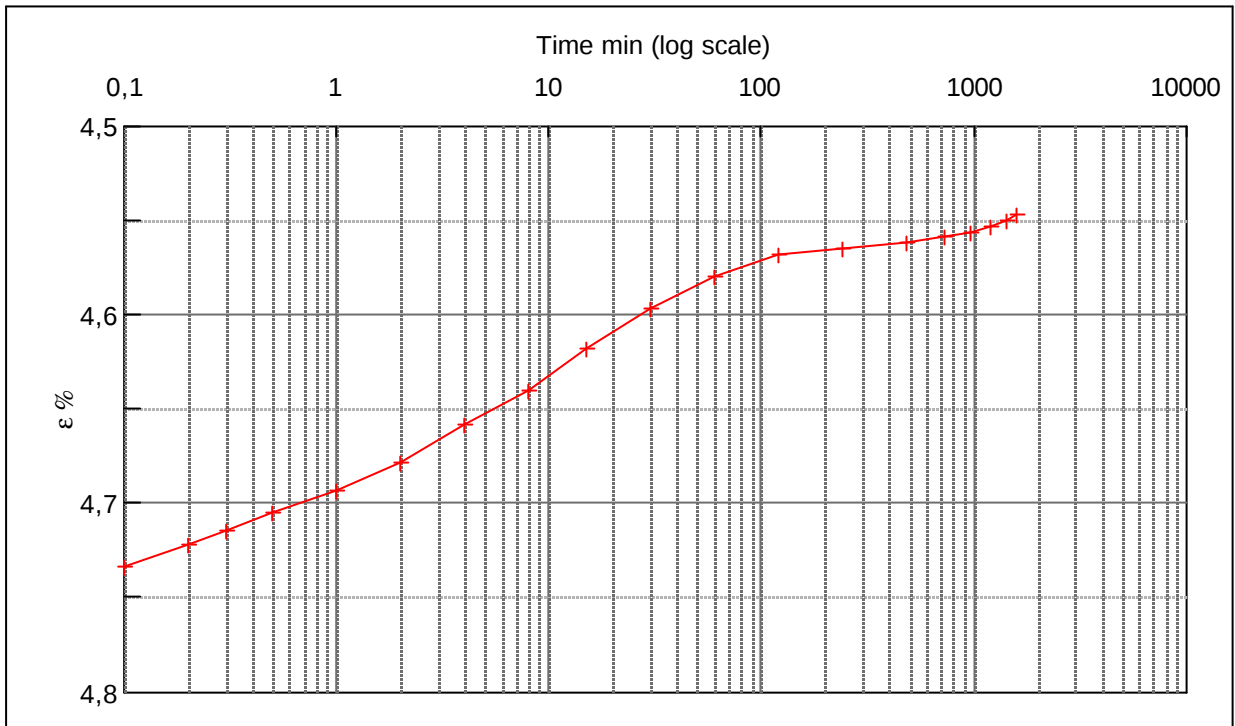
Step no 11	σ	kPa	ϵ	%	ϵ_i	tc in sec	60
	Before	8.329,4	ϵ_0	4,81	ϵ_c %	K i kPa	31.226.200
	After	7.288,5	$\epsilon_{\sim\#}$	4,81	ϵ_s	k10 m/sec	5,1E-12
					ϵ_{kylb}	ck10 m^2 /sec	1,62E-05



Material: Clay middle jura		
Bor no : A III	Depth:	162 m.b.s
Lab. no: k 26	Insitu stress:	~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.13
Executed:	AMS/gt	Check:
Approved:		

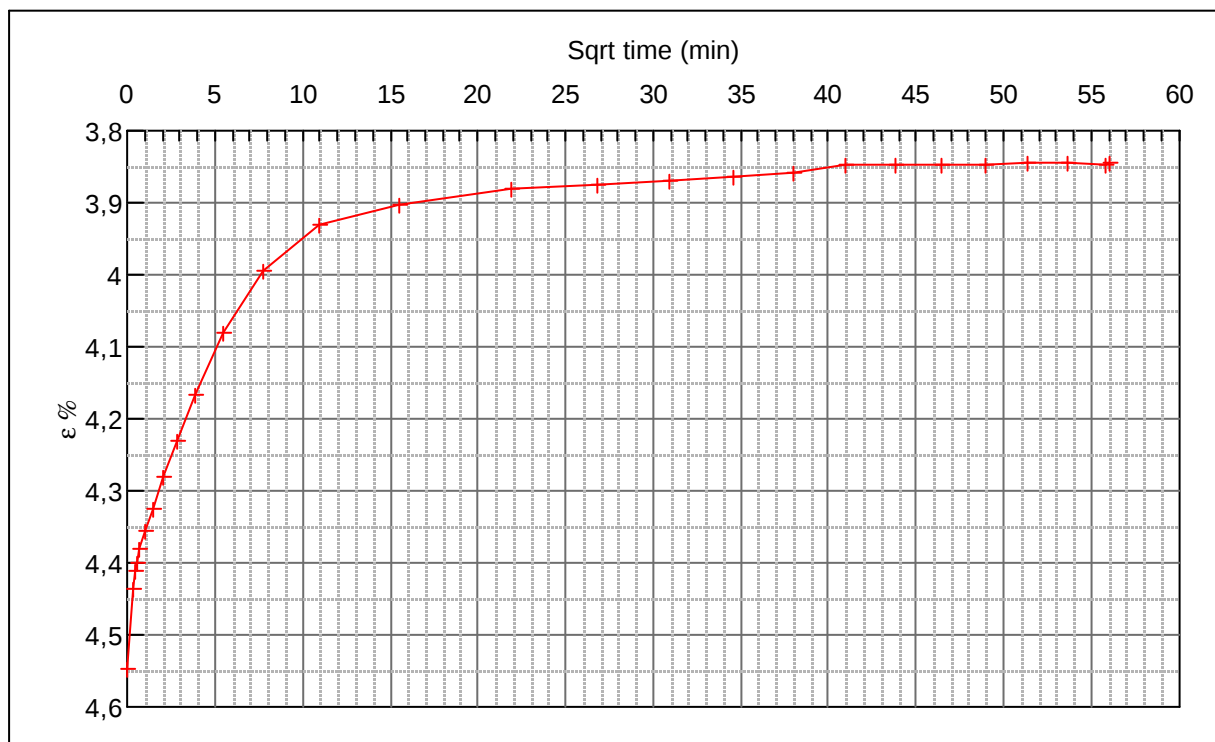
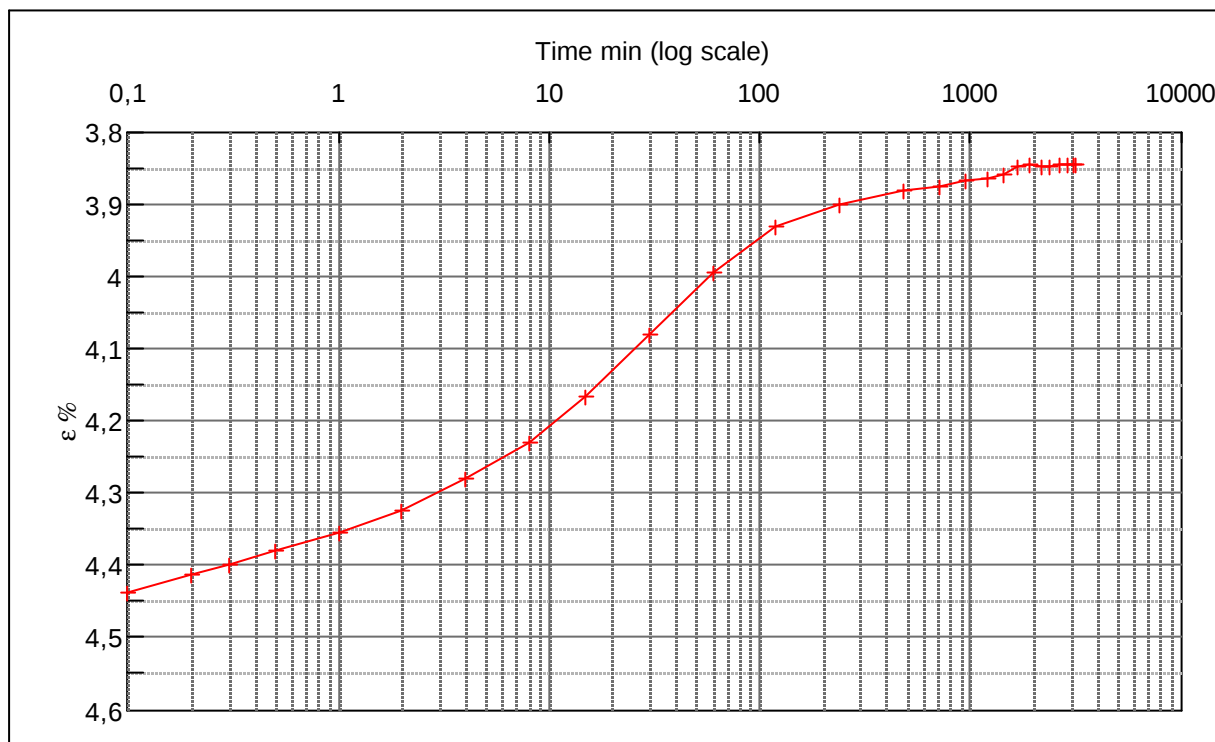
Step no 12	σ	kPa	ϵ	%	ϵ_i	tc in sec	1500
	Before	7.288,5	ϵ_0	4,80	ϵ_c %	K i kPa	1.218.187
	After	4.165,9	$\epsilon_{\sim\#}$	4,55	ϵ_s	k10 m/sec	5,2E-12
					ϵ_{kyb}	ck10 m ² /sec	6,47E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.14
Executed:	AMS/gt	Check:
Approved:		

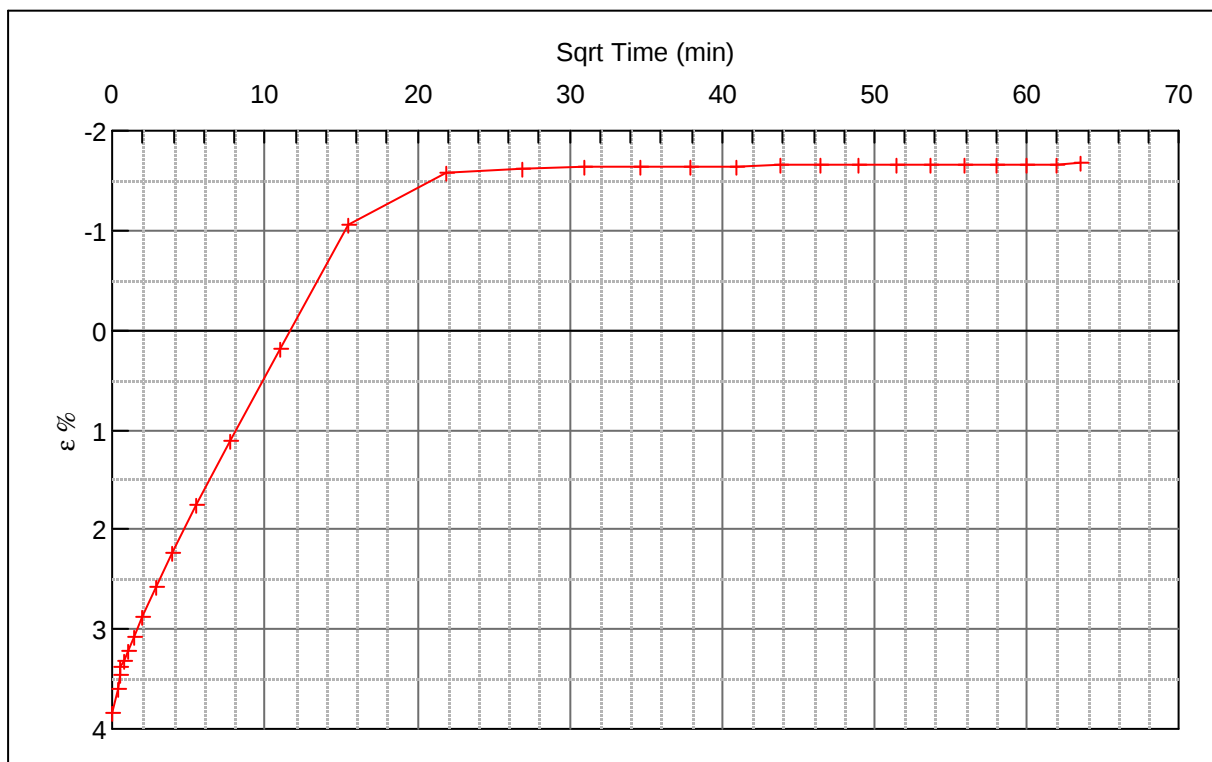
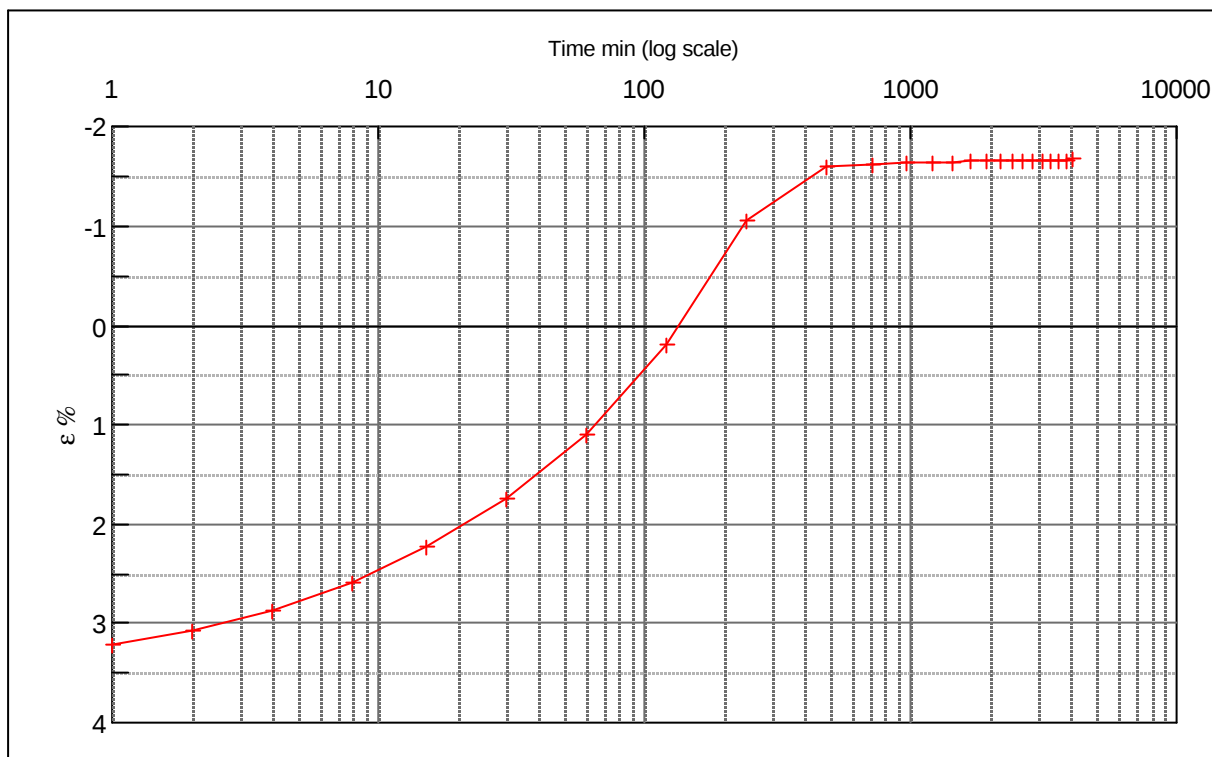
Step no 13	σ	kPa	ϵ	%	ϵ_i		tc in sec	4860
	Before	4.165,9	ϵ_0	4,55	ϵ_c %	3,85	K i kPa	297.392
	After	2.084,2	$\epsilon_{\sim\#}$	3,85	ϵ_s		k10 m/sec	6,6E-12
					ϵ_{kryb}		ck10 m ² /sec	2,00E-07



Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.15
Executed:	AMS/gt	Check:
Approved:		

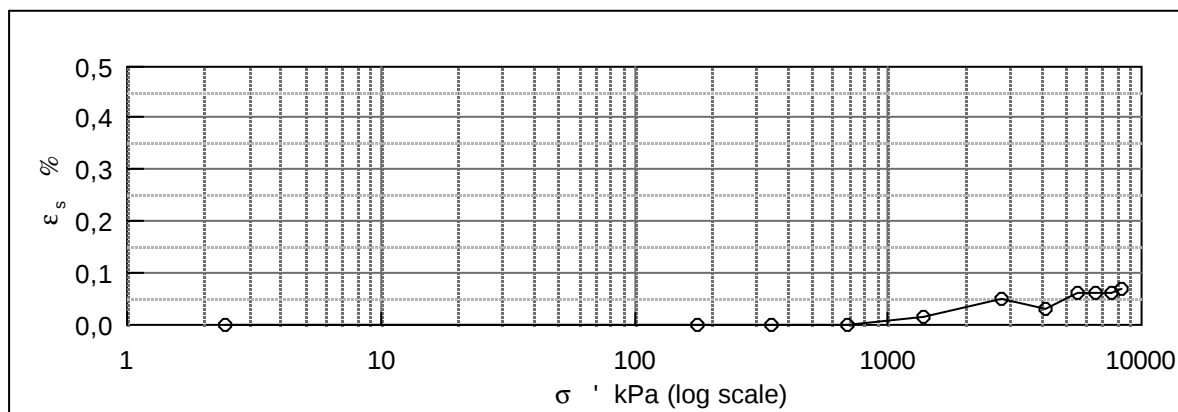
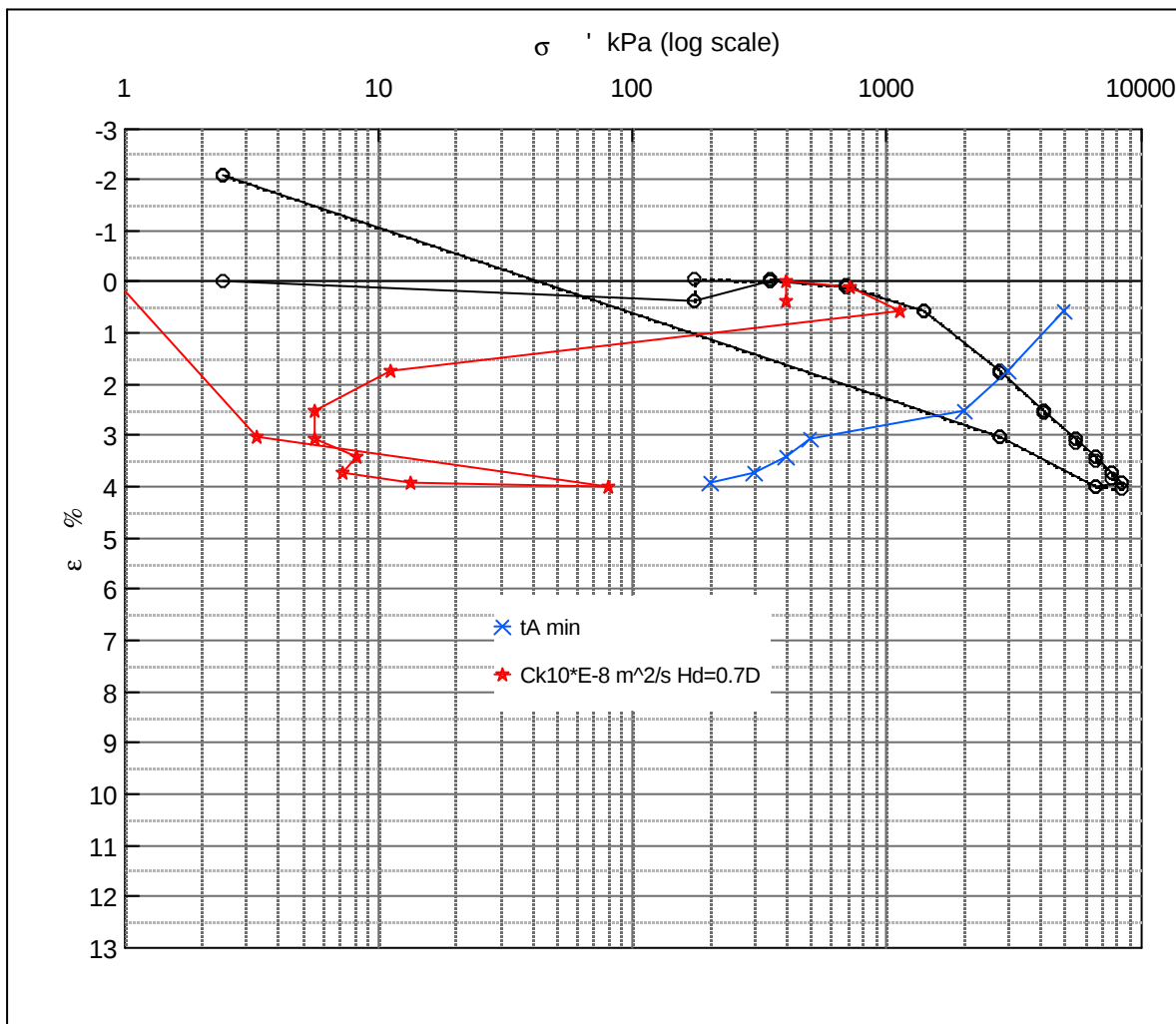
Step no 14	σ	kPa	ε	%	ε_i	ε_c % (1,69)	tc in sec	17340	K_i kPa	37.590	k_{10} m/sec	1,5E-11	ck_{10} m^2 /sec	5,59E-08
	Before	2.084,2	ε_0	3,85	ε_s									
	After	2,43	$\varepsilon_{\sim\#}$	(1,69)	ε_{kryb}									



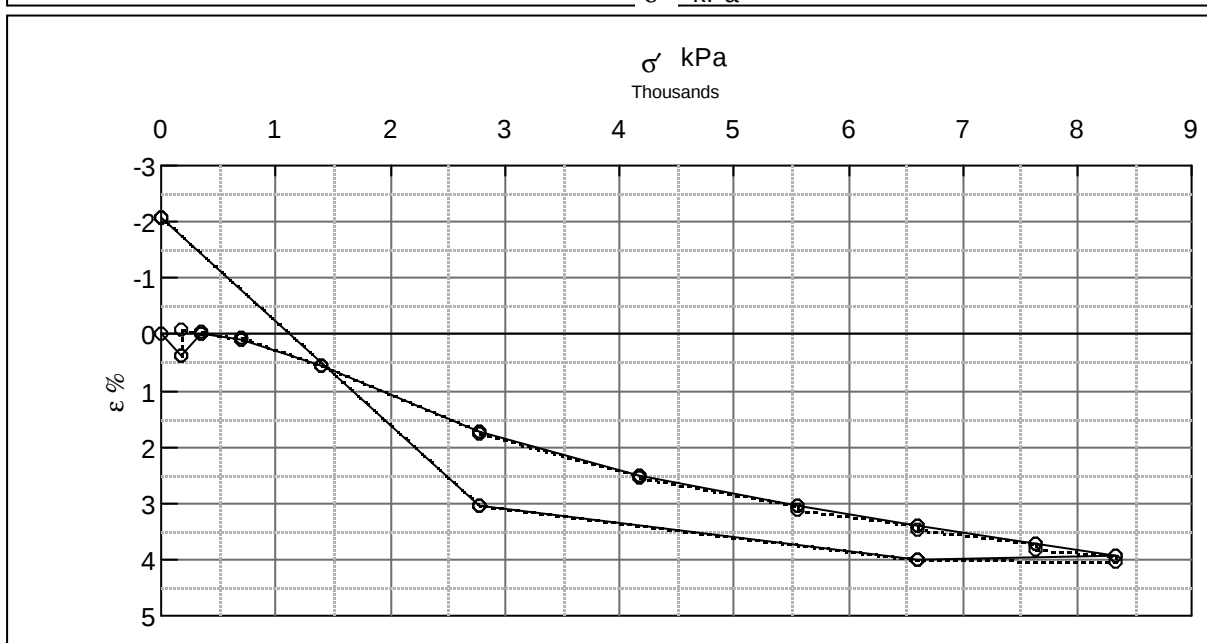
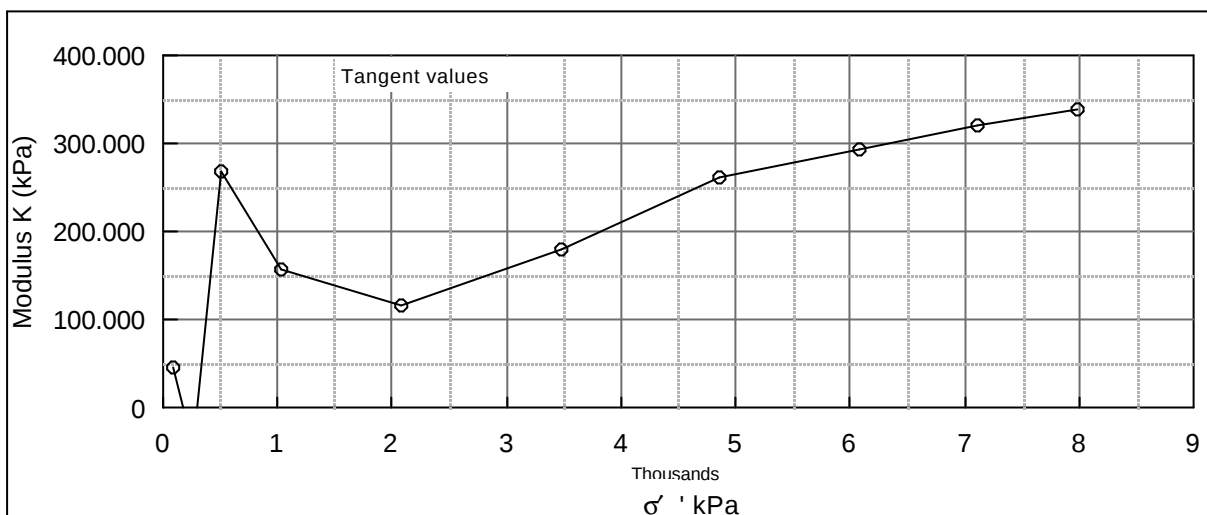
Material: Clay middle jura	
Bor no : A III	Depth: 162 m.b.s
Lab. no: k 26	Insitu stress: ~1620 kPa

Job:	Anholt	AAU
		Encl. No 5.16
Executed:	AMS/gt	Check:
Approved:		

Description of soil: Clay, Lower Jura			Water content %	Before	After
			Bulk density Mg / m ³	16,8	20,3
			Grain density Mg / m ³	2,16	2,1
			Void ratio	~2.7	0,55
Bor no : A IV	Overburden pressure σ'_o	~3040 kPa	Degr. of Saturation %	99	100
Lab. no: k98	Vane strength c_v	kPa	Dimension H x D mm	30x60	30.1x60
Level : 304 m.b.s	CPT - value q_c	MPa			



Job: Anholt		AAU
		Encl. No 6.1
Executed:	AMS/gt	Check:
Approved:		



Test results

Q ~5 %
 Qs ~0.07 %
 σ_{pc} >3000 kPa

σ' kPa	ε_c %	ε_s % / lct	Ck10 m ² /s	σ_m kPa	K kPa	w %
2,4	0,00	0,00				16,8
175,9	0,38	0,00	4,0E-06	89,2	45652,3	16,5
349,4	(0,03)	0,00	4,0E-06	262,6	-42311,9	16,8
696,3	0,10	0,00	7,2E-06	522,9	266890,6	16,7
1.390,3	0,55	0,02	1,1E-05	1.043,3	155936,1	16,3
2.778,1	1,74	0,05	1,1E-07	2.084,2	116136,5	15,3
4.165,9	2,52	0,03	5,6E-08	3.472,0	177927,1	14,7
5.553,8	3,05	0,06	5,6E-08	4.859,8	261854,9	14,2
6.594,6	3,41	0,06	8,2E-08	6.074,2	293203,8	13,9
7.635,5	3,73	0,06	7,2E-08	7.115,1	320268,7	13,6
8.329,4	3,94	0,07	1,3E-07	7.982,5	336852,2	13,5
6.594,6	3,99		8,0E-07	7.462,0	-3401546,8	13,4
2.778,1	3,03		3,3E-08	4.686,4	399637,2	14,2
2,4	(2,08)		3,8E-09	1.390,3	54265,1	18,6

Remark:

Sandsynligvis en genbelastningsgren
 Den normalkonsoliderede tilstand er ikke nået

Job: Anholt

AAU

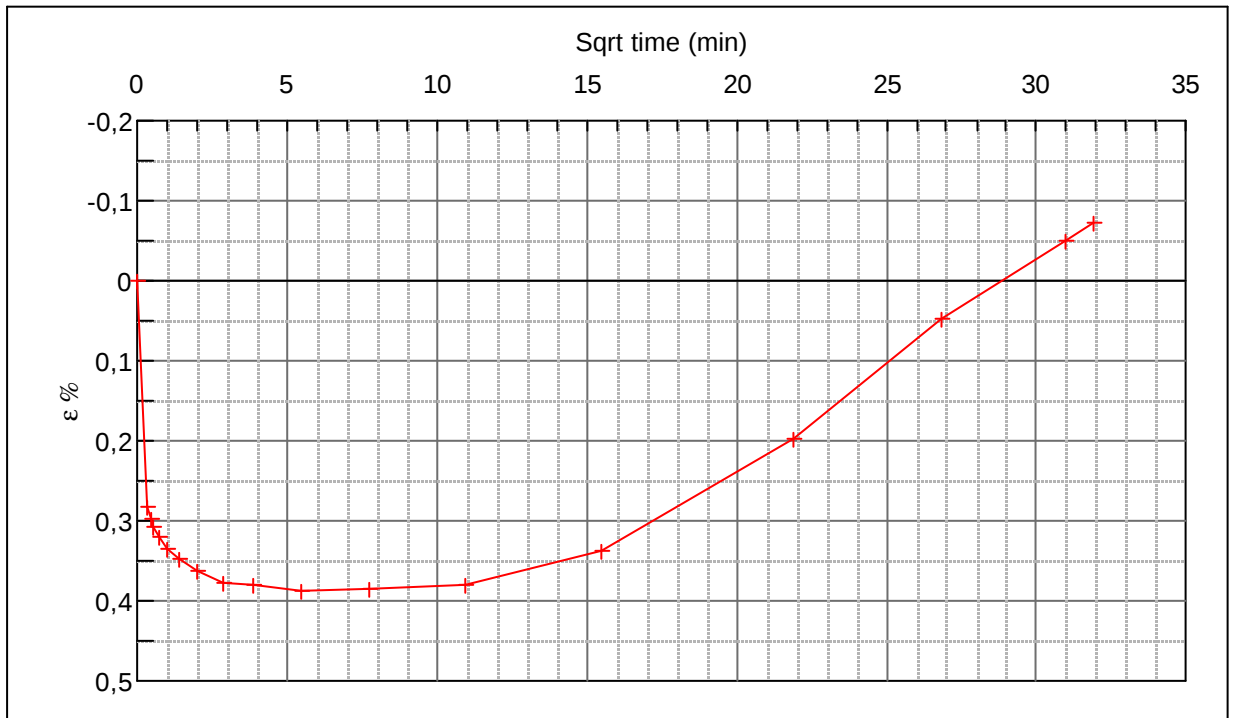
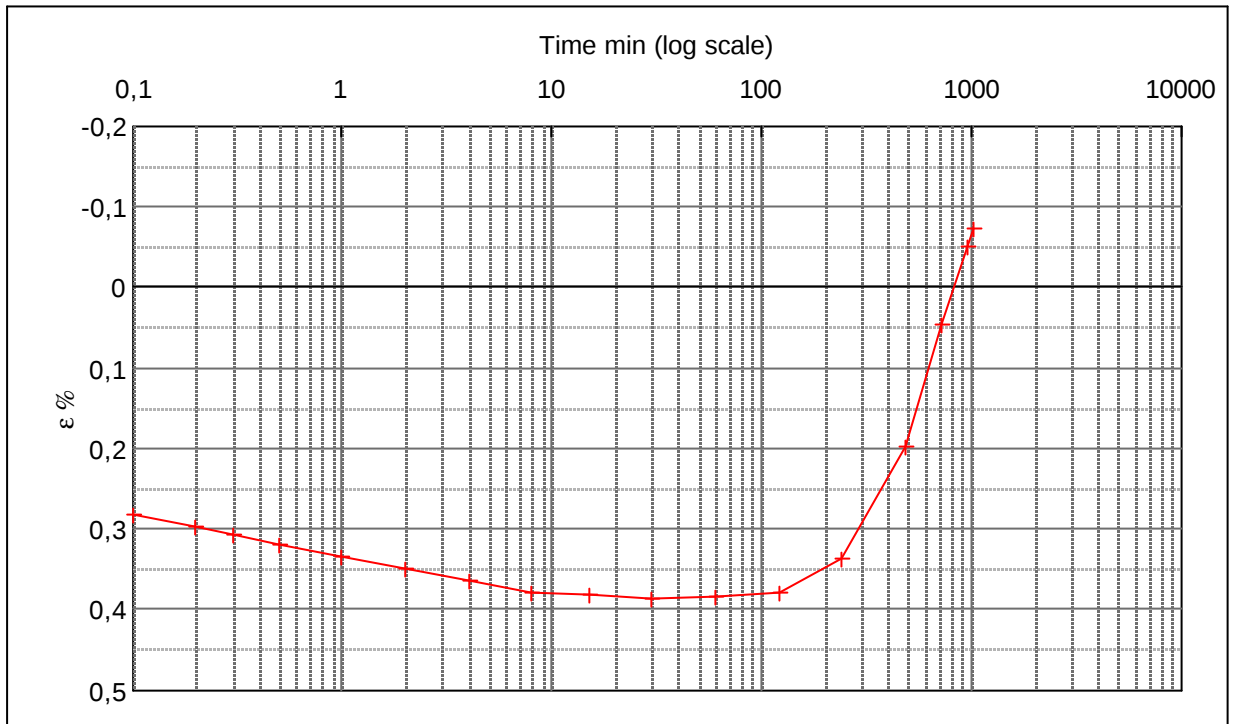
Encl. No
6.2

Executed: AMS/gt

Check:

Approved:

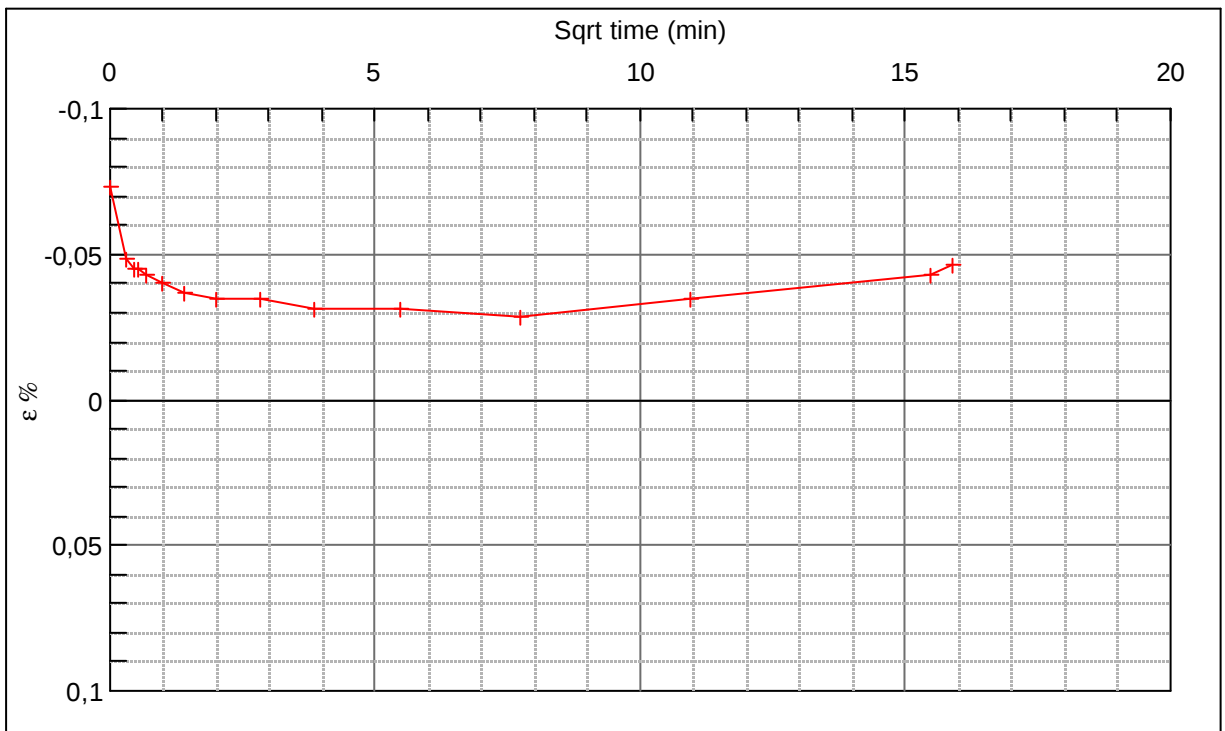
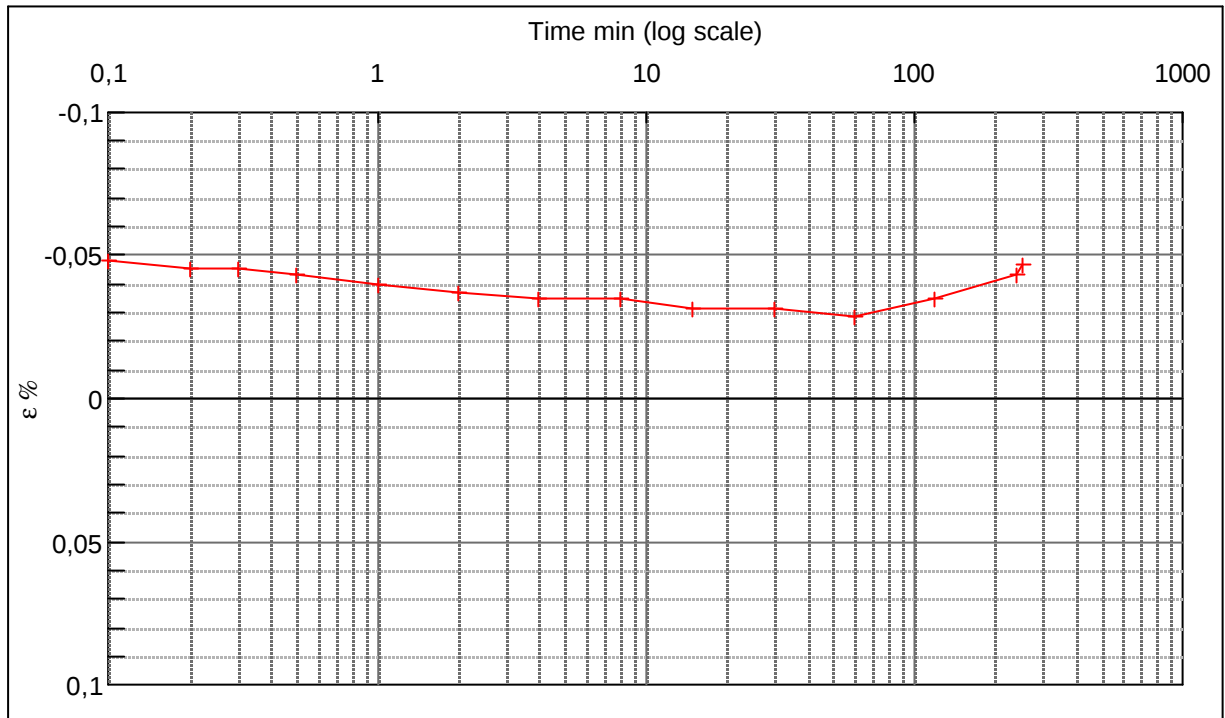
Step no 1	σ	kPa	ϵ	%	ϵ_i		tc in sec	240
	Before	2,43	ϵ_0	0,00	ϵ_c %	0,38	K i kPa	45.652
	After	175,9	$\epsilon_{\sim\#}$	(0,07)	ϵ_s		k10 m/sec	8,7E-10
					ϵ_{kyb}		ck10 m^2 /sec	4,04E-06



Material:	
Clay, Lower Jura	
Bor no :	A IV
Depth:	304 m.b.s
Lab. no:	k98
Insitu stress ~3040 kPa	

Job:	Anholt	AAU
		Encl. No 6.3
Executed:	AMS/gt	Check:
Approved:		

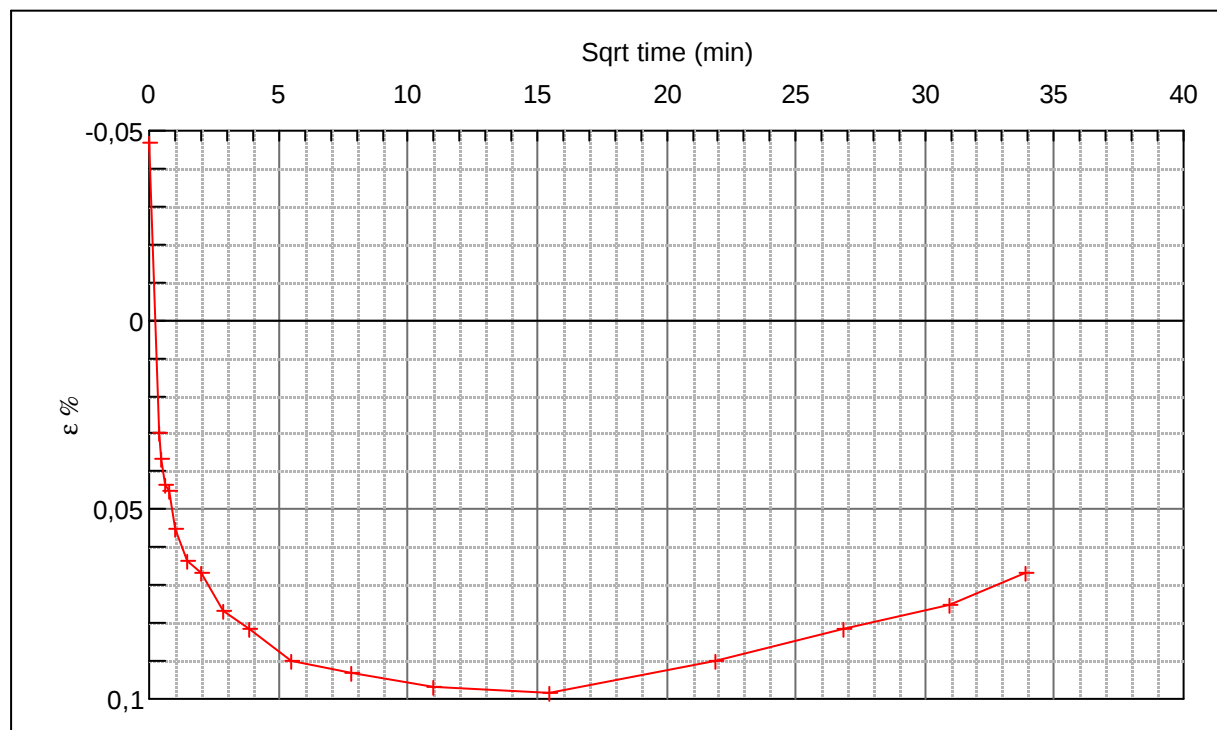
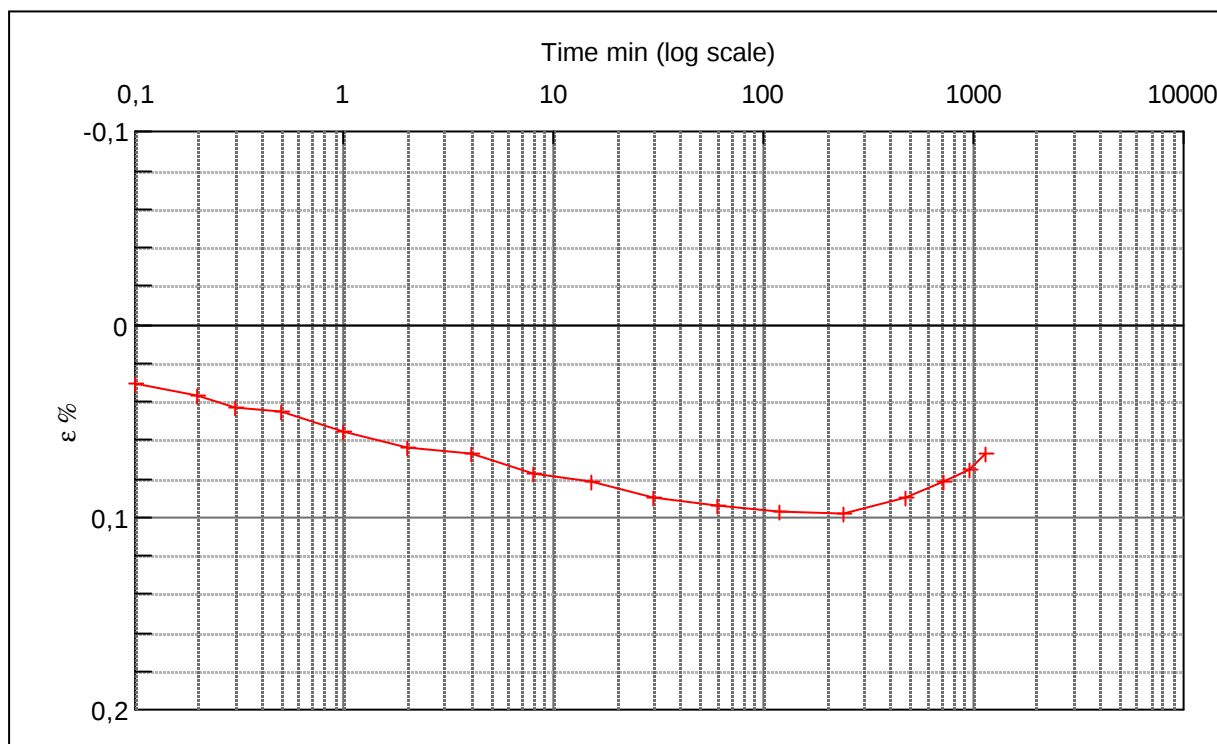
Step no 2	σ	kPa	ϵ	%	ϵ_i	tc in sec	240
	Before	175,9	ϵ_0	(0,07)	ϵ_c %	K i kPa	400.336
	After	349,4	$\epsilon_{\sim\#}$	(0,05)	ϵ_s	k10 m/sec	9,9E-11
					ϵ_{kyb}	ck10 m ² /sec	4,04E-06



Material:	
Clay, Lower Jura	
Bor no :	A IV
Depth:	304 m.b.s
Lab. no:	k98
Insitu stress ~3040 kPa	

Job:	Anholt	AAU
		Encl. No 6.4
Executed:	AMS/gt	Check:
Approved:		

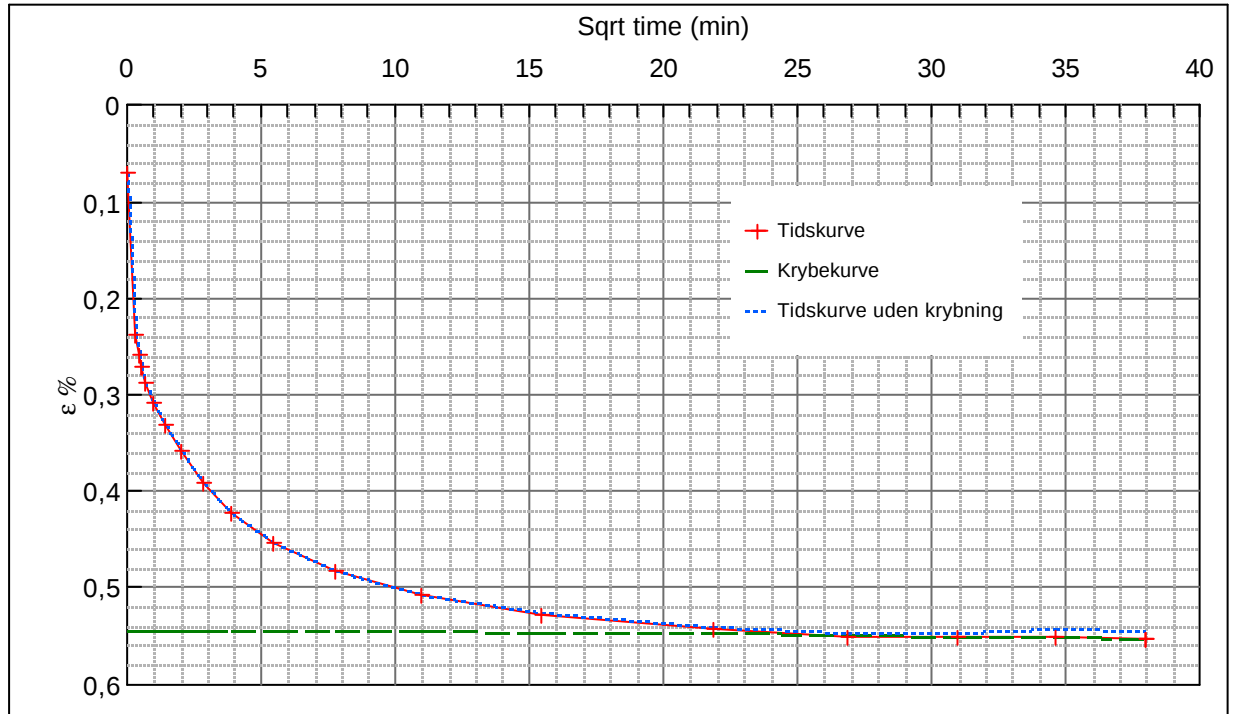
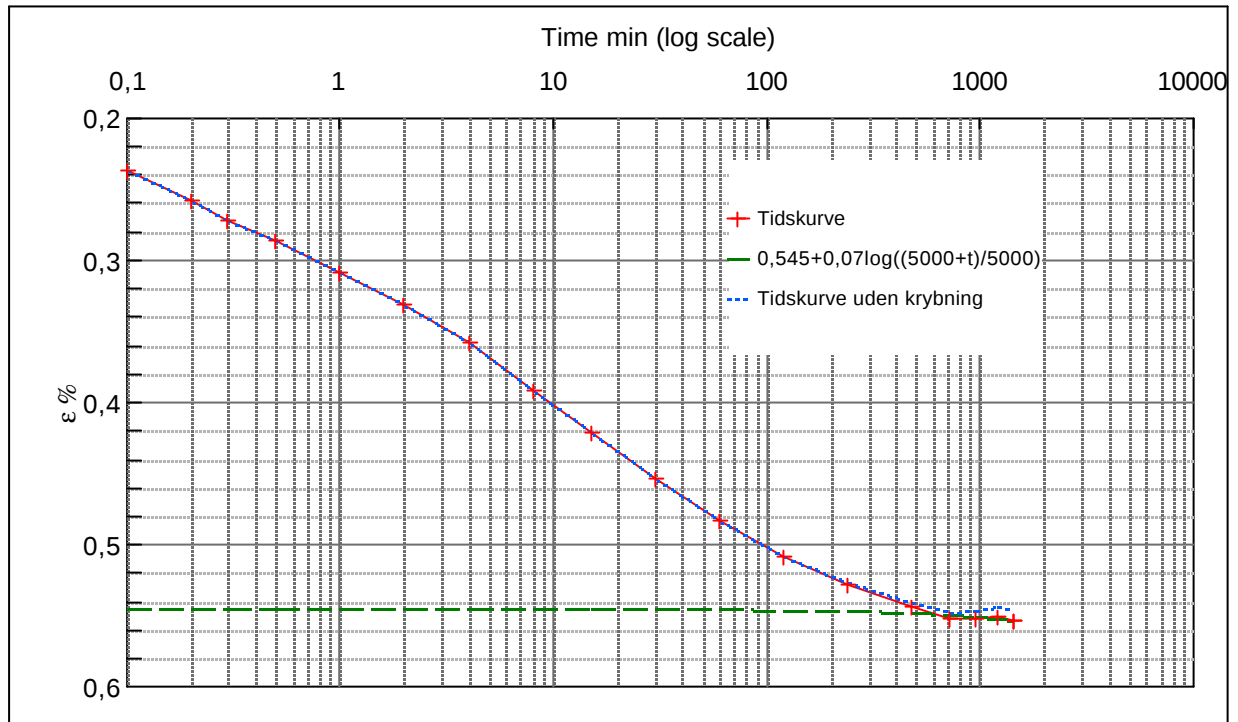
Step no 3	σ	kPa	ε	%	ε_i		tc in sec	135
	Before	349,4	ε_0	(0,05)	ε_c %	0,10	K i kPa	236.562
	After	696,3	$\varepsilon_{-#}$	0,07	ε_s		k10 m/sec	3,0E-10
					ε_{kryb}		ck10 m ² /sec	7,18E-06



Material: Clay, Lower Jura	
Bor no : A IV	Depth: 304 m.b.s
Lab. no: k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.5
Executed:	AMS/gt	Check:
Approved:		

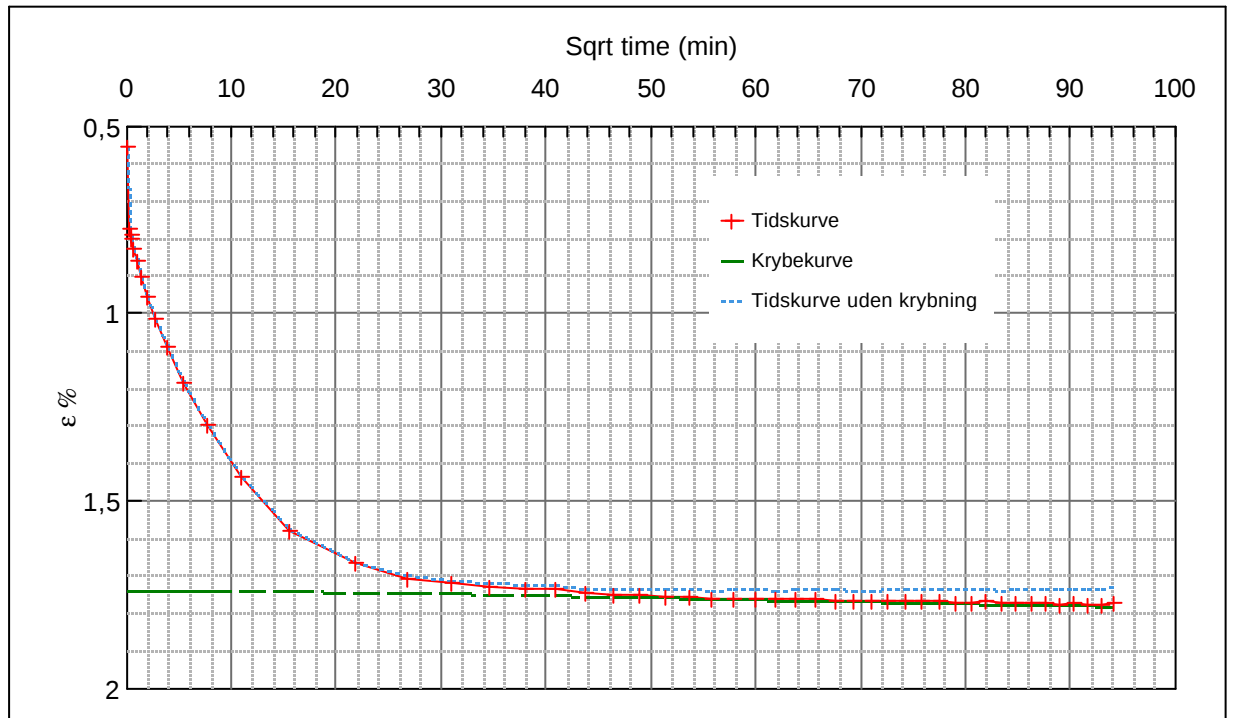
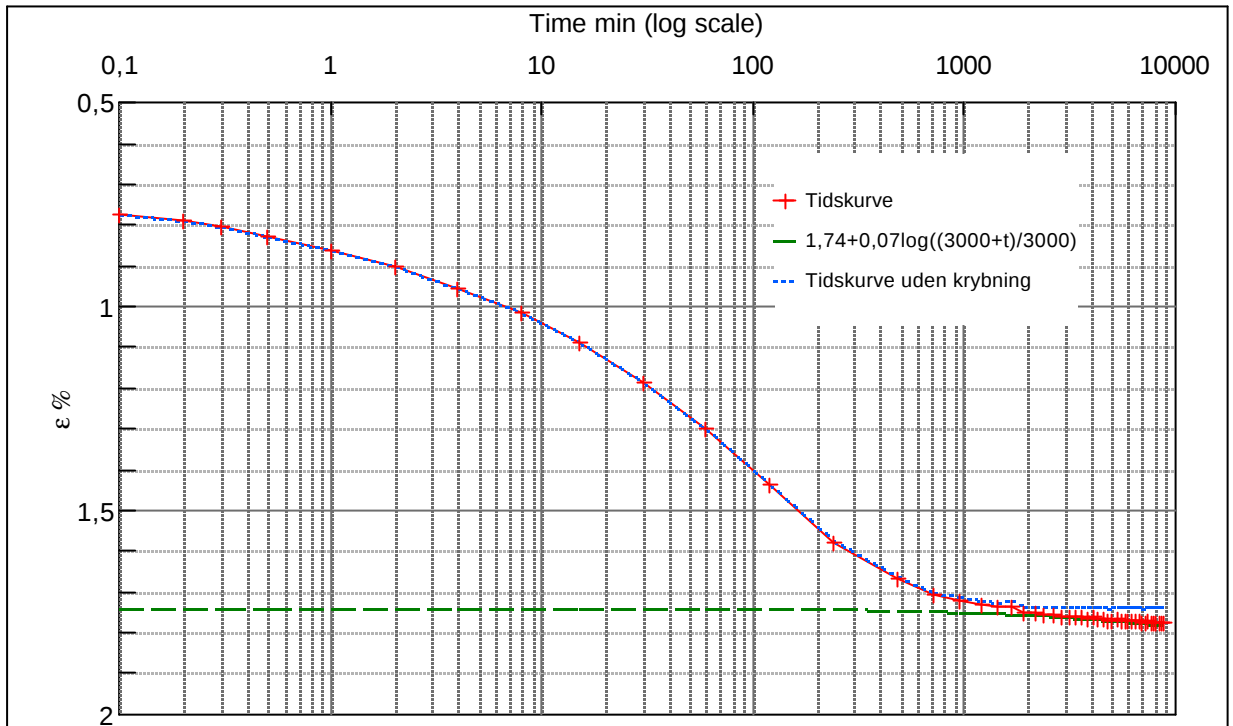
Step no 4	σ	kPa	ϵ	%	ϵ_i		tc in sec	86,4
	Before	696,3	ϵ_0	0,07	ϵ_c %	0,545	K i kPa	146.087
	After	1.390,3	$\epsilon_{\sim\#}$	0,55	ϵ_s	0,015	k10 m/sec	7,5E-10
					ϵ_{kryb}	0,01	ck10 m^2 /sec	1,12E-05



Material: Clay, Lower Jura	
Bor no : A IV	Depth: 304 m.b.s
Lab. no: k98	Insitu stress ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.6
Executed:	AMS/gt	Check:
Approved:		

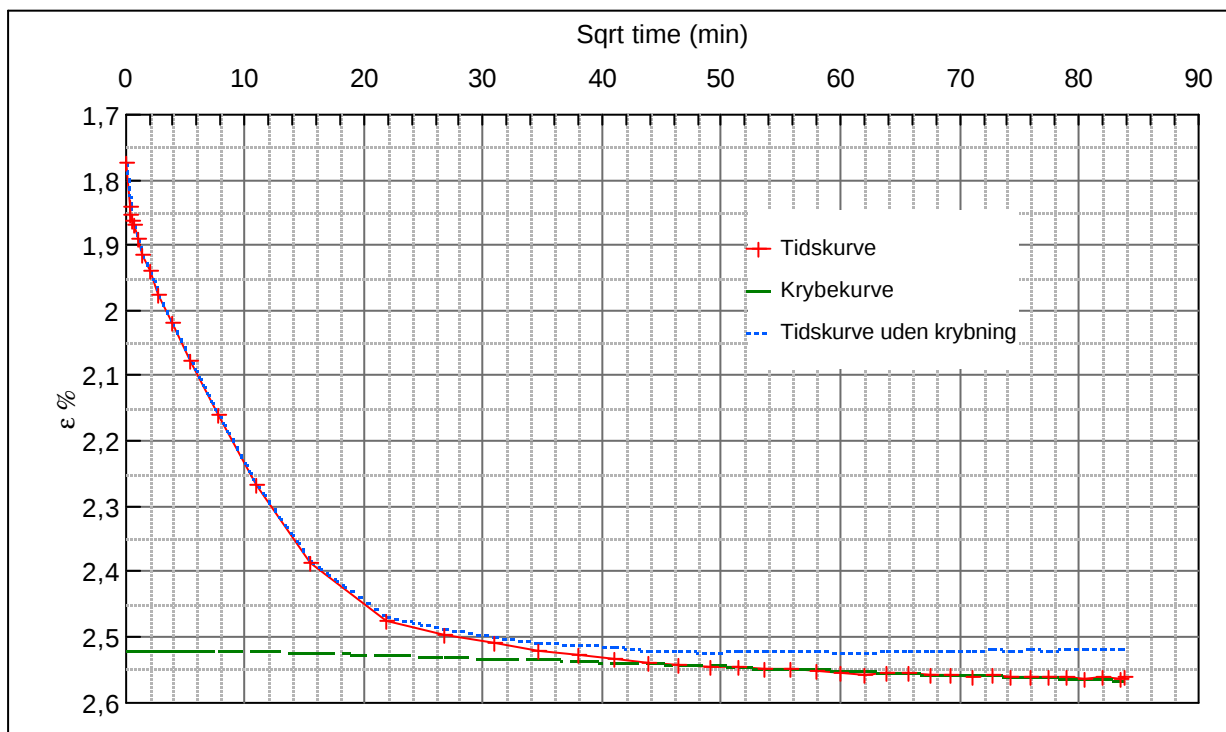
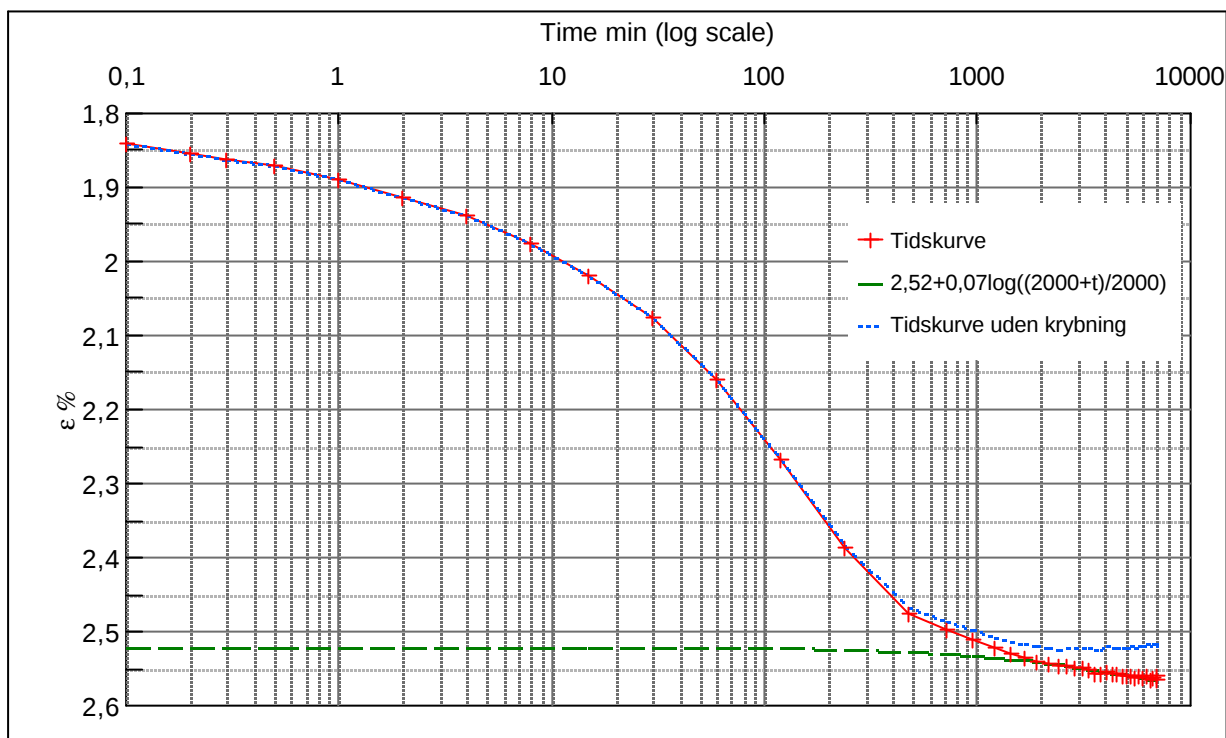
Step no 5	σ	kPa	ϵ	%	ϵ_i		t_c in sec	8640
	Before	1.390,3	ϵ_0	0,56	ϵ_c %	1,74	K_i kPa	117.117
	After	2.778,1	$\epsilon_{\sim\#}$	1,77	ϵ_s	0,05	k_{10} m/sec	9,4E-12
					ϵ_{kryb}	0,03	ck_{10} m ² /sec	1,12E-07



Material:	
Clay, Lower Jura	
Bor no :	A IV
Depth:	304 m.b.s
Lab. no:	k98
Insitu stress ~3040 kPa	

Job:	Anholt	AAU
		Encl. No 6.7
Executed:	AMS/gt	Check:
Approved:		

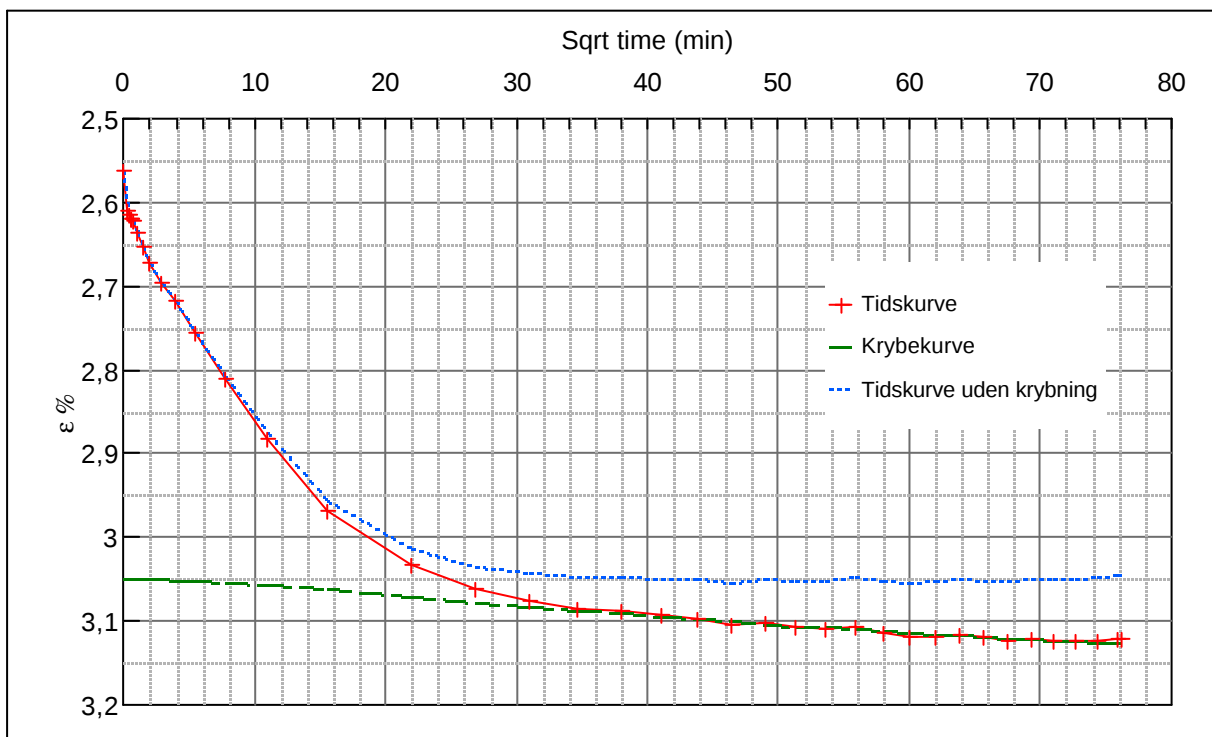
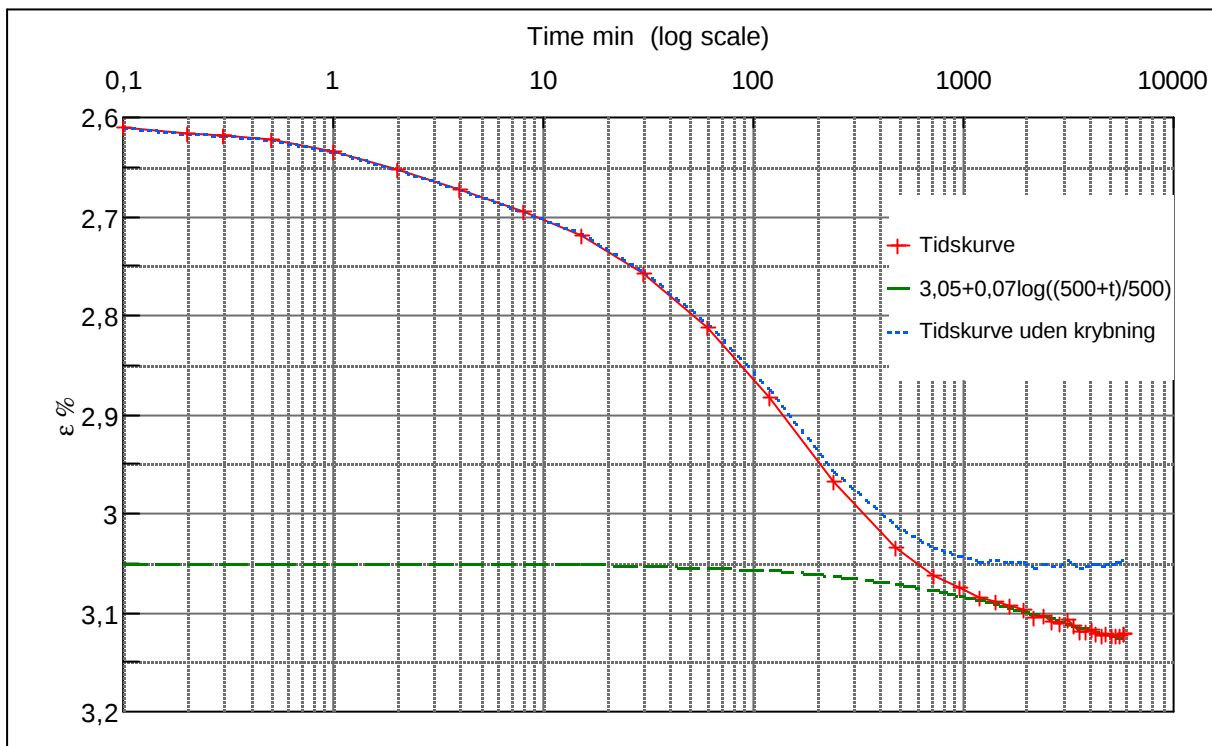
Step no 6	σ	kPa	ϵ	%	ϵ_i		tc in sec	17340
	Before	2.778,1	ϵ_0	1,78	ϵ_c %	2,52	K i kPa	186.286
	After	4.165,9	$\epsilon_{-#}$	2,56	ϵ_s	0,03	k10 m/sec	2,9E-12
					ϵ_{kryb}	0,04	ck10 m ² /sec	5,59E-08



Material: Clay, Lower Jura		
Bor no :	A IV	Depth: 304 m.b.s
Lab. no:	k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.8
Executed:	AMS/gt	Check:
Approved:		

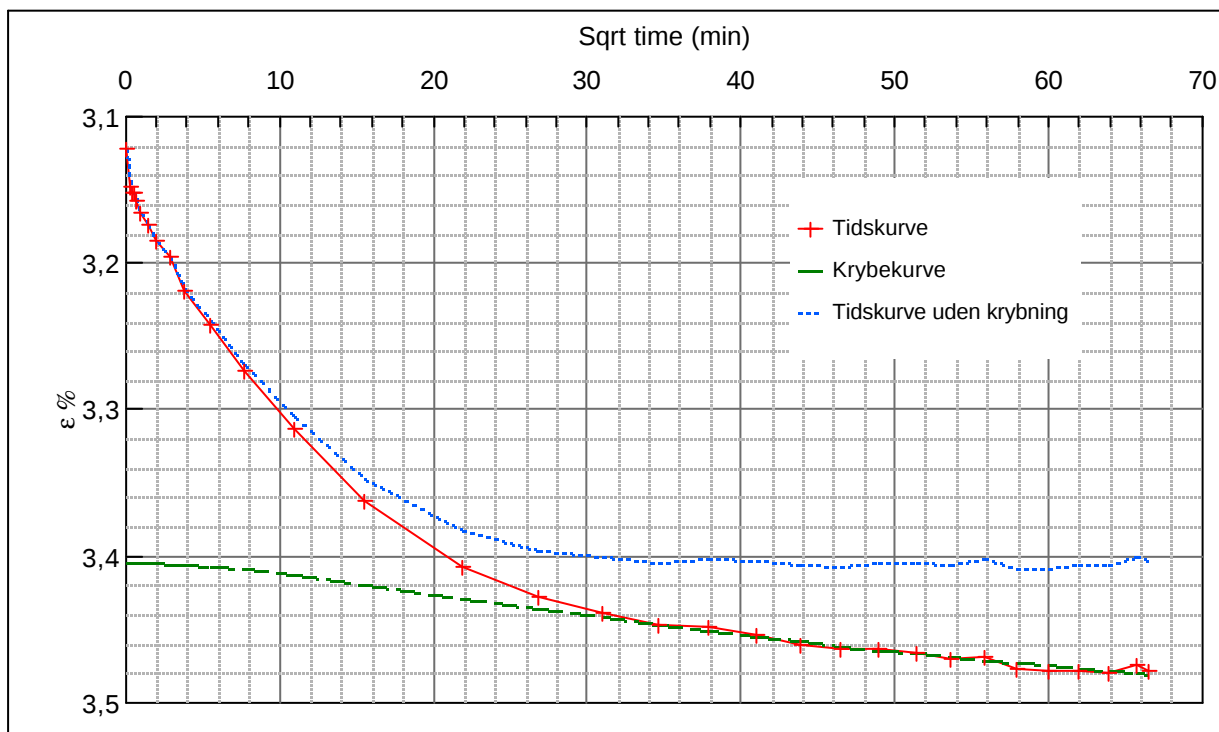
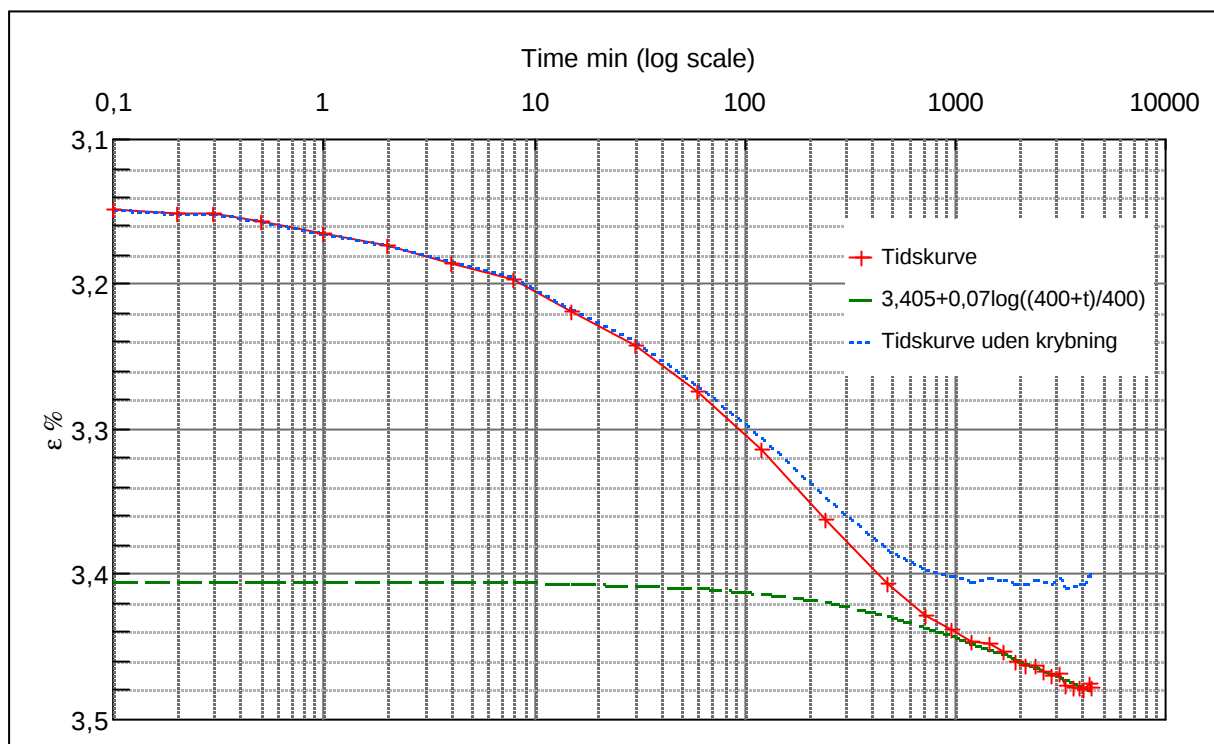
Step no 7	σ	kPa	ϵ	%	ϵ_i		tc in sec	17340
	Before	4.165,9	ϵ_0	2,56	ϵ_c %	3,05	K i kPa	284.197
	After	5.553,8	$\epsilon_{\sim\#}$	3,12	ϵ_s	0,06	k10 m/sec	1,9E-12
					ϵ_{kryb}	0,07	ck10 m ² /sec	5,59E-08



Material: Clay, Lower Jura	
Bor no : A IV	Depth: 304 m.b.s
Lab. no: k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.9
Executed:	AMS/gt	Check:
Approved:		

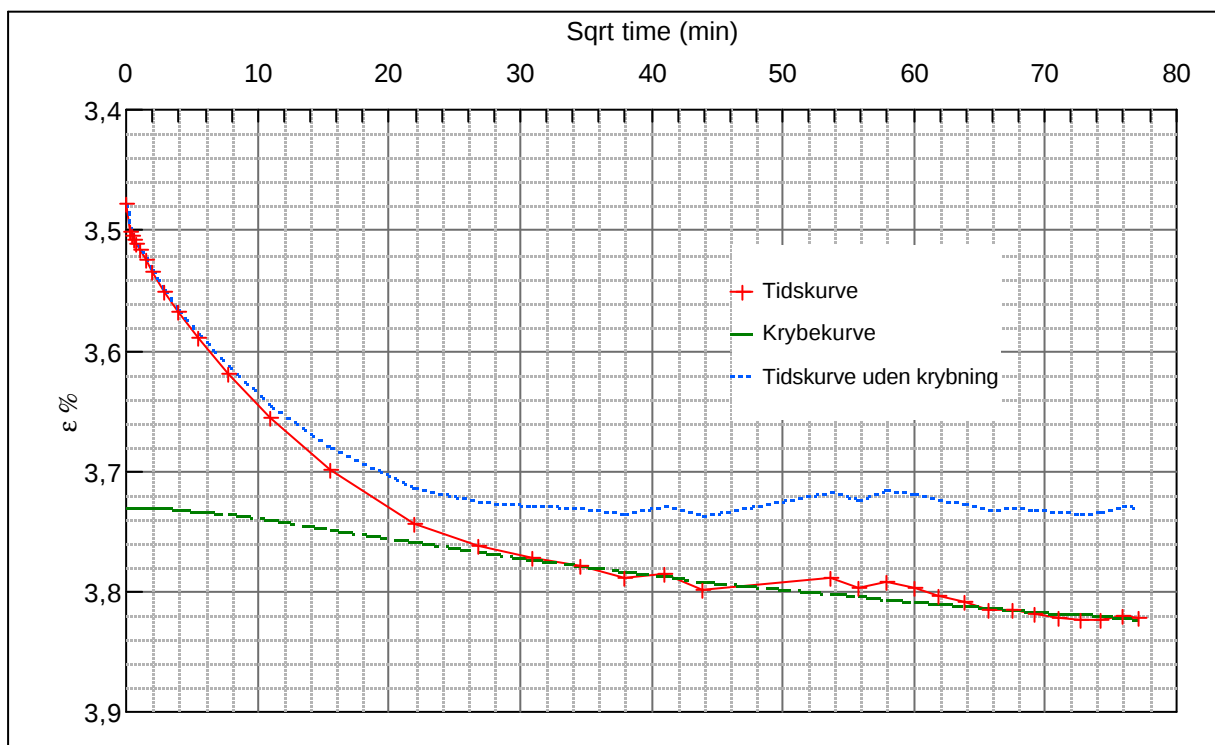
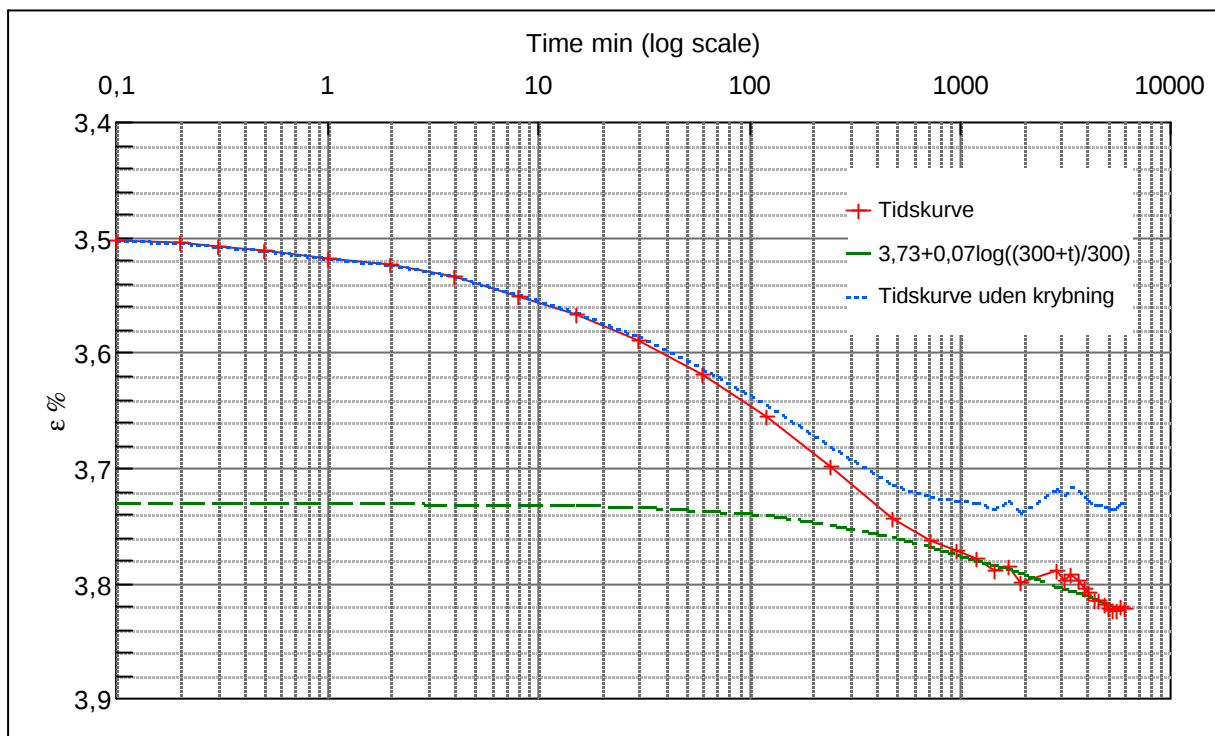
Step no 8	σ	kPa	ϵ	%	ϵ_i	tc in sec	11760
	Before	5.553,8	ϵ_0	3,12	ϵ_c %	K i kPa	367.367
	After	6.594,6	$\epsilon_{-#}$	3,48	ϵ_s	k10 m/sec	2,2E-12
					ϵ_{kryb}	ck10 m ² /sec	8,25E-08



Material: Clay, Lower Jura		
Bor no :	A IV	Depth: 304 m.b.s
Lab. no:	k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.10
Executed:	AMS/gt	Check:
Approved:		

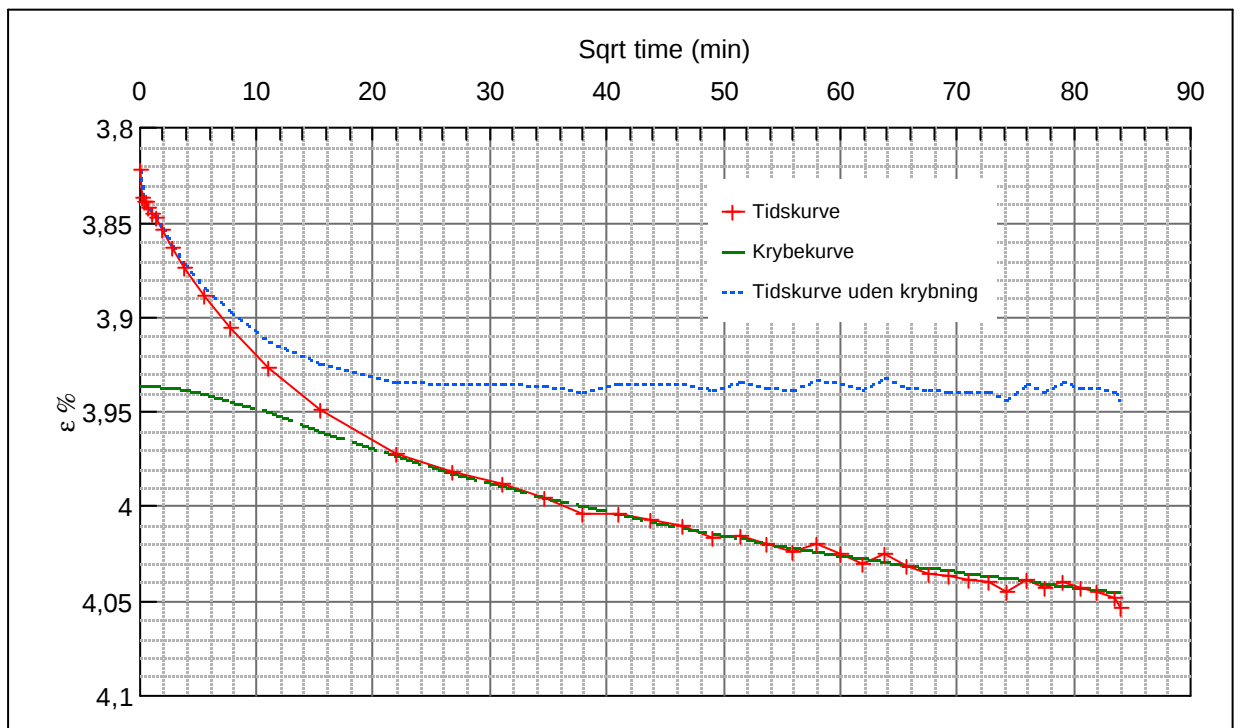
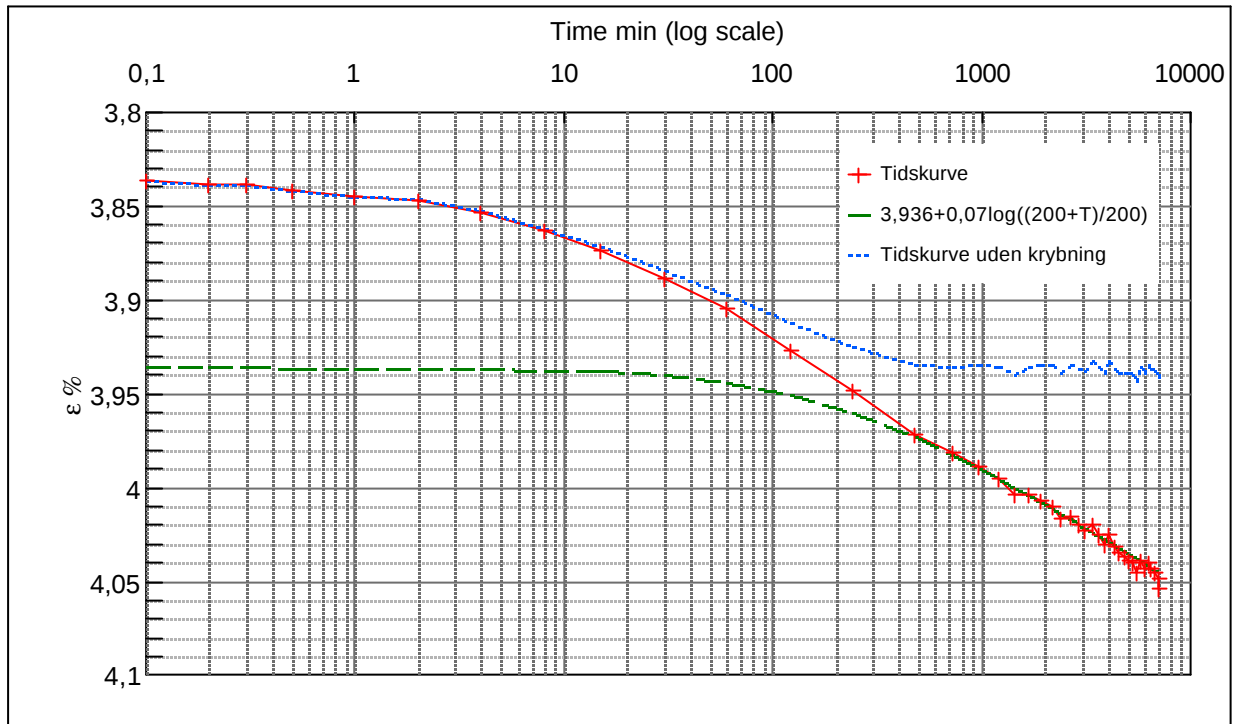
Step no 9	σ	kPa	ε	%	ε_i		tc in sec	13500
	Before	6.594,6	ε_0	3,48	ε_c %	3,73	K i kPa	413.592
	After	7.635,5	$\varepsilon_{\sim\#}$	3,82	ε_s	0,06	k10 m/sec	1,7E-12
					ε_{kryb}	0,09	ck10 m^2/sec	7,18E-08



Material: Clay, Lower Jura	
Bor no : A IV	Depth: 304 m.b.s
Lab. no: k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.11
Executed:	AMS/gt	Check:
Approved:		

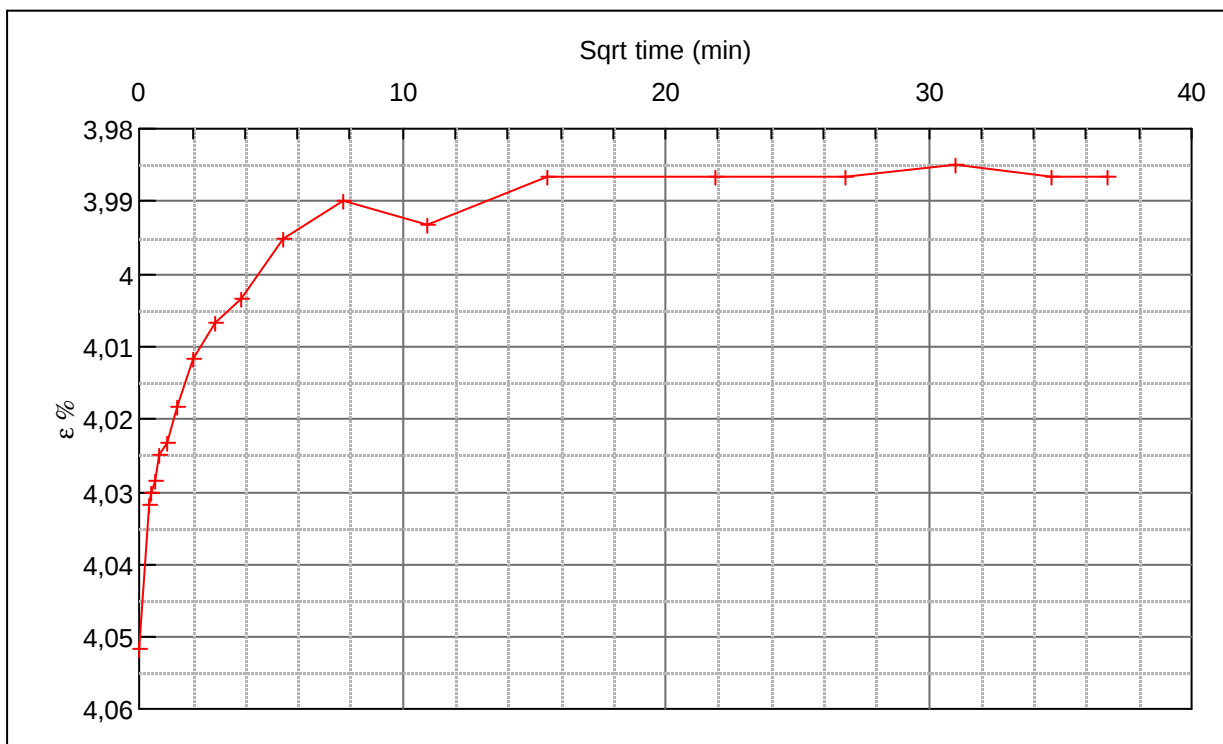
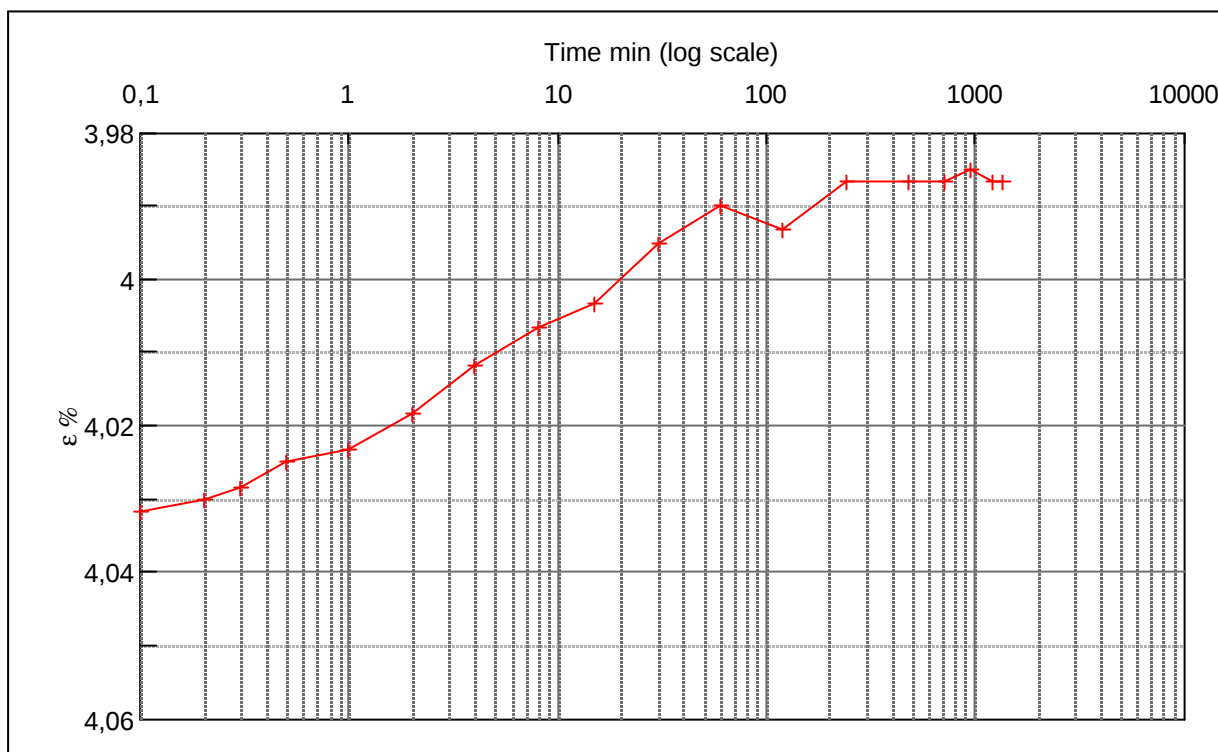
Step no 10	σ	kPa	ϵ	%	ϵ_i		tc in sec	7260
	Before	7.635,5	ϵ_0	3,82	ϵ_c %	3,94	K i kPa	606.923
	After	8.329,4	$\epsilon_{\sim\#}$	4,05	ϵ_s	0,07	k10 m/sec	2,2E-12
					ϵ_{kryb}	0,12	ck10 m ² /sec	1,34E-07



Material:	
Clay, Lower Jura	
Bor no :	A IV
Depth:	304 m.b.s
Lab. no:	k98
Insitu stress ~3040 kPa	

Job:	Anholt	AAU
		Encl. No 6.12
Executed:	AMS/gt	Check:
Approved:		

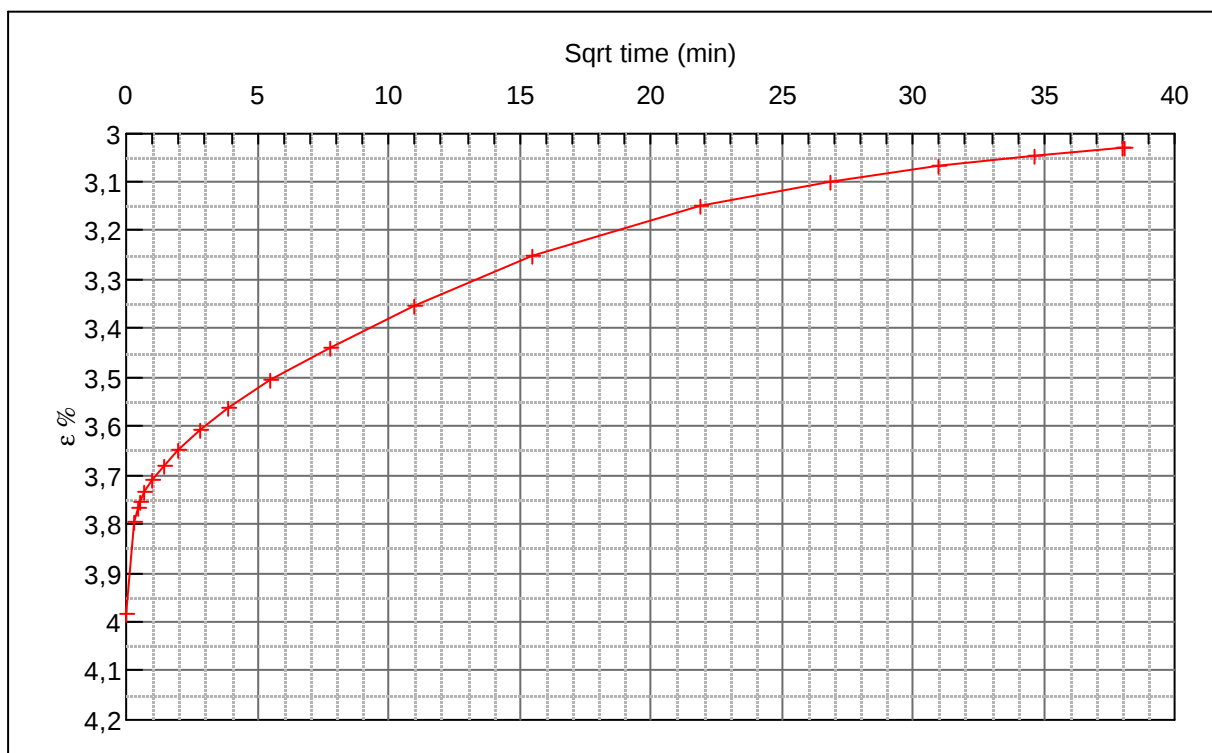
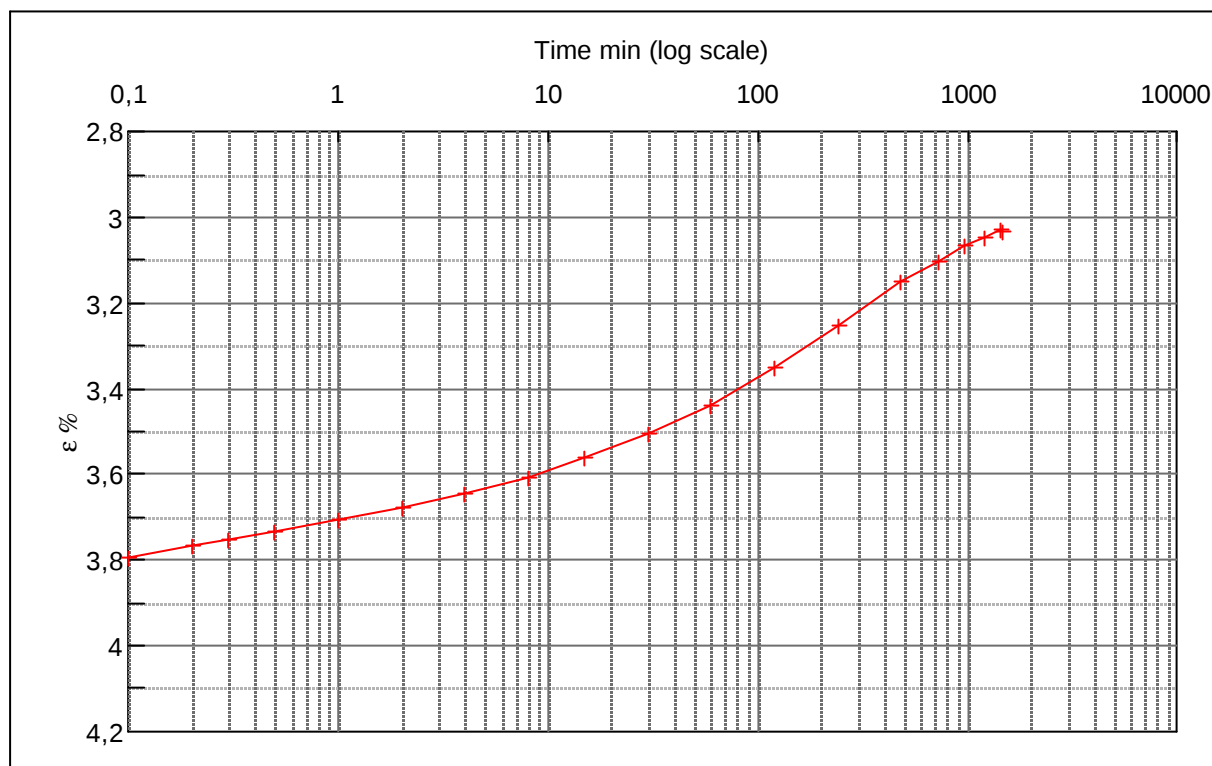
Step no 11	σ	kPa	ϵ	%	ϵ_i	tc in sec 1215 K i kPa 2.682.663 k10 m/sec 2,9E-12 ck10 m ² /sec 7,98E-07
	Before	8.329,4	ϵ_0	4,05	ϵ_c %	
	After	6.594,6	$\epsilon_{\sim\#}$	3,99	ϵ_s	
					ϵ_{kyb}	



Material: Clay, Lower Jura		
Bor no :	A IV	Depth: 304 m.b.s
Lab. no:	k98	Insitu stress: ~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.13
Executed:	AMS/gt	Check:
Approved:		

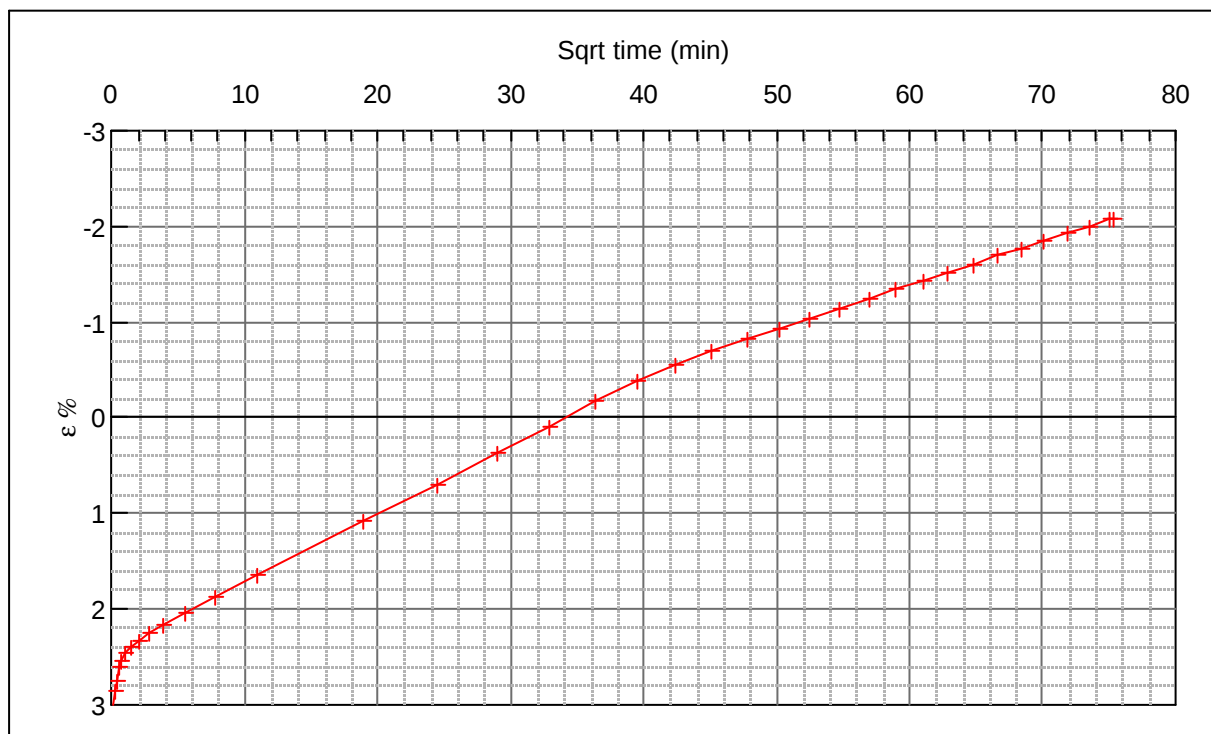
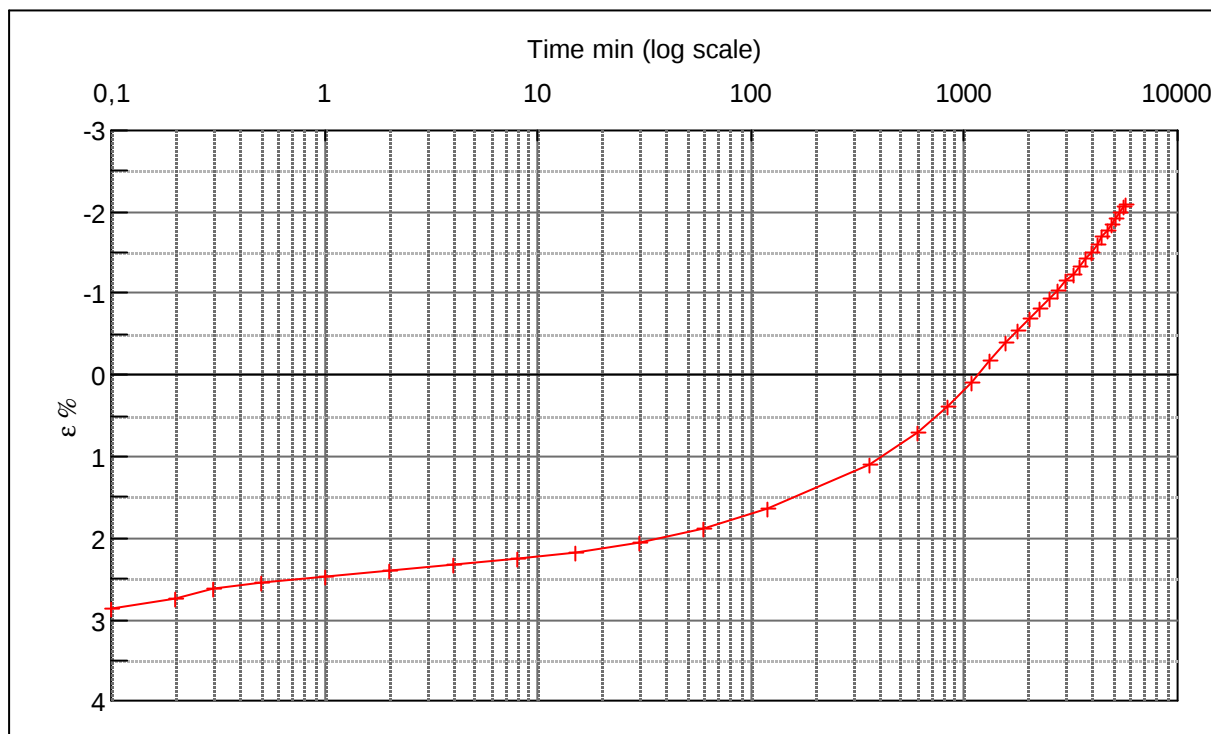
Step no 12	σ	kPa	ϵ	%	ϵ_i		tc in sec	29040
	Before	6.594,6	ϵ_0	3,98	ϵ_c %	3,03	K i kPa	401.178
	After	2.778,1	$\epsilon_{-#}$	3,03	ϵ_s		k10 m/sec	8,2E-13
					ϵ_{kyb}		ck10 m ² /sec	3,34E-08



Material:	
Clay, Lower Jura	
Bor no :	A IV
Lab. no:	k98
Depth:	304 m.b.s
Insitu stress:	~3040 kPa

Job:	Anholt	AAU
		Encl. No 6.14
Executed:	AMS/gt	Check:
Approved:		

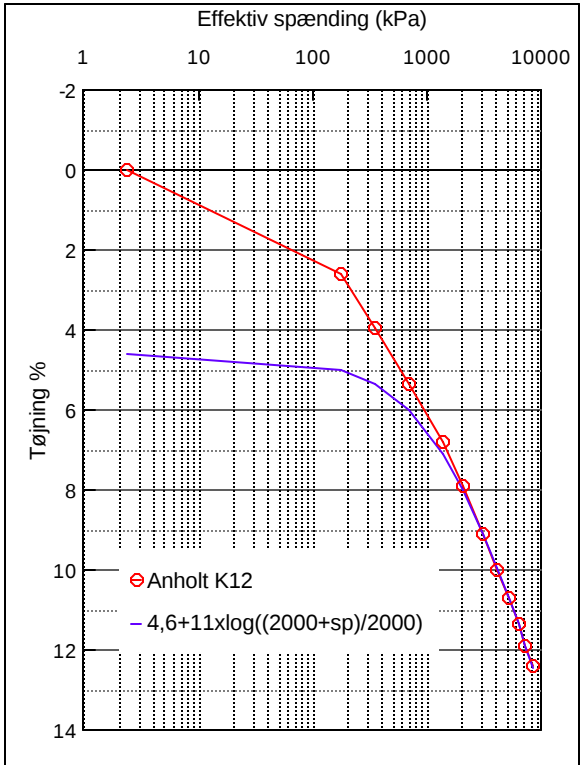
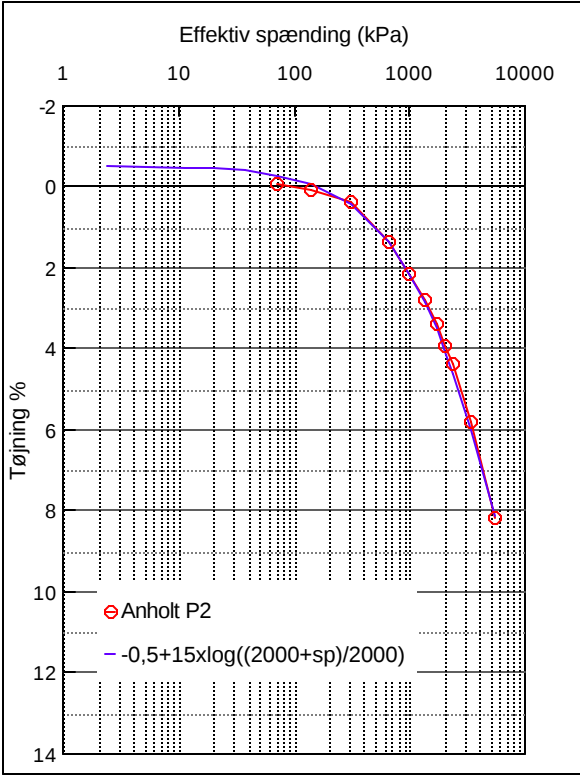
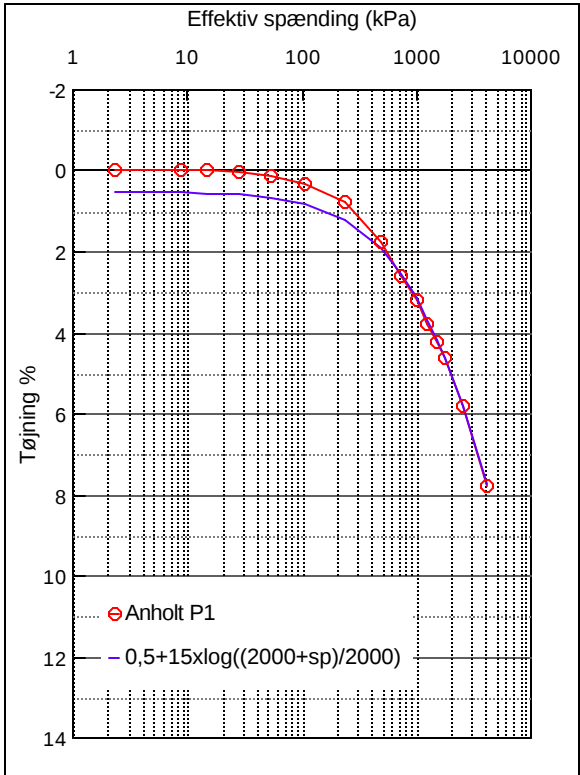
Step no 13	σ	kPa	ϵ	%	ϵ_i	tc in sec	253500
	Before	2.778,1	ϵ_0	3,03	ϵ_c %	K i kPa	54.269
	After	2,43	$\epsilon_{-#}$	(2,08)	ϵ_s	k10 m/sec	6,9E-13
					ϵ_{kryb}	ck10 m ² /sec	3,83E-09



Material: Clay, Lower Jura	
Bor no : A IV	Depth: 304 m.b.s
Lab. no: k98	Insitu stress: ~3040 kPa

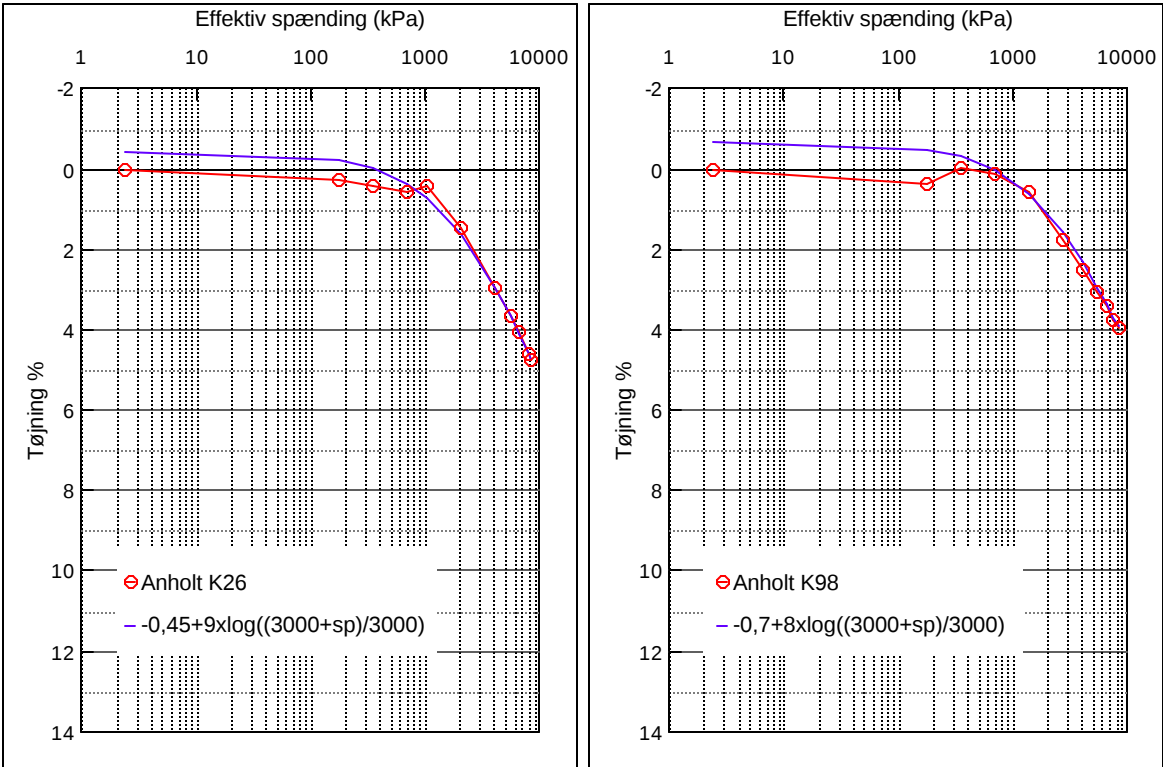
Job:	Anholt	AAU
		Encl. No 6.15
Executed:	AMS/gt	Check:
Approved:		

Eem. Arbejdskurver fra konsolideringsforsøg med tilpassede Terzaghi-kurver



Job: ANHOLT	AAU
	Encl. No 7.1
Executed: gt	Check:
Approved:	

Jura. Arbejdskurver fra konsolideringsforsøg med tilpassede Terzaghi-kurver



Job: ANHOLT	AAU
	Encl. No 7.2
Executed: gt	Check:
Approved:	