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Title:

Musculoskeletal model-based inverse dynamic analysis under ambulatory conditions using inertial motion capture

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Abstract

1

Inverse dynamic analysis using musculoskeletal modeling is a powerful tool, 2 which is utilized in a range of applications to estimate forces in ligaments, muscles, and joints, non-invasively. To date, the conventional input used in this analysis is derived from optical motion capture (OMC) and force plate (FP) systems, which restrict the application of musculoskeletal models to gait labo-6 ratories. To address this problem, we propose the use of inertial motion capture to perform musculoskeletal model-based inverse dynamics by utilizing a universally applicable ground reaction force and moment (GRF&M) prediction q method. Validation against a conventional laboratory-based method showed 10 excellent Pearson correlations for sagittal plane joint angles of ankle, knee, and 11 hip ($\rho = 0.95, 0.99$, and 0.99, respectively) and root-mean-squared-differences 12 (RMSD) of $4.1 \pm 1.3^{\circ}$, $4.4 \pm 2.0^{\circ}$, and $5.7 \pm 2.1^{\circ}$, respectively. The GRF&M pre-13 dicted using IMC input were found to have excellent correlations for three com-14 ponents (vertical: $\rho = 0.97$, RMSD= 9.3 ± 3.0 %BW, anteroposterior: $\rho = 0.91$, 15 RMSD= 5.5 ± 1.2 %BW, sagittal: $\rho = 0.91$, RMSD= 1.6 ± 0.6 %BW*BH), and 16 strong correlations for mediolateral (ρ = 0.80, RMSD=2.1 \pm 0.6 %BW) and 17 transverse ($\rho = 0.82$, RMSD= 0.2 ± 0.1 %BW*BH). The proposed IMC-based 18 method removes the complexity and space-restrictions of OMC and FP systems 19 and could enable applications of musculoskeletal models in either monitoring 20 patients during their daily lives or in wider clinical practice. 21

22 1. Introduction

Assessment of muscle, joint, and ligament forces is important to understand the mechanical and physiological mechanisms of human movement. To date, the measurement of such in-vivo forces is a challenging task. For this reason, computer-based musculoskeletal models have been widely used to estimate the variables of interest non-invasively [1, 2].

The most common approach used in musculoskeletal modeling is the method 28 of the inverse dynamics [3]. This analysis utilizes the equations of motion with 29 input from human body kinematics in conjunction with kinetics obtained from 30 external forces [4], to estimate joint reaction and muscle forces, as well as net 31 joint moments using muscle recruitment methods [5]. Measurements of the 32 external forces are typically required and measured using force plates (FPs). 33 however, the use of FPs has several limitations. First, subjects tend to alter 34 their natural gait patterns in order to hit the small and fixed measurement area 35 of a plate [6]. In addition, this static and limited measurement area, impedes 36 the assessment of several consecutive steps, when only a couple of FPs are 37 available. Finally, the combined use of FP with motion input introduces a 38 dynamic inconsistency, which results to residual forces and moments in the 39 inverse dynamics. [7, 8]. 40

Several studies have proposed replacing the FP input with wearable de-41 vices such as shoes with three-dimensional force and torque sensors beneath 42 the sole [9, 10, 11]. In a similar fashion, pressure insoles were proposed to re-43 construct the complete ground reaction forces and moments (GRF&M) from 44 pressure distributions [12, 13, 14]. Although these wearable devices are suitable 45 for the assessment of external forces, the increased height and weight of the 46 shoes equipped with force/torque sensors [15, 16], as well as the repeatability 47 of the pressure sensors [17] are considered important limitations. 48

Recent research has suggested the replacement of the force input with predictions derived solely from motion input [18, 19, 20, 21, 22, 23]. In these studies,
human body kinematics are combined with the inertial properties of the body

segments, from which Newton-Euler equations are utilized to compute the exter-52 nal forces and moments. Since the system of equations becomes indeterminate 53 during the double stance of gait, each of the aforementioned studies focused on 54 methods to solve this issue. Ren et al. [19] suggested a gait event-based func-55 tion which is only applicable in gait, while Oh et al. [20] and Choi et al. [21] 56 suggested methods based on a machine learning that require a training database 57 and thus are not applicable for movements not included in that database. 58 last approach enables the universal application of these methods using a muscle 59 recruitment approach has shown promising performance for various activities of 60 daily living [22] and sports [23]. 61

The majority of the existing research which studied the prediction of GRF&M. 62 used conventional optical motion capture (OMC) input. Despite the high ac-63 curacy of this method in tracking marker trajectories, its dependence on lab-64 oratory equipment restricts possible applications during daily life activities or 65 in wider clinical practice. In the previous decade, ambulatory motion tracking 66 systems based on inertial measurement units (IMUs), have been proposed as a 67 suitable alternative for estimating 3D segment kinematics [24, 25, 26, 27]. A 68 key benefit of such systems is that they can be applied in virtually any environ-69 ment without depending on external infrastructure, such as cameras. Driven 70 by these advances in inertial motion capture (IMC), recent work of the authors 71 demonstrated its ability to estimate three-dimensional GRF&M [28], which were 72 distributed between the feet using a smooth transition assumption concept [19]. 73 However, limitations of that approach is that it is only valid for gait and has no 74 muscle, bone or ligament force estimate capabilities. 75

To date, the use of detailed musculoskeletal modeling with kinematic inputs from IMUs has only received limited attention. Koning *et al.* [29] previously demonstrated the feasibility of kinematically driving a musculoskeletal model using only orientations from IMUs. However, that study only compared the kinematics of the musculoskeletal model, without any inverse dynamic calculations.

The aim of this study was to develop a workflow to perform musculoskeletal

 $_{\tt 83}$ model-based inverse dynamics using exclusively IMC input, applicable in am-

⁸⁴ bulatory environments and validate it against a conventional laboratory-based
 ⁸⁵ approach.

86 2. Methods

87 2.1. Subjects

The experimental data was collected at the Human Performance Labora-88 tory, at the Department of Health Science and Technology, Aalborg University, 89 Aalborg, Denmark following the ethical guidelines of The Scientific Ethical Com-90 mittee for the Region of North Jutland (Den Videnskabsetiske Komit for Region 91 Nordjylland). Eleven healthy male individuals with no present musculoskeletal 92 or neuromuscular disorders volunteered for the study (age: 31.0 ± 7.2 years; 93 height: 1.81 ± 0.06 m; weight: 77.3 ± 9.2 kg; body mass index (BMI): $23.6 \pm$ 94 2.4 kg/m^2). All participants provided written informed consent, prior to data 95 collection. 96

97 2.2. Instrumentation

Full-body IMC data were collected using the Xsens MVN Link (Xsens Tech-98 nologies B.V., Enschede, the Netherlands), in which 17 IMUs were mounted on 99 the head, sternum, pelvis, upper legs, lower legs, feet, shoulders, upper arms, 100 forearms and hands using the dedicated clothing. The exact location of each 101 sensor on the respective segment followed the manufacturer guidelines described 102 in the manual of Xsens MVN [30]. The affiliated software Xsens MVN Studio 103 4.2.4 was used to track the IMU orientations with respect to an earth-based 104 coordinate frame [24, 25]. Segment orientations were obtained by applying the 105 IMU-to-segment alignment, found using a known upright pose (N-pose) per-106 formed by the subject at a known moment in time, while taking specific care 107 to minimize the effect of magnetic disturbances. In addition, this information 108 is fused with updates regarding the joints and external contacts to limit the 109 position drift [26]. 110

For validation purposes, an OMC system utilizing 8 infrared high speed 111 cameras (Oqus 300 series, Qualisys AB, Gothenburg, Sweden) and the software 112 Qualisys Track Manager 2.12 (QTM) were used to track the trajectories of 53 113 reflective markers mounted on the human body, as described in the Appendix of 114 [28]. In addition, three FP systems (AMTI OR6-7-1000, Advanced Mechanical 115 Technology, Inc., Watertown, MA, USA) embedded in the floor of the laboratory. 116 were utilized using QTM to record the GRF&Ms. Both IMC and OMC systems 117 sampled data at a frequency of 240 Hz, while the FP system sampled data at 118 2400 Hz and subsequently downsampled to 240 Hz to match the IMC and OMC 119 sampling rate. A second-order forward-backward low-pass Butterworth filter 120 was applied to the reflective marker trajectories and measured GRF&M, with 121 cut-off frequencies of 6 Hz and 15 Hz, respectively. 122

123 2.3. Experimental protocol

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For each participant, the body dimensions were extracted using a conven-124 tional tape following the guidelines of Xsens. During the data collection, the 125 subjects were instructed to walk barefoot in three different walking speeds (com-126 fortable; CW, fast; FW, and slow; SW). The walking speeds performed experi-127 mentally were quantified as 1.28 ± 0.14 m/s (mean \pm standard deviation) for CW, 128 1.58 ± 0.09 m/s for FW (CW + 23%) and 0.86 ± 0.11 m/s for SW (CW-33%). 129 For every walking speed, five successful trials were assessed. A successful trial 130 was obtained when a single foot hit one of the FPs entirely, followed by an entire 131 hit of the other foot on the successive FP. 132

133 2.4. Overall description of the components in the musculoskeletal models

Three musculoskeletal models have been constructed in AnyBodyTM Modeling System (AMS) v.6.0.7 (AnyBodyTM Technology A/S, Aalborg, Denmark) [1]:

• a model in which the kinematics are driven by IMC and the GRF&M are predicted from the kinematics (IMC-PGRF).

• a model in which the kinematics are driven by OMC and the GRF&M are predicted from the kinematics (OMC-PGRF).

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• a model in which the kinematics are driven by OMC and the GRF&M are measured from FPs (OMC-MGRF). 142

In the IMC-PGRF model, a Biovision Hierarchy (BVH) file is exported from 143 Xsens MVN Studio and imported in AMS, in which a stick figure model is ini-144 tially reconstructed. The BVH file contains a hierarchy part with a description 145 of the linked segment model in a static pose, as well as a motion part that 146 contains, for each time frame, the absolute position and orientation of the root 147 pelvis segment, and the joint angles between the segments described in the hier-148 archy. The generated stick figure model contains 72 degrees-of-freedom (DOF). 149 In order to match the stick figure model with the musculoskeletal model, we 150 utilize a concept of virtual markers (VMs) demonstrated in a previous Kinect-151 based study [31]. The VMs are mapped to particular points of each model that 152 are well defined in both models, such as joint centers and segment end points. 153 The VM placement is illustrated in Figure 1 and described in more detail in 154 the supplementary material. Following this step, the VMs are treated as actual 155 experimental markers, as if they were derived from an OMC system and they 156 are assigned weights in three directions in the segmentframe. Contrary to OMC, 157 no filtering was applied to the VM trajectories. 158

In all models, the GaitFullBody template of the $AnyBody^{TM}$ Managed 159 Model Repository (AMMR) 1.6.2 was used to reconstruct the musculoskele-160 tal models in AMS. The lumbar spine model was derived from the study of 161 de Zee et al. [32], the lower limb model was derived from the Twente Lower 162 Extremity Model Klein-Horsman et al. [33], and the shoulder and upper limb 163 models were based on the model of the Delft Shoulder Group [34, 35, 36]. The 164 full-body kinematic model contained 39 DOF in total. Specifically, a pelvis segment with three rotational and three translational DOF, two spherical hip 166 joints, two revolute knee joints, two universal ankle joints, a spherical pelvic-167 lumbar joint, two glenohumeral joints with five DOF each, two universal elbow 168

joints, and two universal wrist joints. The motion of the neck joint was lockedto a neutral position.

171 2.5. Scaling and kinematics analysis of the musculoskeletal models

For each subject, a standing reference trial with an anatomical pose was 172 utilized to identify the parameters of segment lengths and the (virtual) marker 173 positions, using a least-square minimization between the model and input (vir-174 tual or skin-mounted) marker positions [37]. In the IMC-PGRF musculoskeletal 175 model, the lengths of the shanks, thighs, head, upper arm and forearms were 176 derived directly from the stick figure, as generated from Xsens MVN studio us-177 ing the measured body dimensions. In contrast, the pelvis width, foot length, 178 and trunk height were optimized based on the above-mentioned least-square 179 minimization method. The estimated segment lengths were used in all subse-180 quent dynamic trials to perform the kinematic analysis based on the method of 181 Andersen et al. [38]. 182

¹⁸³ 2.6. Inertial and geometric scaling of the musculoskeletal models

The mass of each segment was linearly scaled based on the total body mass and the segment mass ratio values reported by Winter [4]. The inertial parameters were calculated by considering the segments as cylinders with uniform density. In addition, geometric scaling of each segment, where the longitudinal axis was defined as the second entry, was achieved using the following matrix:

$$S = \begin{bmatrix} \sqrt{\frac{m_s}{l_s}} & 0 & 0\\ 0 & l_s & 0\\ 0 & 0 & \sqrt{\frac{m_s}{l_s}} \end{bmatrix}$$
(1)

where S is the scaling matrix, l_s is the ratio between the unscaled and scaled lengths of the segment, m_s is the mass ratio of the segment.

191 2.7. Muscle recruitment

The muscle recruitment problem was solved by defining an optimization problem where a system of equations minimizes the cost function, subject to the dynamic equilibrium equations and non-negativity constraints, so that each muscle can only pull, but not push, while its force remains below its strength [1, 31, 39].

The strengths of the muscles were derived from previous studies which de-197 scribed the models of the body parts, and were considered constant for different 198 lengths and contraction velocities [32, 33, 34, 35, 36]. To scale the muscle 199 strengths, fat percentage was used as in Veeger et al. [35], calculated from the 200 body mass index [40]. The model of the lower body contained 110 muscles, 201 distributed into 318 individual muscle paths. In contrast, in the upper body 202 model, ideal joint torque generators were utilized. Actuators for residual forces 203 and moments with capacity up to 10 N and Nm, respectively, were placed at the 204 origin of the pelvis and included in the muscle recruitment problem previously 205 described. 206

207 2.8. Ground reaction force and moment prediction

The GRF&M were predicted by adjusting a method of Skals *et al.* [23]. A set of eighteen dynamic contact points were overlaid 1 mm beneath the inferior surface of each foot. Each dynamic contact point consisted of five unilateral force actuators, which could generate a positive vertical force perpendicular to the ground, and static friction forces in the anterior, posterior, medial, and lateral directions using a friction coefficient of 0.5. In addition, the height and velocity activation thresholds were set to 0.03 m and 1.2 m/s, respectively.

2.9. Data Analysis

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Lower limb joint angles calculated in the IMC-PGRF model were compared
 to the OMC-PGRF/OMC-MGRF. In addition, GRF&M and JRF&M of the
 IMC-PGRF and OMC-PGRF were compared to OMC-MGRF.

Forces were normalized to body weight (BW) and moments to body weight 219 times body height (BW*BH). The time axis of the curves was normalized to 220 100% of the gait cycle for the kinematics (time between two consecutive heel-221 strike events of the analyzed limb) and 100% of the stance phase (time between 222 heel-strike and toe-off events of the analyzed limb) for the kinetics. Measured 223 and estimated GRF&M were expressed on the right handed coordinate frame 224 defined by the walking direction within the trial (given that the subjects walked 225 straight) and the vertical axis equal to the vertical axis of the respective mo-226 tion capture system used. On the other hand, JRF&M were expressed on the 227 coordinate frame of the segment distal to the body in both IMC and OMC 228 methods. 229

The above-mentioned comparisons of kinematic and kinetic variables to their 230 respective references were performed using absolute and relative root-mean-231 square-differences (RMSD and rRMSD, respectively) as described by Ren et al. 232 [19]. In addition, for every curve, the magnitude (M) and phase (P) differ-233 ence metrics [41] have been utilized. Pearson correlation coefficient (ρ) were 234 calculated, averaged using Fisher's z transformation method [42], and cate-235 gorized similarly to Taylor *et al.* [43], as "weak" ($\rho \leq 0.35$), "moderate" 236 $(0.35 < \rho \le 0.67)$, "strong" $(0.67 < \rho \le 0.90)$, and "excellent" $(\rho > 0.90)$. 237

238 3. Results

239 3.1. Estimated kinematics of the musculoskeletal model

Table 1 presents the results for the accuracy analysis for the joint angles of the IMC-driven model versus the OMC-driven model. Similarly, Figure 2 illustrates the curves for the joint angles of the lower extremities averaged across all gait cycles performed by the eleven subjects. Excellent Pearson correlation coefficients have been found in all sagittal plane angles for ankle, knee, and hip (0.95, 0.99, and 0.99, respectively). For the same variables, the RMSDs across a gait cycle were found as $4.1 \pm 1.3^{\circ}$, $4.4 \pm 2.0^{\circ}$ and $5.7 \pm 2.1^{\circ}$, respectively (mean \pm standard deviation). Hip flexion angles were overall underestimated (M =

 $-4.0\pm13.9\%$), whereas knee and ankle magnitude differences showed an average 248 overestimation $(0.7\pm6.2\%)$ and $8.6\pm16.4\%$). The hip abduction showed excellent 249 correlations ($\rho = 0.91$) with an RMSD of $4.1 \pm 2.0^{\circ}$ and a mean underestimation 250 with a magnitude difference $M = -12.2 \pm 34.7\%$. Strong correlation values ($\rho =$ 251 0.68) were observed in the hip internal-external rotation angle with an RMSD 252 of $6.5 \pm 2.8^{\circ}$ and an underestimation of magnitude difference $M = 5.5 \pm 39.0\%$. 253 Finally, the subtalar eversion angle showed strong correlation ($\rho = 0.82$), RMSD 254 of $9.66 \pm 3.07^{\circ}$ and $M = 24.0 \pm 34.7\%$. 255

256 3.2. Predicted kinetics using inertial and optical motion capture

The results of the accuracy analysis for GRF&M and JRF&M are presented in Table 2 and 3, for IMC-PGRF and OMC-PGRF, respectively. The mean values and standard deviations of the curves from IMC-PGRF, OMC-PGRF, and OMC-MGRF models, are illustrated in Figures 3 and 4, for the forces and moments, respectively.

The Pearson correlation coefficients of the IMC-PGRF model were excellent 262 for vertical ($\rho = 0.97$) and anteroposterior GRF&M ($\rho = 0.91$) and strong for 263 mediolateral GRF&M ($\rho = 0.80$). For the same components, RMSD values 264 observed were of 9.3 ± 3.0 , 5.5 ± 1.2 and 2.1 ± 0.6 %BW, respectively (mean 265 \pm standard deviation). The OMC-PGRF model performed better in the an-266 teroposterior GRF&M components ($\rho = 0.96$, RMSD = 3.7 ± 1.1 %BW), and 267 similarly to IMC-PGRF for the other two GRF&M components (mediolateral: 268 $\rho = 0.79$, RMSD = 1.9 ± 0.5 BW, vertical: $\rho = 0.99$, RMSD = 5.9 ± 1.9 BW). 269

Concerning GRM, the sagittal plane was predicted with similar excellent 270 correlations in both IMC-PGRF ($\rho = 0.91$) and OMC-PGRF ($\rho = 0.94$) driven 271 models. The correlation coefficients for frontal and transverse GRM components 272 found in the IMC-PGRF model were $\rho = 0.64$, $\rho = 0.82$, respectively, whereas 273 in the OMC-PGRF model ($\rho = 0.66, \rho = 0.81$, respectively). The RMSDs 274 found in the IMC-PGRF approach were 0.9 ± 0.6 , 1.6 ± 0.6 , and 0.2 ± 0.001 275 %BW*BH for frontal, sagittal and transverse GR&M, respectively, which were 276 either slightly higher or similar to the RMSDs of the OMC-PGRF approach 277

 $_{278}$ (0.7 ± 0.2, 1.2 ± 0.4, and 0.2 ± 0.1 %BW*BH, respectively).

279 4. Discussion

We have presented a method to perform musculoskeletal model-based in-280 verse dynamics using exclusively IMC input (IMC-PGRF). First, we compared 281 the kinematic joint angle estimates of the lower limbs against those assessed 282 through a conventional, laboratory-based OMC input. In addition, we tested 283 the performance of the approach in calculating the JRF&M, while predicting 284 the GRF&M from the kinematics, against a similarly constructed model (OMC-285 MGRF) which uses input from both FP and OMC. Finally, we performed a sim-286 ilar comparison to evaluate the predicted kinetics of a model driven exclusively 287 by OMC input (OMC-PGRF). 288

Regarding the IMC-based joint angles in the musculoskeletal model, all three 289 sagittal plane angles provided excellent correlations (range: 0.95-0.99) and aver-290 age RMSD values remained below 6°. Slightly lower correlations were observed 291 in the frontal and transverse plane angles, which can be explained due to the 292 smaller range of motion within these planes. For instance, even though the 293 hip abduction and external rotation joint angles present absolute RMSD values 294 similar to the flexion component, their rRMSDs which take into account the 295 range of motion are two and three times higher, respectively. 296

Both GRF&M and JRF&M of the vertical axis presented higher correlations 297 and lower RMSDs than the ones in the anteroposterior and mediolateral axes. 298 Similarly, sagittal plane moments were found in most cases to be more accurate 299 than frontal and transverse plane moments. By visual inspection of the curves, 300 we observe that the magnitude of the IMC-PGRF anteroposterior GRF&M 301 seems to be underestimated both in the negative early stance and positive late 302 stance peak, which can be confirmed by the magnitude difference for that curve 303 (M = -28.3%). However, this behaviour is not observed in the OMC-PGRF, 304 nor during the single stance of the IMC-PGRF curve. Despite the higher rRMSD 305 found in the non-sagittal joint angles, the performance of the IMC-PGRF in 306

the mediolateral, frontal and transverse plane GRF&M components matched closely the OMC-PGRF approach. This observation reveals that OMC-based kinematics suffer from errors of similar size, when capturing the typically small movements of the frontal and transverse planes, given the fact that both IMC-PGRF and OMC-PGRF had the same model characteristics. Therefore, OMC-MGRF should also be used with caution, when comparing either kinematic or JRF&M quantities of the non-sagittal planes.

A number of error sources contribute to discrepancies in the OMC kinemat-314 ics. First, soft tissue artefacts can create a relative movement of the marker 315 with respect to the bone [44, 45]. In addition, mismatches between the experi-316 mental and modelled marker positions can lead to errors in segment orientations 317 calculated during inverse kinematics. Both error sources would have a relatively 318 larger impact on the kinematics of the frontal and transverse plane, than on the 319 sagittal plane. Finally, the JRF&M of the OMC-PGRF were compared against 320 a non-independent OMC-MGRF reference, which could have contributed to un-321 derestimation of the actual errors. 322

The IMC-PGRF approach has a number of possible sources of errors which 323 would influence the performance. Similarly to OMC models, soft-tissue ar-324 tifacts may compromise the kinematic estimates. Further errors in segment 325 kinematics may stem due to the N-pose calibration assumptions. In particular, 326 mismatches between the practised and modelled N-pose could result in offsets 327 in the estimated positions. Other common error sources in IMC include manual 328 measurements of segment lengths as well as IMU inaccuracies. In addition, the 329 stick figure model, which was utilized to recreate the VMs, has a higher number 330 of DOF, compared to the musculoskeletal model used. 331

A possible source of error in all inverse dynamic approaches concerns the inertial parameters (masses and moments of inertia), as well as the center of mass (CoM) locations of each human body segment, which were calculated based on anthropometric tables found in the literature.

This study focused on presenting and evaluating a general workflow for musculoskeletal model-based inverse dynamic simulations using ambulatory IMC

systems. The presentation of results in this study was performed on the level of 338 ground and joint reaction forces and moments. These measures are calculated 339 from muscle force estimates derived from a muscle recruitment optimization 340 technique. Given the high number of muscles in the model (110) and without 341 a clear medical research question, it is challenging to choose which muscles are 342 more important to present and analyze. Future studies could examine specific 343 applications and pathologies in order to identify the most important muscles 344 and evaluate their respective force estimates. 345

A limitation of this study is that, even though the method has been pre-346 viously shown to be universally applicable in OMC-based studies [22, 23], we 347 only evaluated its performance in gait of three different speeds. In addition, 348 our experiments included only young healthy male subjects, but the underlying 349 methods to predict kinetics from kinematics have been recently shown to be 350 applicable in Parkinson's patients [46]. Future studies could investigate the ap-351 plication of IMC systems combined with musculoskeletal modeling in groups of 352 larger sample size than the current study, including patients, as well as female 353 subjects. 354

355 5. Conclusion

In this study, we have demonstrated a workflow to perform musculoskeletal model-based inverse dynamics using input from a commercially available IMC system. Our validation findings indicate that the prediction of GRF&M as well as JRF&M using musculoskeletal model-based inverse dynamics based on only IMC data provides comparable performance to both OMC-PGRF and OMC-MGRF methods. The proposed method allows assessment of kinetic variables outside the laboratory.

363 Ethical approval

The ethical guidelines of The Scientific Ethical Committee for the Region of North Jutland (Den Videnskabsetiske Komit for Region Nordjylland) were fol³⁶⁶ lowed and all volunteers signed written informed consent after receiving detailed

³⁶⁷ information prior to data collection.

368 Conflict of interest statement

Three of the authors are employees of Xsens Technologies B.V. that manu-

 $_{\rm 370}$ $\,$ factures and sells the Xsens MVN. One of the authors is employee of AnyBody

³⁷¹ Technology A/S that owns and sells the AnyBody Modeling System.

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47	1	Illustration of the pipeline used in the IMC-PGRF approach. A
48		recording from Xsens MVN Studio (a) is exported to a BVH
49		file to generate a stick figure model (b), in which virtual markers
50		(blue) are placed. Virtual markers (red) are also placed on points
51		of the musculoskeletal model (c), and by projecting b on c the
52		kinematics of the musculoskeletal model are solved. Finally, in-
53		verse dynamic analysis using prediction of ground reaction forces
54		and moments is performed to estimate the kinetics
55	2	Ankle, knee, and hip joint angle estimates (standard deviation
56		around mean) of the IMC-PGRF (orange shaded area around
57		orange dotted line) and OMC-PGRF models (blue shaded area
58		around blue dashed line) versus OMC-MGRF model (thin black
59		solid lines around thick black solid line)
60	3	Ground and lower limb joint reaction force estimates (standard
61		deviation around mean) of the IMC-PGRF (orange shaded area
62		around orange dotted line) and OMC-PGRF models (blue shaded
63		area around blue dashed line) versus OMC-MGRF model (thin
64		black solid lines around thick black solid line)
65	4	Ground reaction and lower limb net joint moment estimates (stan-
66		dard deviation around mean) of the IMC-PGRF (orange shaded
67		area around orange dotted line) and OMC-PGRF models (blue
68		shaded area around blue dashed line) versus OMC-MGRF model
69		(thin black solid lines around thick black solid line)

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Figure 2







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1 Comparison of lower limb joint angles between musculoskele-571 tal model driven by the inertial (IMC-PGRF) and optical mo-572 tion capture (OMC-PGRF/OMC-MGRF), using Pearson corre-573 lation coefficient (ρ) , absolute and relative root-mean-squared-574 differences (RMSD in degrees and rRMSD in %, respectively). 575 M and P denote the % magnitude and phase differences 576 2IMC-PGRF-based ground and joint reaction forces (first three) 577 quantities) and net moments (second three quantities) versus 578 OMC-MGRF. Pearson correlation coefficient is denoted with ρ . 579 Absolute per body weight (or body weight times height) and 580 relative root-mean-squared-difference are denoted with RMSD 581 (%BW or %BW*BH) and rRMSD (%), respectively. M and P 582 indicate the magnitude and phase differences (%). 30 583 OMC-PGRF-based ground and joint reaction forces (first three 3 584 quantities) and net moments (second three quantities) versus 585 OMC-MGRF. Pearson correlation coefficient is denoted with ρ . 586 Absolute per body weight (or body weight times height) and 587 relative root-mean-squared-difference are denoted with RMSD 588 (%BW or %BW*BH) and rRMSD (%), respectively. M and P 589 indicate the magnitude and phase differences (%). 31590

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	Table 1 ρ RMSD rRMSD	М	P	
Subtalar Eversion Ankle Plantarflexion Knee Flexion Hip Abduction Hip External Rotation Hip Flexion		$\begin{array}{c} 24.0 (34.7) \\ 8.6 (16.4) \\ 0.7 (6.2) \\ -12.2 (34.7) \\ 5.5 (39.0) \\ -4.0 (13.9) \end{array}$	$\begin{array}{c} 19.3 \ (10.2) \\ 9.8 \ (\ 3.9) \\ 4.8 \ (2.7) \\ 21.2 \ (9.3) \\ 12.6 \ (6.2) \\ 8.8 \ (4.2) \end{array}$	
cere in the second seco				

Table 2

	ρ	RMSD	rRMSD	Μ	Р
Ground					
Anteroposterior	0.91	5.5(1.2)	15.0(2.4)	-25.4 (7.3)	14.4(3.2)
Mediolateral	0.80	2.1(0.6)	18.5(3.2)	7.3(19.3)	15.4(3.8)
Vertical	0.97	9.3(3.0)	7.7(2.1)	-1.5 (1.5)	3.4(1.0)
Frontal	0.64	0.9(0.6)	38.0(23.1)	125.5(319.9)	30.6(17.3)
Sagittal	0.91	1.6(0.6)	17.5(6.8)	14.3(18.2)	12.1 (4.5)
Fransverse	0.82	0.2(0.1)	23.3(7.2)	-8.5 (41.9)	17.8(5.3)
nkle					
Anteroposterior	0.84	22.2 (10.3)	26.1(10.2)	49.0 (45.8)	10.8(2.1)
Mediolateral	0.93	24.3(8.9)	15.2(5.3)	14.3(17.1)	7.9(2.7)
Proximodistal	0.93	88.5(30.6)	13.6(4.6)	9.8(14.1)	7.2(2.3)
Eversion	0.76	0.6(0.2)	33.3(20.2)	107.7(220.3)	18.9(10.7)
lantar Flexion	0.93	1.6(0.6)	15.1 (6.6)	10.6(18.1)	9.9(3.6)
xial	0.67	0.5(0.2)	30.4(12.2)	46.5(49.1)	27.2(13.5)
Inee					
Interoposterior	0.82	30.6(10.3)	25.8 (9.7)	43.7(53.5)	13.0(4.5)
Iediolateral	0.91	12.0(3.5)	14.1(3.8)	6.6(8.6)	7.0(2.0)
roximodistal	0.90	63.1 (26.9)	14.3(6.6)	5.1(9.1)	7.2(2.8)
bduction	0.81	1.1 (0.4)	18.9(6.8)	-2.7(16.1)	10.7(3.8)
lexion	0.58	1.9(0.5)	29.8(7.6)	17.9(45.0)	32.8(9.6)
xial	0.73	0.3(0.1)	25.4(10.3)	2.3(30.5)	27.9(13.8)
Iip					
nteroposterior	0.71	17.6(7.6)	27.2 (9.6)	6.8(24.4)	27.6 (10.9)
fediolateral	0.73	27.0(12.5)	23.0(7.4)	7.7(14.6)	10.6(4.1)
roximodistal	0.78	102.8(30.6)	21.7(4.5)	20.2(10.0)	9.0(2.5)
bduction	0.83	1.4(0.7)	19.7(5.8)	6.3(16.9)	13.7(7.9)
lexion	0.92	2.2(0.6)	19.4(4.2)	73.2(26.3)	14.8(4.2)
External Rotation	0.50	0.5 (0.2)	31.6(6.6)	-3.9(36.4)	25.6(10.1)

External Rotation 0.50 0.5 (0.2)

Table 3

	ho	RMSD	rRMSD	Μ	Р
Ground					
Anteroposterior	0.96	3.7(1.1)	8.3 (2.0)	7.7 (12.0)	8.8 (1.8)
Mediolateral	0.79	1.9(0.5)	18.6(4.1)	2.4(10.8)	15.2(4.9)
Vertical	0.99	5.9(1.9)	4.9(1.4)	-1.2 (1.1)	2.1(0.7)
Frontal	0.66	0.7(0.2)	30.3 (9.3)	71.0(122.2)	24.5(9.1)
Sagittal	0.94	1.2(0.4)	13.1(3.8)	15.9 (15.3)	9.2(3.2)
Transverse	0.81	0.2(0.1)	20.7(7.5)	7.1(22.9)	17.5 (7.5)
Ankle		- (-)		. (-)	
Antonon octorion	0.02	180 (60)	99.0(6.1)	27.2(29.6)	10.8 (9.2)
Madialataral	0.85	16.9(0.9)	23.0(0.1)	31.3(20.0)	10.0(2.3)
Mediolateral	0.96	10.1 (4.2)	10.7(2.0)	0.8(9.0)	5.8(2.1)
Proximodistal	0.96	02.2(17.0)	9.8(2.7)	(.1 (9.0))	5.2(1.8)
Eversion Diamtan Elemian	0.70	0.0(0.1)	20.0(7.0)	43.5(04.1)	70(26)
Plantar Flexion	0.90	1.0(0.3)	10.1(3.3)	3.9(10.0)	7.0(2.0)
Axial	0.64	0.5(0.1)	27.2 (7.3)	33.3 (36.9)	27.5 (11.5)
Knee					
Anteroposterior	0.93	11.9(4.5)	12.3 (4.3)	-7.3 (8.7)	7.4(2.0)
Mediolateral	0.96	7.2(2.0)	8.8 (2.6)	-4.2(5.6)	4.4(1.0)
Proximodistal	0.95	41.7 (12.0)	9.3(2.6)	-2.7(5.8)	4.9(1.2)
Abduction	0.91	0.8(0.2)	12.6(2.6)	-0.1(10.5)	7.7(1.6)
Flexion	0.86	0.9(0.3)	16.7(4.8)	-1.7 (14.3)	16.9(5.2)
Axial	0.82	0.2(0.1)	-18.5(6.6)	-3.4 (17.7)	20.6(8.0)
Hip					
Anteroposterior	0.89	9.9 (3.6)	16.0(6.7)	-10.4 (10.6)	16.6(7.6)
Mediolateral	0.92	14.7(4.0)	12.7(3.1)	-1.9(6.9)	6.2(1.5)
Provimodistal	0.92	50.0(15.9)	11.5(2.6)	-46(61)	5.5(1.2)
Abduction	0.91	0.8(0.2)	13.3(2.6)	-32(63)	87(24)
Flexion	0.86	1.3(0.4)	16.4(3.4)	-9.3(12.3)	180(41)
External Rotation	0.68	0.3(0.1)	22.5(3.7)	6.5(15.8)	18.8 (4.8)
	0.00		22.0 (0.17)	010 (1010)	

Supplementary material

Title:

Musculoskeletal model-based inverse dynamic analysis under ambulatory conditions using inertial motion capture

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Keywords:

musculoskeletal modeling, inertial motion capture, inverse dynamics, ground reaction forces and moments, gait analysis

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1. Virtual marker placement

Table 1: Description of the placement of virtual markers (VM) on the segments of the Xsens MVN model (stick figure model) and the musculoskeletal model constructed based on the AnyBody Managed Model Repository (AMMR).

VM Name	VM Placement on MVN	VM Placement on AMMR	VM Weight
T1C7	jT1C7	T1/C7 Joint	(1,1,1)
SPNE	jT9T8	Inferior to $T1/C7$ Joint	(1,1,1)
CHST	Anterior to jT9T8	Inferior and Anterior to $T1/C7$ Joint	(1,1,1)
SACR	jL5S1	Anterior to Pelvis/Sacrum Joint	(10,0,0)
RHJC	jRightHip	Right Hip Joint	(10,10,10)
RKJC	jRightKnee	Right Knee Joint	(2,2,2)
RKJL	Lateral to jRightKnee	Lateral to Right Knee Joint	(1,0,0)
RAJC	jRightAnkle	Right Ankle Joint	(1,1,1)
RTOE	jRightBallFoot	Right Big Toe Node	(1,1,1)
RTOL	Lateral to jRightBallFoot	Lateral to Right Big Toe Node	(0,1,0)
RSJC	jRightShoulder	Right Glenohumeral Joint	(0,2,2)
REJC	jRightElbow	Elbow Joint	(2,2,2)
RELA	Lateral to jRightElbow	Lateral to Elbow Joint	(1,1,1)
RWJC	jRightWrist	Right Wrist Joint	(2,2,2)
RHT1	Inferior and Medial to jRightWrist	Inferior and Medial to Right Wrist Joint	(0.5, 0.5, 0.5)
RHT2	Inferior and Lateral to jRightWrist	Inferior and Lateral to Right Wrist Joint	(0.5, 0.5, 0.5)
LHJC	jLeftHip	Left Hip Joint	(10,10,10)
LKJC	jLeftKnee	Left Knee Joint	(2,2,2)
LKJL	Lateral to jLeftKnee	Lateral to Left Knee Joint	(1,0,0)
LAJC	jLeftAnkle	Left Ankle Joint	(1,1,1)
LTOE	jLeftBallFoot	Left Big Toe Node	(1,1,1)
LTOL	Lateral to jLeftBallFoot	Lateral to Left Big Toe Node	(0,1,0)
LSJC	jLeftShoulder	Left Glenohumeral Joint	(0,2,2)
LEJC	jLeftElbow	Elbow Joint	(2,2,2)
LELA	Lateral to jLeftElbow	Lateral to Elbow Joint	(1,1,1)
LWJC	jLeftWrist	Left Wrist Joint	(2,2,2)
LHT1	Inferior and Medial to jLeftWrist	Inferior and Medial to Left Wrist Joint	(0.5, 0.5, 0.5)
LHT2	Inferior and Lateral to <i>jLeftWrist</i>	Inferior and Lateral to Left Wrist Joint	(0.5, 0.5, 0.5)
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Figure 1: Illustration of the placement of the virtual markers (VM) on the segments of the Xsens MVN model (stick figure model) and the musculoskeletal model constructed based on the AnyBody Managed Model Repository (AMMR).

2. Accuracy analysis per walking speed

2.1. Comfortable walking speed

Table 2: Comfortable walking speed; comparison of lower limb joint angles between musculoskeletal model driven by the inertial (IMC-PGRF) and optical motion capture (OMC-PGRF/OMC-MGRF), using Pearson correlation coefficient (ρ), absolute and relative root-mean-squared-differences (*RMSD* in degrees and *rRMSD* in %, respectively). *M* and *P* denote the % magnitude and phase differences .

Normal Walking						
	ρ	RMSD	m rRMSD	Μ	Р	
Subtalar Eversion	0.79	9.7(3.1)	32.6 (10.1)	25.5 (36.2)	18.9(9.6)	
Ankle Plantarflexion	0.95	4.0(1.3)	13.1(4.9)	10.3(16.6)	9.3 (3.6)	
Knee Flexion	0.98	4.6(2.0)	7.4(3.1)	2.1(5.5)	4.9 (2.3)	
Hip Abduction	0.91	3.9(1.9)	25.2(9.1)	-15.9(28.8)	20.4(8.0)	
Hip External Rotation	0.66	6.5(2.6)	35.7(14.1)	7.9(36.7)	12.6(5.5)	
Hip Flexion	0.99	5.6(2.2)	12.5 (5.5)	-3.7(13.0)	8.8(4.4)	

Figure 2: Comfortable walking speed; ankle, knee, and hip joint angle estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Table 3: Comfortable walking speed; IMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).

Table 4: Comfortable walking speed; OMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).



Figure 3: Comfortable walking speed; ground and lower limb joint reaction force estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Figure 4: Comfortable walking speed; ground reaction and lower limb net joint moment estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).

2.2. Slow walking speed

Table 5: Slow walking speed; comparison of lower limb joint angles between musculoskeletal model driven by the inertial (IMC-PGRF) and optical motion capture (OMC-PGRF/OMC-MGRF), using Pearson correlation coefficient (ρ), absolute and relative root-mean-squared-differences (*RMSD* in degrees and *rRMSD* in %, respectively). *M* and *P* denote the % magnitude and phase differences .

Slow Walking					
	ho	RMSD	m rRMSD	Μ	Р
	Corr	RMSE	rRMSE	М	Р
Subtalar Eversion	0.81	10.1(3.5)	32.9(9.6)	29.5(36.3)	17.6(10.1)
Ankle Plantarflexion	0.96	3.9(1.2)	13.7(4.0)	5.1(14.0)	9.5(3.4)
Knee Flexion	0.99	4.1(2.4)	7.0(4.3)	-0.3(7.5)	4.7 (3.6)
Hip Abduction	0.91	4.1(2.1)	27.6(12.4)	-3.3(42.8)	23.2(10.9)
Hip External Rotation	0.76	6.7(3.1)	39.5(17.9)	12.9(46.9)	13.0(6.7)
Hip Flexion	0.99	5.2(1.9)	13.3 (5.7)	-3.8(16.4)	8.6(4.2)

Figure 5: Slow walking speed; ankle, knee, and hip joint angle estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Table 6: Slow walking speed; IMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).

Table 7: Slow walking speed; OMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).



Figure 6: Slow walking speed; ground and lower limb joint reaction force estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Figure 7: Slow walking speed; ground reaction and lower limb net joint moment estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).

2.3. Fast walking speed

Table 8: Fast walking speed; comparison of lower limb joint angles between musculoskeletal model driven by the inertial (IMC-PGRF) and optical motion capture (OMC-PGRF/OMC-MGRF), using Pearson correlation coefficient (ρ), absolute and relative root-mean-squared-differences (*RMSD* in degrees and *rRMSD* in %, respectively). *M* and *P* denote the % magnitude and phase differences .

Fast Walking						
	ho	RMSD	m rRMSD	Μ	Р	
Subtalar Eversion	0.83	9.3(2.8)	32.2 (11.4)	16.1(29.9)	21.6 (10.9)	
Ankle Plantarflexion	0.95	4.6(1.3)	15.4(5.1)	10.4(18.3)	10.8(4.7)	
Knee Flexion	0.98	4.6(1.6)	7.3(2.6)	-0.0 (5.0)	4.6 (1.9)	
Hip Abduction	0.9	4.2(2.0)	25.0(10.3)	-17.6(29.6)	20.0 (8.4)	
Hip External Rotation	0.62	6.2(2.6)	35.3(12.8)	-5.4(29.1)	12.0(6.4)	
Hip Flexion	0.99	6.3(1.9)	12.5(4.4)	-4.6(12.0)	9.1 (3.8)	

Figure 8: Fast walking speed; ankle, knee, and hip joint angle estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Table 9: Fast walking speed; IMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).

	ρ	RMSD	rRMSD	М	Р
Ground					
Anteroposterior	0.92	6.5(1.2)	14.1(2.0)	-25.2 (6.6)	13.0(2.7)
Mediolateral	0.75	2.5(0.7)	19.3(3.4)	3.9(15.2)	17.5(3.8)
Vertical	0.95	11.5(3.2)	8.8 (2.2)	-1.7 (1.8)	4.1 (1.1)
Frontal	0.61	0.9(0.5)	34.1(15.5)	91.7(269.9)	30.9(15.0)
Sagittal	0.90	1.7(0.4)	17.1(4.2)	21.6(15.2)	12.7(4.1)
Transverse	0.81	0.2(0.1)	24.4(9.3)	-13.1 (33.0)	18.4(6.8)
Ankle					
Anteroposterior	0.84	22.0 (8.0)	23.4(6.9)	41.8 (34.5)	10.7(1.5)
Mediolateral	0.94	25.0(6.2)	14.9(3.7)	17.7(13.1)	8.0(2.9)
Proximodistal	0.93	93.3(23.8)	13.6(3.2)	13.8(9.3)	7.5(2.5)
Eversion	0.75	0.7(0.2)	30.7(13.7)	81.9 (137.1)	19.8 (9.8)
Plantar Flexion	0.93	1.6(0.4)	14.1(4.2)	14.8 (12.5)	10.1(3.3)
Axial	0.65	0.6~(0.1)	28.3(8.4)	54.9 (33.2)	28.6(12.1)
Knee					
Anteroposterior	0.75	39.4 (8.2)	25.3(7.4)	29.3 (38.3)	15.7 (4.6)
Mediolateral	0.90	145(30)	143(33)	80(89)	73(15)
Proximodistal	0.92	66.8(19.0)	12.8(4.0)	50(70)	67(18)
Abduction	0.92	11(02)	15.5(3.3)	0.0(11.0)	0.7(1.0) 0.8(2.1)
Flovion	0.67	20(0.2)	24.6(5.3)	0.1(10.3) 0.2(18.7)	3.0(2.1)
Axial	0.83	0.3(0.1)	24.0(3.3) 20.6(8.1)	-4.9(25.8)	22.2(0.5) 22.2(11.5)
Hip		. ,			()
Anteroposterior	0.80	19.0 (8.3)	22.5 (6.7)	33 (23 4)	20.7(5.9)
Mediolateral	0.00	31.8(11.6)	22.0(0.1) 21.1(6.8)	10.5(20.4)	10.6(3.7)
Provimodistal	0.11	1220(225)	21.1(0.0) 20.3(4.0)	10.0(10.0) 21.7(11.2)	10.0(0.1)
Abduction	0.82	125.9(52.5) 1.5(0.6)	20.3(4.5) 10.5(4.5)	10.7(11.2)	$\frac{9.2}{144} (2.4)$
Florier	0.00	1.5(0.0)	13.0(4.0)	10.7 (10.0)	14.4(0.9)
Flexion	0.91	2.0(0.0)	10.4(5.1)	35.2(20.0)	14.0(5.6)
External Rotation	0.44	0.5 (0.2)	31.7 (5.6)	-4.5 (30.2)	20.0 (9.9)
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Table 10: Fast walking speed; OMC-PGRF-based ground and joint reaction forces (first three quantities) and net moments (second three quantities) versus OMC-MGRF. Pearson correlation coefficient is denoted with ρ . Absolute per body weight (or body weight times height) and relative root-mean-squared-difference are denoted with RMSD (%BW or %BW*BH) and rRMSD (%), respectively. M and P indicate the magnitude and phase differences (%).

	ρ	RMSD	rRMSD	М	Р
Ground	,				
Anteroposterior	0.96	4.2(0.8)	7.9(1.5)	0.1 (7.4)	9.0 (1.7)
Mediolateral	0.76	2.2(0.5)	19.4(5.3)	1.2(10.6)	16.5(6.0)
Vertical	0.98	7.2(2.3)	5.4(1.6)	-1.0 (0.9)	2.6(0.8)
Frontal	0.59	0.8(0.2)	30.1(8.1)	59.1(92.8)	26.9(9.3)
Sagittal	0.94	1.5(0.3)	14.3(2.9)	28.3(13.3)	9.7(2.8)
ransverse	0.80	0.2(0.1)	21.0(8.5)	1.1 (19.8)	17.9 (8.3)
nkle					
nteroposterior	0.83	21.3 (7.0)	22.9 (5.2)	39.4 (23.6)	11.0 (1.9)
Mediolateral	0.95	19.4(4.2)	11.9(2.3)	12.5(8.6)	6.6(2.2)
Proximodistal	0.96	76.4(15.8)	11.0(2.0)	13.7(6.9)	5.7 (1.7)
version	0.72	0.6(0.1)	26.2(5.6)	47.5 (55.2)	20.3(7.5)
lantar Flexion	0.96	1.3(0.3)	10.9(2.6)	13.8 (8.0)	7.7(2.7)
axial	0.60	0.5 (0.1)	27.0(8.2)	33.3(32.7)	30.6(12.1)
nee					
Interoposterior	0.94	15.2(4.1)	10.8(2.3)	-3.0 (5.8)	7.4 (1.6)
[Iediolateral	0.96	8.2(1.6)	8.5 (1.4)	-0.6(4.7)	4.5(0.8)
roximodistal	0.95	49.6 (9.0)	9.4(1.6)	1.7(4.7)	5.3(0.9)
bduction	0.92	0.9(0.2)	11.8(1.8)	6.1(9.0)	7.6(1.5)
lexion	0.90	1.2(0.3)	14.6(3.4)	-1.1(11.2)	15.2(4.0)
xial	0.89	0.2(0.1)	14.8 (4.7)	-6.5(18.5)	16.1(4.9)
Iip					
Interoposterior	0.91	11.9 (4.0)	15.4(6.4)	-9.1 (13.3)	14.4(5.4)
/lediolateral	0.94	16.6(3.5)	11.7(2.4)	-1.2 (7.9)	5.8(1.2)
roximodistal	0.93	59.5(17.0)	10.8(2.5)	-2.6(7.2)	5.5(1.3)
bduction	0.88	1.0(0.2)	14.3(2.5)	-3.5(7.2)	10.4(2.4)
lexion	0.89	1.6(0.3)	13.8(2.9)	-6.1 (13.0)	15.3(3.8)
External Rotation	0.67	0.4(0.1)	22.2(3.5)	-0.9(12.6)	20.7(5.3)

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Figure 9: Fast walking speed; ground and lower limb joint reaction force estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).



Figure 10: Fast walking speed; ground reaction and lower limb net joint moment estimates (standard deviation around mean) of the IMC-PGRF (orange shaded area around orange dotted line) and OMC-PGRF models (blue shaded area around blue dashed line) versus OMC-MGRF model (thin black solid lines around thick black solid line).