

A power calculation algorithm for single-phase droop-operated-inverters considering linear and nonlinear loads HIL-assessed

Mariachet, Jorge El; Matas, Jose; Martín, Helena; Li, Mingshen; Guan, Yajuan; Guerrero, Josep M.

Published in:
Electronics (Switzerland)

DOI (link to publication from Publisher):
[10.3390/electronics8111366](https://doi.org/10.3390/electronics8111366)

Creative Commons License
CC BY 4.0

Publication date:
2019

Document Version
Publisher's PDF, also known as Version of record

[Link to publication from Aalborg University](#)

Citation for published version (APA):

Mariachet, J. E., Matas, J., Martín, H., Li, M., Guan, Y., & Guerrero, J. M. (2019). A power calculation algorithm for single-phase droop-operated-inverters considering linear and nonlinear loads HIL-assessed. *Electronics (Switzerland)*, 8(11), Article 1366. <https://doi.org/10.3390/electronics8111366>

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal -

Take down policy

If you believe that this document breaches copyright please contact us at vbn@aub.aau.dk providing details, and we will remove access to the work immediately and investigate your claim.

Article

A Power Calculation Algorithm for Single-Phase Droop-Operated-Inverters Considering Linear and Nonlinear Loads HIL-Assessed

Jorge El Mariachet ^{1,*} , Jose Matas ¹ , Helena Martín ¹ , Mingshen Li ², Yajuan Guan ² and Josep M. Guerrero ² 

¹ Electric Engineering Department, Polytechnic University of Catalonia (EETEC-UPC), 08019 Barcelona, Spain; jose.matas@upc.edu (J.M.); m.helena.martin@upc.edu (H.M.)

² Energy Teknik Department, Aalborg University (ET-AAU), 9220 Aalborg, Denmark; msh@et.aau.dk (M.L.); ygu@et.aau.dk (Y.G.); joz@et.aau.dk (J.M.G.)

* Correspondence: jorge.el.mariachet@upc.edu

Received: 30 September 2019; Accepted: 7 November 2019; Published: 18 November 2019



Abstract: The active and reactive powers, P and Q , are crucial variables in the parallel operation of single-phase inverters using the droop method, introducing proportional droops in the inverter output frequency and voltage amplitude references. P and Q , or $P-Q$, are calculated as the product of the inverter output voltage and its orthogonal version with the output current, respectively. However, when sharing nonlinear loads these powers, P_{av} and Q_{av} , should be averaged by low-pass filters (LPFs) with a very low cut-off frequency to avoid the high distortion induced by these loads. This forces the droop method to operate at a very low dynamic velocity and degrades the system stability. Then, different solutions have been proposed in literature to increase the system velocity, but only considering linear loads. Therefore, this work presents a method to calculate P_{av} and Q_{av} using second-order generalized integrators (SOGI) to face this problem with nonlinear loads. A double SOGI (DSOGI) approach is applied to filter the nonlinear load current and provide its fundamental component to the inverter, leading to a faster dynamic velocity of the droop-based load sharing capability and improving the stability. The proposed method is shown to be faster than others in the literature when considering nonlinear loads, while smoothly driving the system with low distortion levels. Simulations, hardware-in-loop (HIL) and experimental results are provided to validate this proposal.

Keywords: droop method; active and reactive power calculation; single-phase parallelized inverters; nonlinear loads; HIL

1. Introduction

The parallelization of single-phase inverters without communications between them has usually been performed using the droop method, which drives the sinusoidal references of the inverters for sharing the common loads [1–3]. The method introduces proportional droops in the inverter frequency ω^* and voltage amplitude V^* references, respectively, according to the P and Q load consumed powers. These powers are usually obtained as the product of the measured output current $i_o(t)$ with the measured output voltage $v_o(t)$ and its quadrature version, $v_{o\perp}(t)$, respectively. The droop method works well for the sharing of linear loads but not for nonlinear ones, due to the nonlinear currents drawn by these loads, which highly distort P and Q , and the provided droop references. Therefore, LPFs in P and in Q with a very low cut-off frequency are used to deal with this problem. The LPFs provide the average powers consumed by the load P_{av} and Q_{av} and removes the double frequency components

resulting from the product of $i_o(t)$ with $v_o(t)$ and $v_{o\perp}(t)$. However, these LPFs force the droop to run slowly, with a low dynamic response to changes in the load, worsening the system stability [4–15].

The calculation of P_{av} and Q_{av} is performed by the droop-based local control algorithm of the single-phase inverters and needs of the $i_o(t)$, $v_o(t)$ and $v_{o\perp}(t)$ inverter sensed signals. The quadrature output voltage $v_{o\perp}(t)$ has been performed using different approaches applied to $v_o(t)$, such as a transport delay (TD) [15,16], an extended three-phase dq-Synchronous Reference Frame (dq-SRF) approach [17,18], and the SOGI filter [19]. Additionally, P_{av} and Q_{av} have been obtained by different approaches for improving the performance of the droop method. In [20], a method based on the SOGI structure for the calculation of P_{av} and Q_{av} was proposed. The method was similar to [9], and cancelled the double frequency components resulting from the products in the same manner. In this case, the dynamic response of the calculated powers was reduced by one order of magnitude. However, this work only considered the use of linear loads, and used LPFs to obtain P_{av} and Q_{av} that constrained the dynamic response of the system. In [21], a method based on the discrete Fourier transform (DFT) was presented for extracting P_{av} and Q_{av} . This method had the drawback of introducing a severe delay into the process, making it unsuitable for systems with abrupt load changes. In [22], a Least Mean Squares (LMS) approach was presented for obtaining the averaged powers through optimization of a cost function depending on P and Q . However, the validity of these approaches was only partial when sharing nonlinear loads, except for the last one, in which nonlinear loads were considered. In general, all of these proposals have in common the objective of trying to achieve a faster and accurate calculation of the averaged powers for enhance the droop system stability.

This paper is a natural continuation of our previous work [23] in which a DSOGI approach was introduced in the power calculation scheme proposed in [9] and [20]. The DSOGI achieves the fundamental component of the inverter output current and removes the LPFs from the scheme, which had until now been the main limitation on the performance of the droop controller. The DSOGI has an inherent trade-off relationship between its filtering capability for extracting the fundamental component and its transient response speed to changes in the input signal. This trade-off is regulated by the adjustment of the DSOGI damping factor ξ . The DSOGI trade-off is better than that achieved by the standard SOGI. Then, the DSOGI can reach a faster transient time response to changes in the load for similar filtering capability than the SOGI structure. In this paper, comparisons with the calculation methods of [6] and [17] when using symmetrical and non-symmetrical nonlinear loads are presented using simulations, HIL platform and experimental platform results to prove the validity of this proposal for calculating the average powers.

2. Materials and Methods

The scheme of a single-phase voltage source inverter (VSI) operated with the droop method when sharing a nonlinear load Z_{NL} with another inverter is depicted in Figure 1. From the scheme, the main parts considered in this work can be seen: the power stage with inner controller, the pulse width modulation block (PWM), the LC output filter, the v_o and i_o sensing, the P_{av} and Q_{av} calculation block, and the droop generator producing the voltage reference v_{ref} [24,25]. In Figure 1, the scheme of the second inverter is not depicted. Rather, it is only outlined with discontinuous lines and indicated as #Inv. 2, due to the fact that this proposal is only concerned with the dynamic behavior and accuracy of the P - Q calculation block. For this reason, the simulations and experimental results shown from now on will only correspond to a single VSI.

In the simulations and experiments, a diode bridge rectifier (DBR) supplying a RC load is used as a nonlinear load Z_{NL} (see Figure 2). At steady state, Z_{NL} draws a distorted and symmetrical nonlinear current with peak levels reaching ± 2.48 A for the Z_{NL} specified in Table 1, which induces a high distortion in P_{av} and Q_{av} , as well as in v_{ref} . Likewise, a switch $S1$ is inserted in the Z_{NL} scheme (see Figure 2), allowing for step-perturbations for testing the dynamic behavior of P_{av} and Q_{av} and for assessment and comparison purposes.

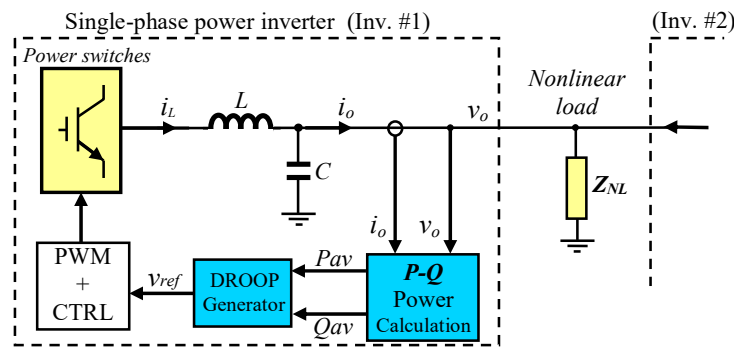


Figure 1. Block scheme of a single-phase voltage source inverter (VSI) (Inv. #1) sharing a nonlinear load with a second inverter (Inv. #2) and showing the P-Q power calculation, the Droop Generator and the PWM (pulse width modulation) control blocks.

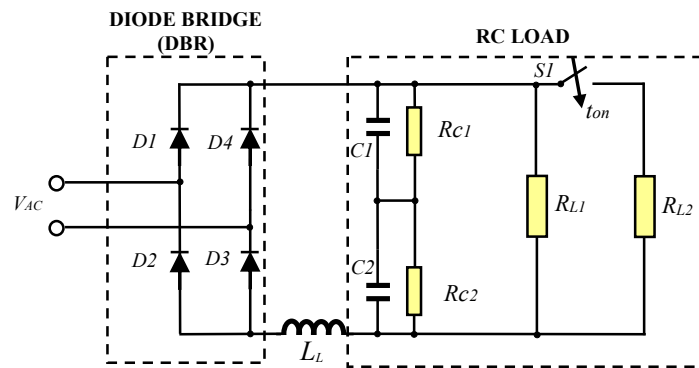


Figure 2. Diode-bridge rectifier nonlinear load supplying a resistive-capacitive load.

Table 1. Main parameters of VSI and Z_{NL} .

Parameter	Value
LC Filter	1.8 mH; 25 μ F
Switching frequency, f_s	10 kHz
$R_{onD1-D4}$	0.01 Ω
L_L	84 μ H
$C1, C2$	470 μ F
R_{C1}, R_{C2}	37 k Ω
R_{L1}, R_{L2}	960 Ω

Simulations of the proposed system for the design and comparisons with [6,17] were performed with Matlab/Simulink/Simscape Power Systems software. Table 1 shows the main parameters of the inverter and Z_{NL} .

All the power calculation schemes were tuned to achieve the same power-ripple in order to obtain a fair comparison between the methods and to accurately measure the settling time of their transient responses when Z_{NL} changes suddenly. The simulation results were obtained using Matlab/Simulink/Simscape Power Systems software, and were contrasted with HIL results at the inverter-based intelligent Microgrid Laboratory (iML) of the department of Energy Technology at the Aalborg University (iML-AAU) in Denmark (Figure 3).

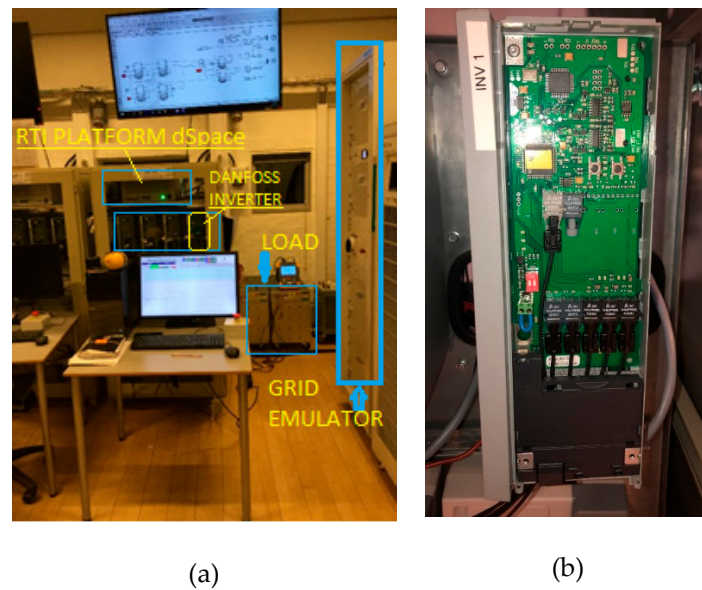


Figure 3. Experimental setup at the intelligent Microgrid Laboratory in Aalborg University (iML-AAU), Denmark: (a) Complete experimental setup; (b) detail of the Danfoss© single-phase inverter.

A second similar test was performed with another diode bridge rectifier nonlinear load drawing an asymmetrical nonlinear current in order to further test the calculation power block. This current reached a peak of 4.2 A in the positive half-cycle of the VSI and a negative one of -2.2 A in the VSI negative half-cycle after an abrupt load change. This asymmetry in the current introduced an extra distortion to the calculated powers. Experimental results for this load with a VSI inverter of the iML-AAU were also obtained. The inverter used in the iMG is a Danfoss© FC302, 2.2 kW rated, interfaced to a real-time dSPACE 1006. The algorithms for operating the VSI are developed in Matlab/Simulink software and compiled into the dSPACE. Figure 4 depicts the scheme of this experimental setup.

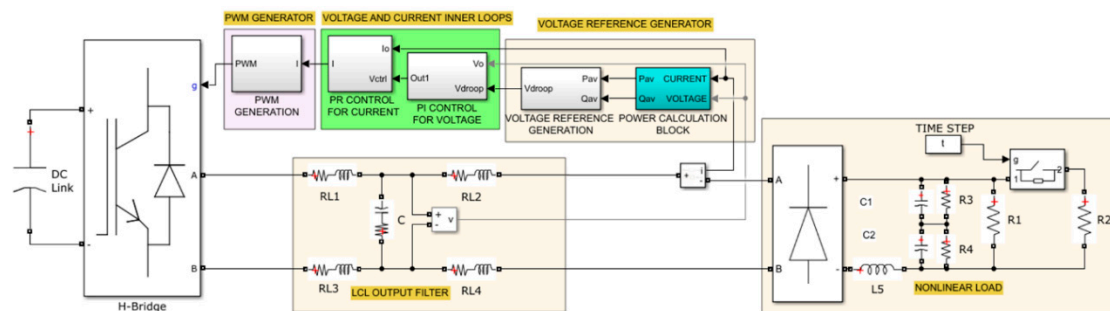


Figure 4. Scheme of the VSI experimental setup implemented at the iMG_AAU.

2.1. Droop Principle-Based Control Scheme

The power calculation block of Figure 1 provides the frequency and voltage amplitude references ω^* and V^* , respectively, as can be seen in the following equations:

$$\omega^* = \omega_n - m \cdot P_{av} \quad (1)$$

$$V^* = V_n - n \cdot Q_{av} \quad (2)$$

where m and n are the droop coefficients and ω_n and V_n are the nominal frequency and voltage amplitude, respectively. These references are used to generate the sinusoidal voltage reference v_{ref} for the inverter inner control loops:

$$v_{ref} = V^* \cdot \sin(\omega^* \cdot t) \quad (3)$$

Assuming that the output voltage and current of the inverter are [15]

$$v_o(t) = V \cdot \sin(\omega_o \cdot t) \quad (4)$$

$$i_o(t) = I \cdot \sin(\omega_o \cdot t - \varphi_o) \quad (5)$$

where V and I are the voltage and current amplitudes, ω_o is the fundamental frequency and φ_o is the phase angle between $v_o(t)$ and $i_o(t)$, the quadrature voltage, with a $-\pi/2$ delay, is defined as

$$v_{o\perp}(t) = V \cdot \sin\left(\omega_o \cdot t - \frac{\pi}{2}\right) \quad (6)$$

Therefore, the instantaneous active and reactive powers can be formulated as

$$p_i(t) = v_o(t) \cdot i_o(t) = \frac{VI}{2} \cdot [\cos\varphi_o - \cos(2\omega_o \cdot t - \varphi_o)] = P_{av} + \tilde{p} \quad (7)$$

$$q_i(t) = v_{o\perp}(t) \cdot i_o(t) = \frac{VI}{2} \cdot [\sin\varphi_o - \sin(2\omega_o \cdot t - \varphi_o)] = Q_{av} + \tilde{q} \quad (8)$$

where \tilde{p} and \tilde{q} are the oscillating components that pulsate at twice the fundamental frequency ω_o . These equations reveal that for a linear load that draws a sinusoidal current, the instantaneous powers oscillate around the averaged powers P_{av} and Q_{av} . However, if the load is nonlinear, the instantaneous powers are going to be highly distorted by harmonics, for which the nonlinear current can be expressed as:

$$i_o(t) = I_0 \cdot \sin(\omega_o t - \varphi_o) + \sum_{h=2}^N I_h \cdot \sin(h \cdot \omega_o \cdot t - \varphi_h) \quad (9)$$

leading to

$$p_i(t) = P_{av} + \tilde{p} + v_o(t) \cdot \sum_{h=2}^N I_h \cdot \sin(h \cdot \omega_o \cdot t - \varphi_h) \quad (10)$$

$$q_i(t) = Q_{av} + \tilde{q} + v_{o\perp}(t) \cdot \sum_{h=2}^N I_h \cdot \sin(h \cdot \omega_o \cdot t - \varphi_h) \quad (11)$$

where the subscript h represents the harmonic order, N is the maximum considered value for h and I_h , $h \cdot \omega_o$ and φ_h are the amplitude, the frequency and the phase-shift of the current harmonic components, respectively. As can be seen in Equations (10) and (11), $p_i(t)$ and $q_i(t)$ contain higher harmonic order components, in addition to the DC P_{av} and Q_{av} and the double frequency components \tilde{p} and \tilde{q} that were already present in the linear case. Then, for a nonlinear Z_{NL} , Equations (1) and (2) can be expressed as follows when they are calculated employing the instantaneous powers in Equations (10) and (11):

$$\omega^*(t) = \omega_n - m \cdot \left(P_{av} + \tilde{p} + v_o(t) \cdot \sum_{h=2}^N I_h \cdot \sin(h \cdot \omega_o \cdot t - \varphi_h) \right) \quad (12)$$

$$V^*(t) = V_n - n \cdot \left(Q_{av} + \tilde{q} + v_{o\perp}(t) \cdot \sum_{h=2}^N I_h \cdot \sin(h \cdot \omega_o \cdot t - \varphi_h) \right) \quad (13)$$

and the voltage reference is

$$v_{ref}(t) = V^*(t) \cdot \sin(\omega^*(t) \cdot t) \quad (14)$$

2.2. Conventional P-Q Calculation Schemes

Figure 5 shows the conventional P-Q calculation scheme for obtaining P_{av} and Q_{av} , in which the instantaneous powers $p_i(t)$ and $q_i(t)$ are obtained as the products of $i_o(t)$ with $v_o(t)$ and $v_{o\perp}(t)$, respectively [6]. The quadrature voltage $v_{o\perp}(t)$ is obtained by delaying $v_o(t)$ by $\pi/2$, and P_{av} and Q_{av} by using LPFs with a low cut-off frequency value f_c , to filter the multiple frequency components in the instantaneous powers [18]. When sharing linear loads, the value of f_c is usually set to one or two orders of magnitude lower than the inverter fundamental operating frequency [22,23], which determines the transient dynamic performance of the system. However, in the case of nonlinear loads, the value of f_c should be further reduced (usually to less than 1 Hz), to avoid strong distortions in the inverter output current and in the instantaneous powers [24]. Conversely, the distortion in the current induces excessive ripple in the averaged powers, which in turn is translated to the droop references $\omega^*(t)$ and $V^*(t)$, and then to $v_{ref}(t)$, causing bad operation of the system. Nevertheless, this bandwidth reduction slows down the transient dynamic behavior of the system. The transfer functions of the averaged P_{av} and Q_{av} are shown in Appendix A.

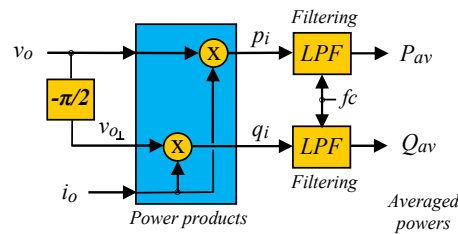


Figure 5. Block diagram of conventional P-Q power calculation providing the averaged powers P_{av} and Q_{av} .

2.3. The SOGI and DSOGI Approach

A SOGI is a special linear filter with one input, $v_{in}(t)$, and two outputs, $v_d(t)$ and $v_q(t)$, one in phase and the other delayed $\pi/2$ with respect to the input, respectively, see Figure 6.

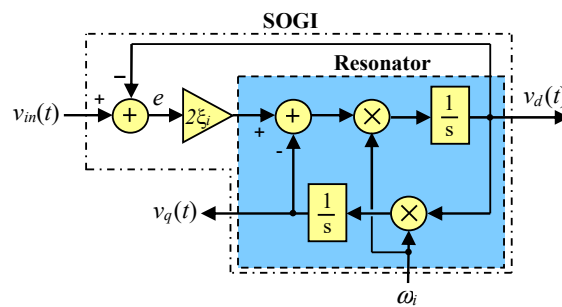


Figure 6. Block diagram of the SOGI (second-order generalized integrator) filter.

The outputs of the SOGI filter, $v_d(t)$ and $v_q(t)$, have the following band-pass filter (BPF) and LPF transfer function relationships regarding to the input:

$$H_d(s) = \frac{v_d(s)}{v_{in}(s)} = \frac{2\xi_i\omega_i s}{s^2 + 2\xi_i\omega_i s + \omega_i^2} H_d(s) = \frac{v_d(s)}{v_{in}(s)} = \frac{2\xi_i\omega_i s}{s^2 + 2\xi_i\omega_i s + \omega_i^2} \quad (15)$$

$$H_q(s) = \frac{v_q(s)}{v_{in}(s)} = \frac{2\xi_i\omega_i^2}{s^2 + 2\xi_i\omega_i s + \omega_i^2} H_q(s) = \frac{v_q(s)}{v_{in}(s)} = \frac{2\xi_i\omega_i^2}{s^2 + 2\xi_i\omega_i s + \omega_i^2} \quad (16)$$

where ξ_i is the filter damping factor and ω_i is the tuning center frequency. In addition, a DSOGI is a four-order filter that consist in the cascade connection of two SOGI filters, as seen in Figure 7 [26]:

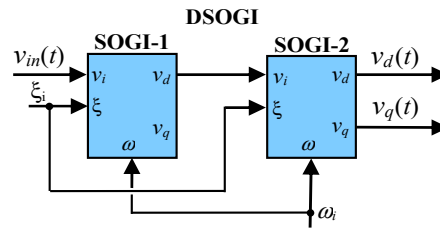


Figure 7. Block diagram of a DSOGI (double SOGI) filter as the cascading of two individual SOGIs.

The transfer functions of the DSOGI with respect to the input [26]:

$$H'_d(s) = \left(\frac{2\xi_i\omega_i s}{s^2 + 2\xi_i\omega_i s + \omega_i^2} \right)^2 \quad (17)$$

$$H'_q(s) = \frac{4\xi_i^2\omega_i^3 s}{(s^2 + 2\xi_i\omega_i s + \omega_i^2)^2} \quad (18)$$

When ω_i is tuned to match ω_o , and for harmonic components higher than the fundamental ($h \gg 1$), the gain of the BPF characteristic in Equation (17) can be simplified to:

$$|H'_d(s)| = \left(\frac{2\xi_i h}{\sqrt{(1-h^2)^2 + (2\xi_i h)^2}} \right)^2 \approx \left(\frac{2\xi_i}{h} \right)^2 |H'_d(s)| = \left(\frac{2\xi_i h}{\sqrt{(1-h^2)^2 + (2\xi_i h)^2}} \right)^2 \approx \left(\frac{2\xi_i}{h} \right)^2 \quad (19)$$

On the other hand, the frequency and damping factor are the parameters that determine the settling time t_s (2% criterion) of the transient response of the BPF in Equation (15) for a step input:

$$t_s \approx \frac{4}{\xi_i \omega_i} \quad (20)$$

The SOGI filter has an inherent trade-off relationship between bandwidth (rejection capability to harmonics) and settling time response, Equation (20). This trade-off cannot be overcome, and relies on the damping factor parameter ξ_i . However, in [26], it was shown that the DSOGI has a better trade-off than the SOGI and can achieve a faster transient response when it is designed to have the same bandwidth behavior. In this paper, this characteristic is used to achieve a faster response when extracting the fundamental component of the nonlinear load current and thereby to improve the droop transient response to load changes.

2.4. Advanced P-Q Calculation Scheme

Figure 8 shows a P-Q calculation method based on the proposed scheme in [17] for accelerating the computation of P_{av} and Q_{av} . In this figure, the SOGI1 and SOGI2 blocks are used for extracting the double frequency pulsating power components \tilde{p} and \tilde{q} , which are then removed from p_i and q_i . These SOGIs are both tuned at $\omega_i = 2\omega_o$ and $\xi_1 = \xi_2 = 1$. The LPFs are used for improved filtering and for providing the averaged powers P_{av} and Q_{av} , by attenuating the higher harmonics components reported in Equations (10) and (11). This figure does not show the method for generating the $\pi/2$ delay, since it is not mentioned in [17]. Therefore, another SOGI, SOGI0, tuned at ω_o and $\xi_0 = \xi_v = 0.707$, is used for generating this delay, as shown in Figure 9, for avoiding the delay issues reported in [15,16].

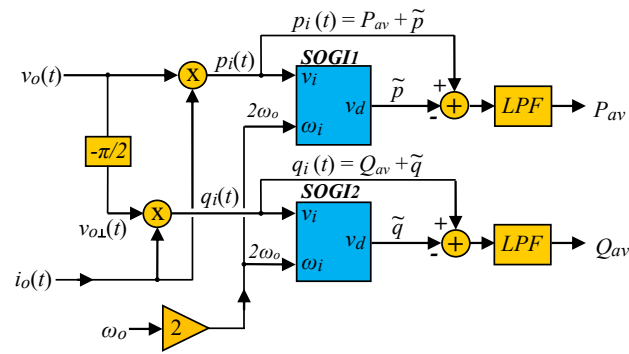


Figure 8. Scheme for the calculation of P_{av} and Q_{av} proposed in [20].

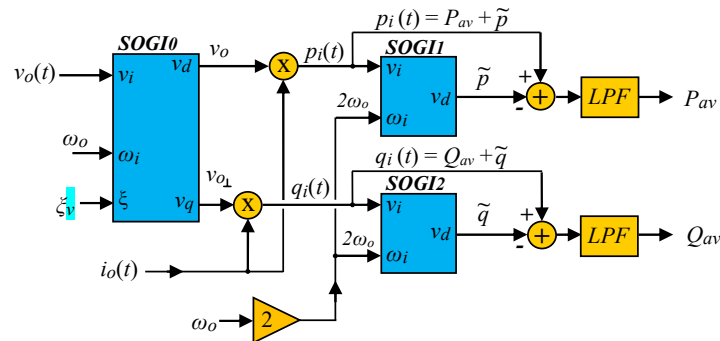


Figure 9. Addition to Figure 8 of a new SOGI for archiving the quadrature component of the output voltage $v_{o\perp}(t)$.

The transfer functions for the calculated averaged active and reactive power are included in Appendix A, with the numbers (24) and (25). Please note that the current is not filtered.

Figure 10 shows the simulation results using the P-Q algorithms of the schemes in Figures 5 and 9 when sharing a linear load that produces a current perturbation from peak 2 A to peak 4 A at a time of 3 s.

For the sake of simplicity, Figure 10 only shows the dynamic behavior of P_{av} , obviating the representation of Q_{av} . The dynamics of P_{av} obtained with the advanced scheme in Figure 9 (hereinafter called P_{adv}) are compared with those obtained for P_{av} by the conventional droop method depicted in Figure 5 (hereinafter called P_{droop}). The cut-off frequency of the LPFs in Figure 9 was designed to be $f_c = 3.7$ Hz, whereas it was set to $f_c = 0.37$ Hz for the scheme in Figure 5. As shown in Figure 10, the double frequency component \tilde{p} was removed from P_{adv} . Likewise, the higher cut-off frequency of its LPFs results in much faster dynamics than those of P_{droop} . Also, the ripple corresponding to the double frequency component \tilde{p} , which is not completely filtered by the LPFs in Figure 5, can be observed in P_{droop} . These results are compatible with those reported in [21]. However, the good dynamic behavior depicted in Figure 10 for P_{adv} vanishes when a nonlinear load is used, as is shown in Figure 11. In this case, the nonlinear load is a DBR that draws a peak current of ± 2.48 A and suffers a perturbation that pushes the peak to ± 4.15 A. The simulation parameters are listed in Table 2.

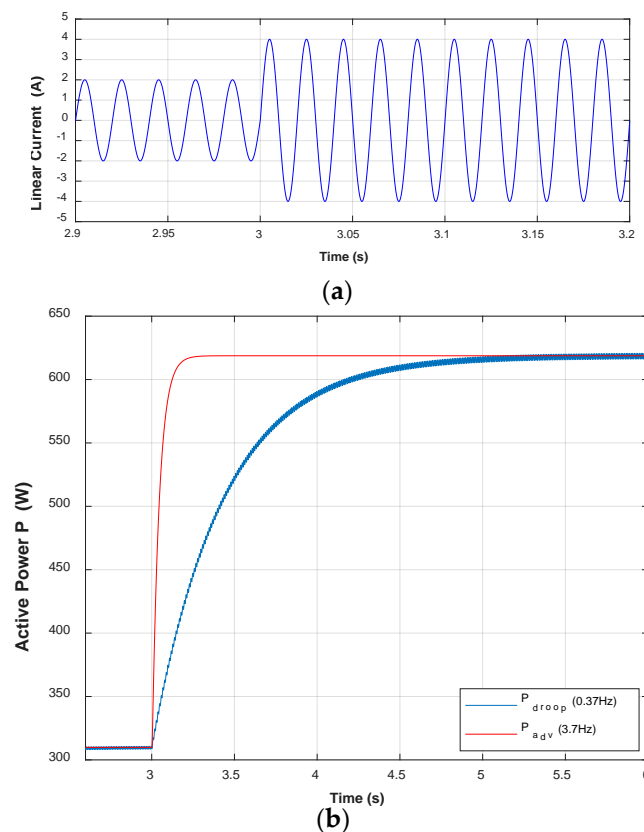


Figure 10. Simulation of the load current and P_{av} transient responses for a linear load current perturbation from peak 2A to peak 4A at 3 s: (a) detail of the load current perturbation, (b) comparison between P_{av} obtained with Figure 9 scheme (P_{adv}) and P_{av} obtained with Figure 5 scheme (P_{droop}).

Table 2. Simulation parameters for Figure 10.

Parameter	Value
V_n	311 V
ω_o	$2\pi 50$ rad/s
DBR RESISTOR LOAD FOR $T < 3S$	950Ω
DBR RESISTOR LOAD FOR $T > 3S$	471.8Ω
THD $i_o(t)$	215%
ξ_0	0.7
$\xi_1 = \xi_2$	1

As shown in Figure 11, the dynamics of the method proposed in [20] worsen using a nonlinear load, similarly to [26]. Thus, in the presence of a nonlinear load, the method has excessive steady state ripple that corrupts the calculated powers, opposite to what is stated in [20]. To reduce the ripple, the filtering capabilities of the LPFs in Figure 9 can be improved by reducing f_c . By decreasing f_c from 3.7 Hz to 1.1 Hz, the ripple of P_{adv} matches that of P_{droop} , as can be seen in Figure 12. Although the advanced method of Figure 9 calculates faster P_{av} than the conventional droop controller, it presents less effectivity than initially argued. It can be clearly seen in Figures 11 and 12 that there is a trade-off between the filtering capability of the P_{av} calculation scheme and the transient speed of its dynamical response. Note also that there is a positive offset in the calculated P_{av} at steady state, since the mean value of P_{adv} is slightly higher than that of P_{droop} (see Figure 11). Comparing the transfer functions for the P-Q calculation by the conventional, Equations (22) and (23), or by the advanced method, Equations (24) and (25), it can be seen the filtering capabilities of each algorithm. Please note that the

magnitude of the ripple of P_{adv} forces the system's dynamic response to slow down by reducing more the cut-off frequency.

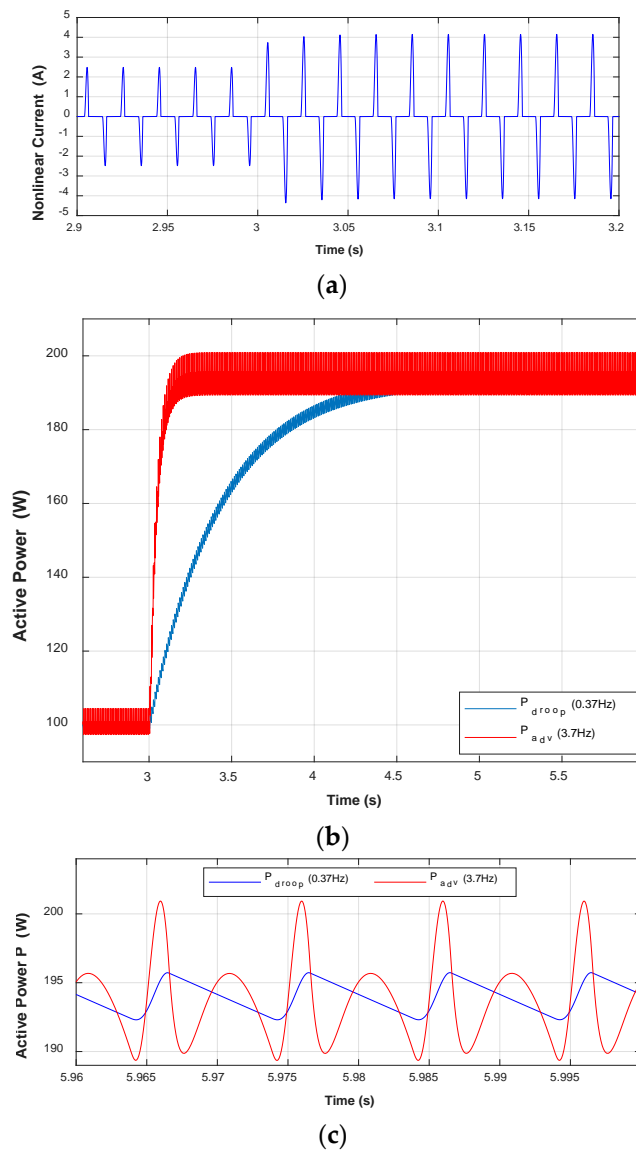


Figure 11. Simulation of the load current and P_{adv} transient responses for a nonlinear Diode Bridge Rectifier (DBR) load current perturbation from a peak at 2.48 A to a peak at 4.15 A at 3 s: (a) detail of the distorted load current perturbation, (b) P_{adv} and P_{droop} , (c) detail of P_{adv} and P_{droop} ripples.

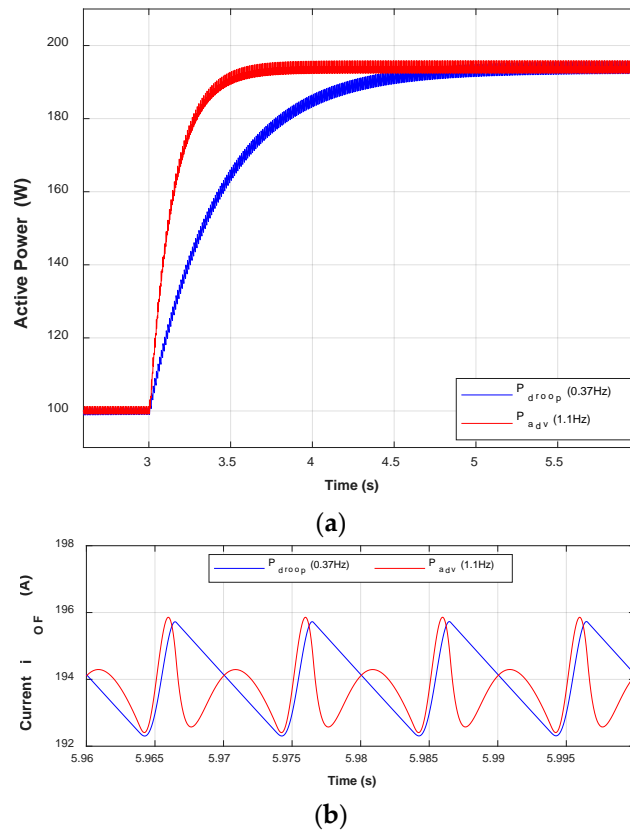


Figure 12. Simulation of the P_{av} transient responses for a nonlinear DBR (diode bridge rectifier) load current perturbation from a peak at 2.48 A to a peak at 4.15 A at 3 s: (a) P_{adv} (with reduced $f_c = 1.1$ Hz) and P_{droop} , (b) detail of P_{adv} and P_{droop} ripples.

2.5. Proposed P-Q Calculation Scheme

The scheme of the proposed P - Q calculation is shown in Figure 13. A DSOGI approach is applied to $i_o(t)$ in order to extract the fundamental component i_{OF} , see Equation (28) in Appendix A. There, the DSOGI composed of the $SOGI3$ and $SOGI4$ blocks filters the distorting high-order harmonics of $i_o(t)$ by means of its higher BPF capability and avoids coping with a highly distorted current signal. Consequently, the instantaneous powers $p_i(t)$ and $q_i(t)$ are obtained as the product of the in-phase $v_o(t)$ or the quadrature $v_{o\perp}(t)$ voltages with the fundamental output current i_{OF} , respectively. This produces a result with only double frequency components and without third or higher order harmonics.

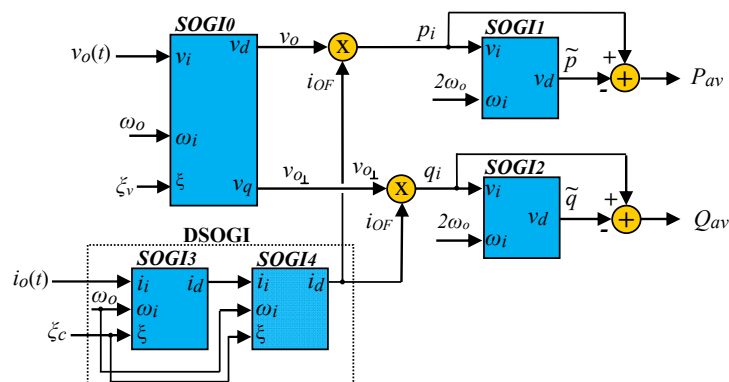


Figure 13. Scheme for the proposed P - Q calculation based on a DSOGI approach.

Later, the *SOGI1* and *SOGI2* blocks were used as in Figure 9 for removing only the double frequency components with the help of the subtracting blocks. Therefore, the LPFs can now be removed from the scheme, since they are no longer necessary. The transfer function of the proposed scheme in Figure 13 is shown in Appendix A as Equations (26) and (27). This overcomes the main limitation of previous schemes and further accelerates the dynamic response of P_{av} and Q_{av} . To distinguish P_{av} and Q_{av} obtained with this proposed scheme, in the following they will be referred to as P_{DSOGI} and Q_{DSOGI} .

In this case, because a DSOGI is used for filtering the current in Equation (28), and considering that the center frequencies provided by the droop method ω^* vary in a small range around the nominal frequency ω_n , the transient response speed is determined mainly by the DSOGI transient response, which is related to ξ_c ; see [26]. The damping factors of the DSOGI are here tuned to produce a power ripple identical in amplitude to that of the conventional droop controller, which is achieved for $\xi_c = \xi_3 = \xi_4 = 0.129$.

Figure 14 shows the simulation results of the same nonlinear DBR load drawing a peak current of ± 2.48 A and suffering a perturbation that pushes the peak to ± 4.15 A. It can be observed that the proposed method is faster for calculating P_{av} than the previously considered methods.

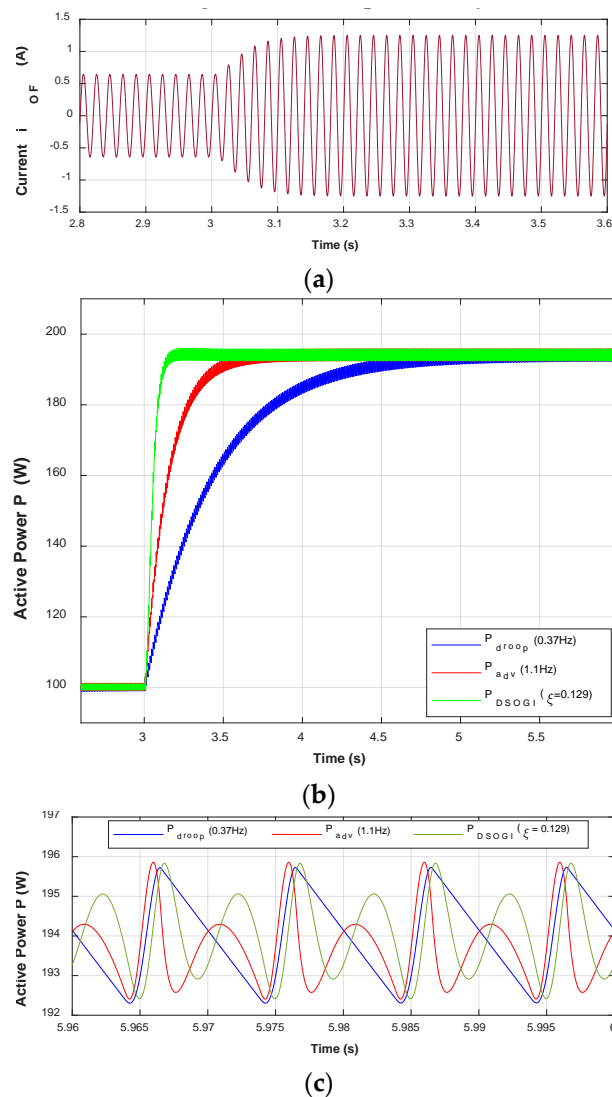


Figure 14. Simulation of i_{OF} and P_{av} transient responses for a nonlinear DBR load current perturbation from a peak of 2.48 A to 4.15 A at 3 s: (a) detail of the i_{OF} perturbation, (b) P_{DSOGI} , P_{adv} and P_{droop} , (c) detail of P_{DSOGI} , P_{adv} and P_{droop} ripples.

Figure 15 depicts the simulation results using a Z_{NL} drawing an asymmetrical current, reaching a positive peak of 5.21 A and a negative peak of -3.07 A after the perturbation. In this case, the asymmetry in the nonlinear current (see Figure 15a), introduces further distortion into the calculated P_{av} , showing higher ripple at steady state (see Figure 15c).

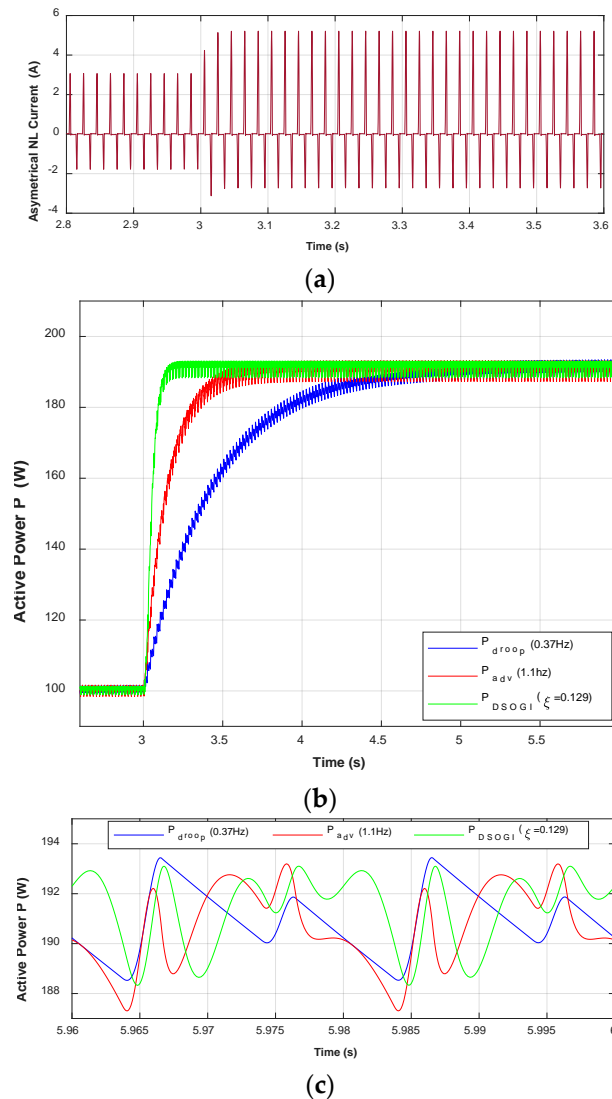


Figure 15. Simulation of the load current and P_{av} transient responses for an asymmetrical nonlinear DBR load current with a positive peak of 5.21 A and a negative peak of -3.07 A after the perturbation at 3 s: (a) detail of the asymmetrical load current perturbation, (b) P_{DSOGL} , P_{adv} and P_{droop} , (c) detail of P_{DSOGL} , P_{adv} and P_{droop} ripples.

Please note that unlike P_{adv} , P_{DSOGL} does not exhibit a positive offset error in steady state. This means that the proposed method is also more accurate than that in [20]. Table 3 contains the measured settling time for the P_{av} transient responses depicted in Figure 15, which shows that the P_{DSOGL} calculated with the proposed method implies a 60.00% and a 79.69% reduction in the response time regarding P_{adv} and P_{droop} , respectively.

Table 3. Settling time simulation measurements from Figure 15.

Parameter	Value
P_{DROOP}	325 ms
P_{ADV}	165 ms
P_{DSOGI}	66 ms

3. Experimental Results

Hardware in Loop, as well as experimental results with an VSI inverter of the iML-AAU, were obtained. The HIL setup consisted of a dSpace 1006© digital Real-Time Interface platform that carried out the processor-based simulations with parameters configured by the dSpace Configuration Desk © tool. The setup supports models based on the physical modelling libraries of electrical plants designed by Matlab/Simulink/SimPowerSystems©. These models are integrated into the dSpace tool chain and are used for building the electrical system under test along with the Electronic Central Unit, ECU, of the dSpace. The control algorithms described in this paper were loaded and executed in real time in the ECU. In this case, the H-Bridge Inverter, the LCL filter and the Nonlinear Load depicted in Figure 4 are the electrical system implemented in the ECU under the HIL test. The experimental setup consisted of an inverter Danfoss© FC302, 2.2 kW rated, interfaced to the real-time dSPACE 1006 digital platform. The algorithms for operating the VSI were developed in Matlab/Simulink software and compiled in the dSPACE multiprocessor core, with its parameters configured and controlled through the Configuration-Desk software. The sampling frequency for the system was 10 kHz, which was the switching frequency for the VSI. A third-order method for discretizing the SOGI and DSOGI algorithms was employed, whereby the integrator $\frac{1}{s}$ was approximated as:

$$\frac{T_s}{12} \cdot \frac{5z^{-3} - 16z^{-2} + 23z^{-1}}{1 - z^{-1}} \quad (21)$$

with T_s being the sample time of 100 μ s, which is consistent with the 10 kHz frequency. The experimental setup parameters for the LCL filter and for the nonlinear load are listed in Table 4.

Table 4. Main parameters of VSI and Z_{NL} .

Parameter	Value
$RL1 = RL2 = RL3 = RL4$	1.8 mH; 0.01 Ω
RC branch	25 μ F; 1 Ω
Switching frequency, f_s	10 kHz
$R_{onD1 \text{ and } D4} / R_{onD2 \text{ and } D3}$	0.01 Ω / 1 Ω
L_L	84 μ H
$C1 = C2 / R_{c1} = R_{c2}$	470 μ F / 37 k Ω
R_{L1}, R_{L2}	960 Ω

In this section, HIL results are shown first for a Z_{NL} drawing a symmetrical current, and then the results for a VSI with a Z_{NL} drawing an asymmetrical current.

Figure 16 depicts the HIL P_{av} results for a Z_{NL} drawing a symmetrical current with peak values transitioning from ± 2.48 A to ± 4.15 A after a step perturbation at 1.28 s. The dynamics of P_{av} obtained with the different considered methods are represented in green for P_{droop} , in blue for P_{adv} and in red for P_{DSOGI} .

Figure 17 shows a detail of the P_{av} ripple waveforms at steady state, evidencing the different nonlinearities resulting from each power calculation method. There are some DC errors in the calculated powers that can mainly be attributed to the discretization method in Equation (21) and to the sampling frequency. This phenomenon was not evidenced in the simulations shown in Figure 15c, but is reflected in the HIL results.

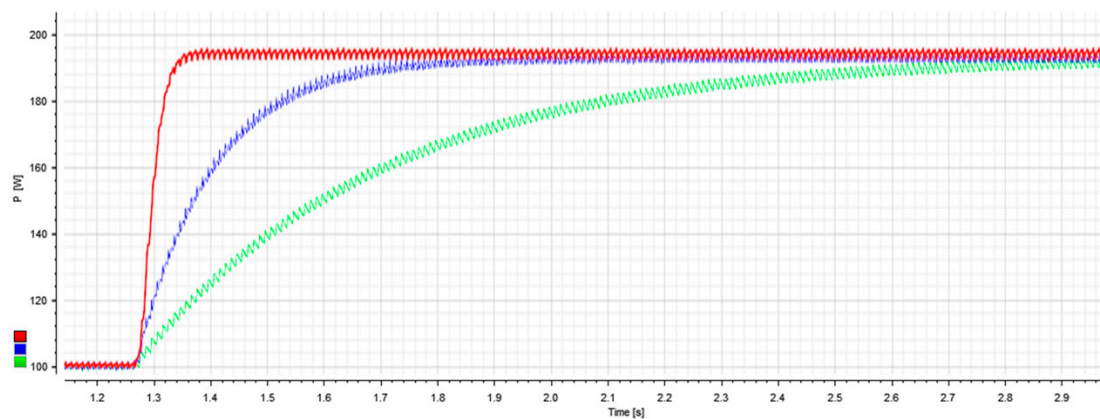


Figure 16. HIL P_{av} results for a Z_{NL} drawing a symmetrical current with peak values from ± 2.48 A to ± 4.15 A after a step perturbation at 1.28 s (P_{droop} in green, P_{adv} in blue, P_{DSOGI} in red).

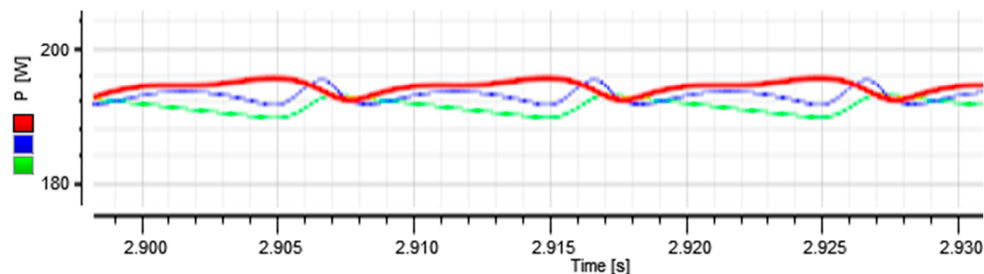


Figure 17. Detail of HIL P_{av} ripples at steady-state from Figure 14 (P_{droop} in green, P_{adv} in blue, P_{DSOGI} in red).

Figure 18 shows the output voltage $v_o(t)$ waveform of the VSI (Figure 18a), the current waveform drawn for the DBR load and used for obtaining the VSI results (Figure 18b) and the fundamental current component i_{OF} extracted by the DSOGI (Figure 18c). Note the current asymmetry, with positive peaks that reach 4.2 A and negative ones that reach -2.8 A. Note how a fundamental current component i of 1.5 A amplitude has been achieved.

Finally, Figure 19 depicts the P_{av} experimental VSI results with the DBR load when a perturbation is applied at 8.9 s. Note in this figure that the results are coherent with those obtained by HIL, as shown in Figure 16, and by the simulations in Figure 15.

Table 5 presents the settling time of P_{av} obtained with all the considered P-Q calculation methods, as measured in Figure 15 for Matlab/Simulink[®] simulations results, in Figure 16 for the HIL results, and in Figure 19 for the experimental VSI results. In this table, the achieved percentage of settling time reduction with respect to the conventional droop method is also indicated. Note how the proposed method achieves a faster response. The transfer functions for the active and reactive averaged powers of the droop, advanced and DSOGI methods are shown in Appendix A.

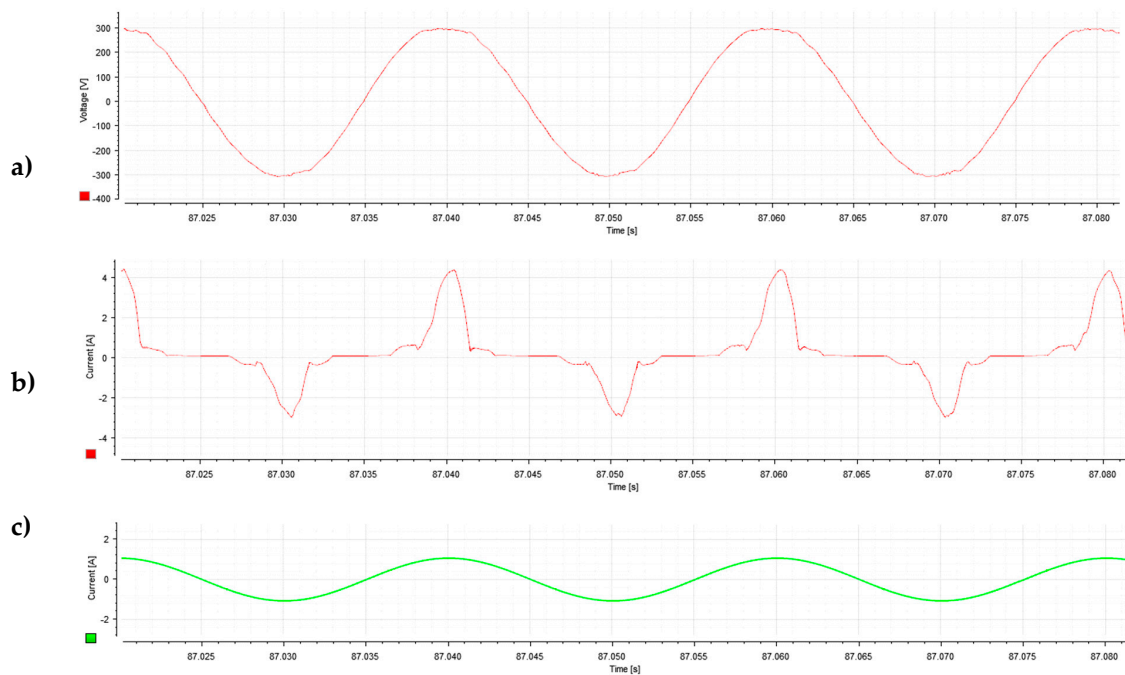


Figure 18. VSI output voltage and asymmetrical current waveforms drawn by the nonlinear DBR load used to obtain the VSI results. (a) Output voltage, $v_o(t)$; (b) asymmetrical nonlinear current; (c) fundamental component i_{OF} extracted by the DSOGI.

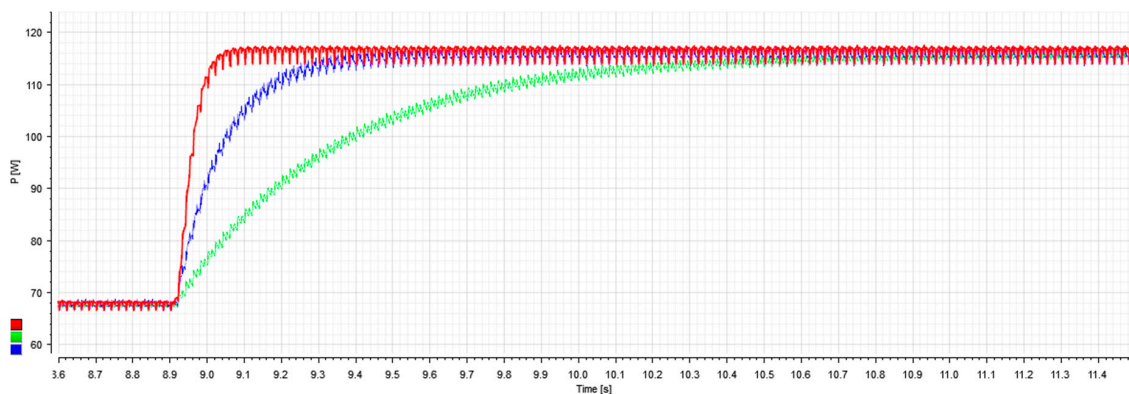


Figure 19. VSI experimental result of the P_{droop} transient response for the nonlinear DBR load current perturbation in Figure 18 (P_{droop} in green, P_{adv} in blue, P_{DSOGI} in red).

Table 5. Experimental results for the VSI setup.

P-Q Algorithm	Settling Time Matlab (ms)/(%reduction)	Settling Time HIL (ms)/(%reduction)	Settling Time VSI (ms) /(%reduction)
Conventional, P_{droop}	760 / (—)	780 / (—)	930 (—)
Advanced, P_{adv}	310 / (59%)	330 / (58%)	360 (61%)
Proposed, P_{DSOGI}	130 / (83%)	140 / (82%)	180 (80%)

4. Discussion

In this work, a P - Q calculation method was proposed for single-phase inverters with the purpose of improving the speed and accuracy of the power calculation when they are sharing linear and nonlinear loads. The dynamic response of the power calculation used in the conventional droop method and in another advanced method was first analyzed to show their limitations in speed and accuracy

when sharing a DBR-type nonlinear load. For this reason, a novel calculation method was proposed, bearing in mind the dynamic transient response velocity of the system to sudden perturbations in the shared load. The method was studied and compared with previous ones by obtaining results from Matlab®-based simulations, the HIL platform, and a VSI experimental setup. These results show how the proposed method achieves, under the same distorting conditions, a faster calculation settling time with a measured time reduction over the conventional droop method that arrives around 80%, which is higher than the achieved by the advanced method. This improvement supposes an enhancement in the droop speed operation under linear and nonlinear load conditions that leads to a better dynamic performance of the system when parallelizing inverters or microgrid operation in islanded mode.

The aim of this work was to identify what the main limitation of the power calculation methods was for sharing linear and nonlinear loads, and to propose a new approach based on the DSOGI scheme. This issue can be further investigated by using the SOGI approach and other ones for obtaining the fundamental component of the distorted current signals with less effort, faster, and best quality. This would help in the operation and stability of the inverters when sharing linear and nonlinear loads.

Author Contributions: Investigation, simulation results and writing—original draft, J.E.M. and J.M.; methodology and formal analysis, J.E.M., J.M., H.M. and J.M.G.; writing—review and editing, J.E.M., J.M., H.M.; writing—response to reviewers, J.M. and H.M.; software design, J.E.M., J.M. and M.L.; laboratory setup, HIL and experimental results, J.E.M., M.L., and Y.G.; data curation, J.E.M., J.M. and M.L.; laboratory organization and supervision, J.M.G.

Funding: J. M. Guerrero was funded by a Villum Investigator grant (no. 25920) from The Villum Fonden.

Acknowledgments: Thanks to Alexander Micallef, University of Malta, for his crucial support during the experimental campaign. Thanks also to the E3PACS laboratory staff from UPC, that provided technical support during the redaction of this work.

Conflicts of Interest: The authors declare no conflict of interest.

Appendix A

The transfer functions of the active and reactive averaged powers regarding the instantaneous powers of the methods described here are as follows:

$$P_{droop}(s) = \left(\frac{\omega_c}{s + \omega_c} \right) p_i(s) \quad (A1)$$

$$Q_{droop}(s) = \left(\frac{\omega_c}{s + \omega_c} \right) q_i(s) \quad (A2)$$

$$P_{adv}(s) = \left(\frac{s^2 + (2\omega_o)^2}{s^2 + 2(2\omega_o) \cdot s + (2\omega_o)^2} \right) \left(\frac{\omega_c}{s + \omega_c} \right) p_i(s) \quad (A3)$$

$$Q_{adv}(s) = \left(\frac{s^2 + (2\omega_o)^2}{s^2 + 2(2\omega_o) \cdot s + (2\omega_o)^2} \right) \left(\frac{\omega_c}{s + \omega_c} \right) q_i(s) \quad (A4)$$

$$P_{DSOGI}(s) = \left(\frac{s^2 + (2\omega_o)^2}{s^2 + 2(2\omega_o) \cdot s + (2\omega_o)^2} \right) p_i(s) \quad (A5)$$

$$Q_{DSOGI}(s) = \left(\frac{s^2 + (2\omega_o)^2}{s^2 + 2(2\omega_o) \cdot s + (2\omega_o)^2} \right) q_i(s) \quad (A6)$$

where $\omega_c = 2\pi f_c$ is the cut-off frequency in rad/s of the LPFs used in the droop- and advanced-based methods. The instantaneous powers, $p_i(t)$ and $q_i(t)$, are derived from the product between $i_o(t)$ and $v_o(t)$ and $v_{o\perp}(t)$, respectively. The transfer functions for $v_o(t)$ and $v_{o\perp}(t)$ correspond to Equations (15)

and (16) in all the methods, since a SOGI was used to achieve these signals. In addition, in the case of the current, the fundamental component i_{OF} in the DSOGI method has the following transfer function:

$$i_{OF}(s) = \left(\frac{2\xi_c \omega_o s}{s^2 + 2\xi_c \omega_o s + \omega_c^2} \right)^2 i_o(s) \quad (A7)$$

References

- Kim, J.-H.; Lee, Y.-S.; Kim, H.-J.; Han, B.-M. A New Reactive-Power Sharing Scheme for Two Inverter-Based Distributed Generations with Unequal Line Impedances in Islanded Microgrids. *Energies* **2017**, *10*, 1800. [CrossRef]
- Ren, B.; Sun, X.; Chen, S.; Liu, H. A Compensation Control Scheme of Voltage Unbalance Using a Combined Three-Phase Inverter in an Islanded Microgrid. *Energies* **2018**, *11*, 2486. [CrossRef]
- Ma, J.; Wang, X.; Liu, J.; Gao, H. An Improved Droop Control Method for Voltage-Source Inverter Parallel Systems Considering Line Impedance Differences. *Energies* **2019**, *12*, 1158. [CrossRef]
- Coelho, E.A.A.; Cortizo, P.C.; Garcia, P.F.D. Small signal stability for single phase inverter connected to stiff AC system. In Proceedings of the Record of the IEEE Industry Applications Conf. 34th IAS Annual Meeting (Cat. No.99CH36370), Phoenix, AZ, USA, 1999; Volume 4, pp. 2180–2187.
- Soshinskaya, M.; Graus, W.H.J.; Guerrero, J.M.; Vasquez, J.C. Microgrids: experiences barriers and success factors. *Renew. Sustain. Energy Rev.* **2014**, *40*, 659–672. [CrossRef]
- Araújo, L.S.; Narváez, D.I.; Siqueira, T.G.; Villalva, M.G. Modified droop control for low voltage single phase isolated microgrids. In Proceedings of the IEEE Int. Conf. on Automatica (ICA-ACCA), Curico, Chile, 19–21 October 2016; pp. 1–6.
- IEEE. *IEEE Standard Definitions for the Measurement of Electric Power Quantities Under Sinusoidal, Nonsinusoidal, Balanced or Unbalanced Conditions*; IEEE Standard 1459-2010; IEEE: New York, NY, USA, 2000; pp. 1–52.
- Lu, J.; Wen, Y.; Zhang, Y.; Wen, W. A novel power calculation method based on second order general integrator. In Proceedings of the IEEE 8th Int. Power Electronics and Motion Control Conf. (IPEMC-ECCE Asia), Hefei, China, 22–26 May 2016; pp. 1975–1979.
- Andrade, E.T.; Ribeiro, P.E.M.J.; Pinto, J.O.P.; Chen, C.L.; Lai, J.S.; Kees, N. A novel power calculation method for droop-control microgrid systems. In Proceedings of the 2012 27th Annual IEEE Applied Power Electronics Conf. and Exp. (APEC), Vladivostok, Russia, 9–10 September 2012; pp. 2254–2258.
- Ren, Z.; Gao, M.; Mo, Q.; Liu, K.; Yao, W.; Chen, M.; Qian, Z. *Power Calculation Method Used in Wireless Parallel Inverters Under Nonlinear Load Conditions*; IEEE: New York, NY, USA, 2010.
- Furtado, E.C.; Aguirre, L.A.; Torres, L.A.B. UPS Parallel Balanced Operation Without Explicit Estimation of Reactive Power—A Simpler Scheme. In *Circuits and Systems II: Express Briefs*; IEEE Trans. Eds.; IEEE: New York, NY, USA, 2008; pp. 1061–1065.
- Guerrero, J.; Matas, J.; Vicuna, L.G.; Castilla, M.; Miret, J. Decentralized Control for Parallel Operation of Distributed Generation Inverters Using Resistive Output Impedance. In *Industrial Electronics*; IEEE Trans. Eds.; IEEE: New York, NY, USA, 2007; pp. 994–1004.
- Silva, S.A.; Novotny, R.; Modesto, R.A. Single-phase PLL structure using modified p-q theory for utility connected systems. In Proceedings of the IEEE PESC, Rhodes, Greece, 15–19 June 2008; pp. 4706–4711.
- Wang, H.; Yue, X.; Pei, X.; Kang, Y. A new method of power calculation based on parallel inverters. In Proceedings of the IEEE EPE-PEMC, Novi Sad, Serbia, 28–30th October 2009; pp. 1573–1576.
- Wei, Y.; Xu, D.; Ma, K. A Novel Accurate Active and Reactive Power Calculation Method for Paralleled UPS System. In Proceedings of the APEC, Singapore, 15–16 November 2009; pp. 1269–1275.
- Ren, Z.; Gao, M.; Mo, Q.; Liu, K.; Yao, W.; Chen, M.; Qian, M. Power calculation method used in wireless parallel inverters under nonlinear load conditions. In Proceedings of the 25th Annual IEEE Applied Power Electronics Conf. and Exp., Palm Springs, CA, USA, 21–25 February 2010; pp. 1674–1677.
- Akagi, H.; Watanabe, E.; Aredes, M. *Instantaneous Power Theory and Application to Power Conditioning*; IEEE Press Series in Power Engineering; IEEE: New York, NY, USA, 2007; pp. 5–28.

18. Gao, M.; Yang, S.; Jin, C.; Ren, Z.; Chen, M.; Qian, Z. Analysis and experimental validation for power calculation based on p-q theory in single-phase wireless-parallel inverters. In Proceedings of the 26th Annual IEEE Applied Power Electronics Conference and Exposition (APEC), Hyderabad, India, 16–18 December 2011; pp. 620–624.
19. Matas, J.; Castilla, M.; d. Vicuña, L.G.; Miret, J.; Vasquez, J.C. Virtual Impedance Loop for Droop-Controlled Single-Phase Parallel Inverters Using a Second-Order General-Integrator Scheme. In *Power Electronics*; IEEE Trans. Eds.; IEEE: New York, NY, USA, 2010; pp. 2993–3002.
20. Tolani, S.; Sensarma, P. An improved droop controller for parallel operation of single-phase inverters using R-C output impedance. In *Power Electronics, Drives and Energy Systems (PEDES)*, Bengaluru; IEEE Trans. Eds.; IEEE: New York, NY, USA, 2012; pp. 1–6.
21. Yang, Y.; Blaabjerg, F. A new power calculation method for single-phase grid-connected systems. In *IEEE International Symposium on Industrial Electronics*; IEEE Eds.; IEEE: New York, NY, USA, 2013; pp. 1–6.
22. Guerrero, J.M.; Berbel, N.; Matas, J.; de Vicuna, L.G.; Miret, J. Decentralized Control for Parallel Operation of Distributed Generation Inverters in Microgrids Using Resistive Output Impedance. In Proceedings of the IECON 2006—32nd Annual Conference on IEEE Industrial Electronics, Paris, France, 7–10 November 2006; pp. 5149–5154.
23. Mariachet, J.E.; Matas, J.; Martín, H.; Abusorrah, A. Power Calculation Algorithm for Single-Phase Droop-Operated Inverters Considering Nonlinear Loads. *Renew. Energy Power Qual. J.* **2018**, *1*, 16.
24. Song, H.; Nam, K. Dual current control scheme for PWM converter under unbalanced input voltage conditions. In *Ind. Electron*; IEEE Trans. Eds.; IEEE: New York, NY, USA, 1991; pp. 953–959.
25. *IEEE Standard Definitions for the Measurement of Electric Power Quantities Under Sinusoidal, Nonsinusoidal, Balanced, or Unbalanced Conditions-Redline*; IEEE: New York, NY, USA, 2010; pp. 1–52, 1459–2010 (Revision of IEEE Std 1459-2000)-Redline, 19 March 2010.
26. Matas, J.; Castilla, M.; Miret, J.; Vicuna, L.G.; Guzman, R. An adaptive prefiltering method to improve the speed/accuracy tradeoff of voltage sequence detection methods under adverse grid conditions. *IEEE Trans. Ind. Electron.* **2014**, *61*, 2139–2151. [[CrossRef](#)]



© 2019 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).