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Drozdov, Aleksey D.; Christiansen, Jesper de Claville

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# Mechanical response and equilibrium swelling of thermo-responsive copolymer hydrogels

A.D. Drozdov and J. deClaville Christiansen

Department of Materials and Production

Aalborg University

Fibigerstraede 16, Aalborg 9220, Denmark

## Abstract

Covalently cross-linked thermo-responsive (TR) gels form a special class of hydrogels that swell noticeably below their volume phase transition temperature  $T_c$  and shrink above  $T_c$ . As the critical temperature is weakly affected by the preparation conditions and molar fractions of monomers and cross-linkers in a pre-gel solution, a facile method to modulate  $T_c$  (which is required for biomedical applications of TR gels and their use as temperature-triggered actuators) is to incorporate relatively small amounts of neutral monomers whose hydrophilicity differs from that of the basic monomers. Although observations on copolymer gels confirm the effectiveness of this method, molar fractions of comonomers necessary for tuning of  $T_c$  remain unknown.

A model is developed for the mechanical response and equilibrium swelling of TR gels. Adjustable parameters in the governing relations are found by fitting equilibrium swelling diagrams on poly(*N*-isopropylacrylamide) homo- and copolymer gels. Good agreement is demonstrated between the experimental data and results of simulation. Based on the model, an analytical formula is derived that expresses the volume phase transition temperature in terms of the molar fraction of comonomers. Its ability to predict the critical temperature is confirmed by comparison with observations on several copolymer gels.

## 1. Introduction

Hydrogels are three-dimensional networks of polymer chains bridged by chemical and/or physical bonds. Due to the hydrophilic nature of segments of chains, they swell substantially being immersed into water, but preserve their structural integrity. Thermo-responsive (TR) gels form a special class of hydrogels whose equilibrium degree of swelling is strongly affected by temperature. At temperatures  $T$  below the volume phase transition temperature  $T_c$ , TR gels swell noticeably. When  $T$  exceeds the critical temperature, these gels shrink [1]. Equilibrium and transient swelling of TR

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gels has recently become a focus of attention due to a wide range of industrial and biomedical applications of these materials [2, 3, 4].

Poly(*N*-isopropylacrylamide) (PNIPA) is one of the most extensively studied TR gels that exhibits a sharp volume phase transition at temperatures in the vicinity of  $T_c = 32$  to  $34$  °C accompanied by good mechanical properties below and above  $T_c$  and a fast response to changes in temperature [5]. Applications of TR hydrogels in the biomedical field [6], for DNA and proteins electrophoretic separation [7] and manufacture of temperature-triggered actuators [8] require modulation of the volume phase transition temperature  $T_c$  in a rather wide interval. Preparation of TR gels with tunable volume phase transition temperatures has been analyzed in a number of studies [9-13]. It is found that (i)  $T_c$  is practically unaffected by molar fractions of monomers and cross-linkers and preparation conditions (temperature at which cross-linking polymerization is performed and solvent for synthesis), (ii) it changes weakly with addition of polymer chains into a pre-gel solution to form semi-interpenetrating polymer networks, and (iii)  $T_c$  changes pronouncedly when TR monomers are mixed with relatively small amounts of monomers whose hydrophilicity differs from that of the basic monomers.

Although the qualitative trend in alternation of  $T_c$  is clear: the volume phase transition temperature decreases under insertion of hydrophobic monomers and increases when hydrophilic monomers are incorporated, no explicit relations have been proposed for the quantitative description of this phenomenon. The aim of this study is to develop a constitutive model able to predict changes in  $T_c$  with molar fraction of comonomers  $\psi$  in TR gels.

Experimental and theoretical studies on water uptake by TR gels have been initiated about 40 years ago [14, 15]. Changes in the equilibrium degree of swelling  $Q$  with temperature  $T$  are conventionally described within the Flory-Rehner theory, where the Flory-Huggins (FH) parameter  $\chi$  is replaced with an "effective" coefficient  $\chi(T, \phi_n)$ , where  $\phi_n$  denotes volume fraction of polymer network. Evolution of the effective FH parameter with temperature is described by the equation

$$\chi = \chi_0(T) + \chi_1(T)\phi_n \quad (1)$$

where the coefficients  $\chi_0$  and  $\chi_1$  evolve linearly with  $T$  or  $T^{-1}$  [16, 17]. A constitutive framework for the analysis of solvent transport and the mechanical response of TR gels under three-dimensional deformations with finite strain grounded on Eq. (1) was developed in [18-22], see recent reviews [23, 24]. A phenomenological approach to the description of equilibrium swelling of TR gels based on the Landau theory of phase transition was proposed in [25, 26]. A model for equilibrium swelling of TR gels, where the Flory expression for the specific energy of interaction between monomers and solvent molecules was replaced with more sophisticated relations based on the double lattice concept, was developed in [27].

Although the models grounded on the Flory-Rehner concept reveal an acceptable agreement with observations in swelling tests (in particular, when higher order terms with respect to  $\phi_n$  are introduced into Eq. (1) [28]), they were criticized for two reasons. First, the coefficients in Eq. (1) (these parameters are expressed in terms of the specific enthalpy and specific entropy of a polymer network) that ensure good fit of experimental data adopt unrealistic values [29, 30]. Secondly, this concept implies that the shear modulus  $G$  evolves with volume fraction of polymer network  $\phi_n$  following the pattern

$$\frac{G(\phi_{n1})}{G(\phi_{n2})} = \left(\frac{\phi_{n2}}{\phi_{n1}}\right)^{\frac{1}{3}} \quad (2)$$

where  $\phi_{n1}$  and  $\phi_{n2}$  are volume fractions of polymer at temperatures  $T_1$  and  $T_2$ . Although Eq. (2) predicts adequately mechanical properties of swollen elastomers [31], substantial (by an order of magnitude) deviations from this law were reported in tensile tests on PNIPA gels [32-35]. A pronounced increase in the elastic modulus of TR gels  $T > T_c$  was recently observed by means of small-amplitude oscillatory shear tests in [36-40], see Fig. 1. For the purposes of this study (analysis of the volume phase transition temperature of copolymer gels), an important shortcoming of the models based on the Flory-Rehner theory is that they do not involve  $T_c$  explicitly, and, as a consequence, cannot predict how this quantity is affected by chemistry and molar fraction of comonomers.

To describe a strong decay in the equilibrium degree of swelling of a TR gel above  $T_c$  accompanied by a substantial growth of its shear modulus, we presume polymer chains in a network to be composited of hydrophilic and hydrophobic segments and adopt a concept of thermally-induced breakage of cages formed by water molecules around hydrophobic segments [41, 42], see also recent reviews [43, 44]. At temperatures below  $T_c$ , each hydrophobic segment is surrounded by a cage-like structure formed by water molecules bridged by hydrogen bonds [45]. When temperature grows, these clusters of water molecules are destabilized by thermal fluctuations. Their breakage induces agglomeration of hydrophobic segments and formation of aggregates from which water molecules are expelled. At temperatures above  $T_c$ , when cage-like structures are broken, a TR gel consists of a number of deswollen hydrophobic aggregates bridged by hydrophilic segments and separated by nano-channels in which water molecules are located [46].

The objective of this work is three-fold: (i) to derive a mean-field model for the elastic response and equilibrium swelling of TR gels that takes into account formation of physical bonds due to aggregation of hydrophobic segments above  $T_c$ , (ii) to determine adjustable parameters in the governing equations by fitting observations on several homo- and copolymer gels, and (iii) to derive a simple relation that expresses the volume phase transition temperature of copolymer gels  $T_c$  in terms of molar fraction of comonomers  $\psi$ .

The novelty of our study consists in treatment of the polymer network in a TR gel as a superposition of two networks: the first is formed under preparation when chains are chemically cross-linked, while the other is developed when temperature exceeds  $T_c$  and new physical bonds between chains arise due to aggregation of hydrophobic segments. These two networks have different reference (stress-free) states and different elastic moduli (the modulus of the network with covalent cross-links is temperature-independent, while that of the network with physical bonds increases with temperature).

Another approach to the analysis of swelling diagrams for stimuli-sensitive gels is grounded on ab initio calculations and Monte Carlo simulation of their deformation, see recent reviews [47, 48]. We do not apply these techniques as our purpose is to develop analytical expressions for the degree of swelling and volume phase transition temperature.

## 2. Model

A gel is modeled as a two-phase medium composed of solid (an equivalent polymer network) and fluid (water) constituents. The solid and fluid phases are treated as immiscible interpenetrating continua. The polymer network in a TR gel consists of two components. The first (covalent) network is formed under preparation when cross-linking polymerization of a pre-gel solution is conducted. The other (physical) network is formed at temperatures  $T > T_c$  due to aggregation of hydrophobic segments of chains. Both networks are treated as permanent. Their deformations obey the affinity hypothesis and the molecular incompressibility condition.

The initial configuration of a gel coincides with that of an undeformed dry specimen at some temperature  $T_0 < T_c$ . Transformation of the initial configuration into the reference (stress-free) configuration of the first (covalently cross-linked) network is described by the deformation gradient  $\mathbf{f}_1 = f_1^{\frac{1}{3}} \mathbf{I}$ , where  $\mathbf{I}$  is the unit tensor,  $f_1 = 1 + Q_0$  is a coefficient of inflation under transition from the initial to the reference configuration, and  $Q_0$  is the degree of swelling in the reference state. The reference state of the second network (with physical junctions) coincides with the initial state of the gel (all water molecules are expelled from hydrophobic clusters).

For definiteness, the neo-Hookean formulas are adopted for the strain energy densities of polymer networks with covalent and physical bonds

$$W_m = \frac{1}{2} G_m \left[ \left( I_{e1}^{(m)} - 3 \right) - \ln I_{3e}^{(m)} \right], \quad (m = 1, 2) \quad (3)$$

where  $G_m$  stands for the shear modulus of the  $m$ th network, and  $I_{e1}^{(m)}, I_{e2}^{(m)}, I_{e3}^{(m)}$  are the principal invariants of the Cauchy-Green tensors for elastic deformation. The physical meaning of these relations was discussed in [49], where Eq. (3) was derived within the concept of entropic elasticity. More sophisticated expressions for the functions  $W_m$  were developed and verified by comparison with observations in [50, 51].

The elastic modulus  $G_1$  of the covalently cross-linked network is presumed to be independent of temperature. The elastic modulus  $G_2$  of the network with physical junctions vanishes below  $T_c$  and grows with the difference  $T - T_c$  above the volume phase transition temperature following the pattern

$$G_2(T) = 0, \quad (T < T_c), \quad G_2(T) = \bar{G}_2 [1 - \exp(-\beta\sqrt{T - T_c})], \quad (T \geq T_c) \quad (4)$$

where  $\bar{G}_2$  and  $\beta$  are adjustable parameters. Eq. (4) differs from the equation for evolution of elastic modulus with temperature proposed in [52]. The ability of Eq. (4) to described observations is verified in Fig. 1, where experimental data in shear oscillatory tests on PNIPA gels are approximated by this relation with the material constants listed in Tab. S1.

The specific Helmholtz free energy (per unit volume of a gel in its initial configuration)  $\Psi$  equals the sum of the energies of phases not interacting with each other and the energy of their interaction,  $\Psi = \Psi_1 + \Psi_2 + \Psi_3$ , where  $\Psi_1$  is the specific energy of water molecules not interacting with the polymer network,  $\Psi_2$  is the specific energy of the polymer network not interacting with water, and  $\Psi_3$  is the specific energy of mixing of water molecules with segments of chains.

The specific energy of water reads  $\Psi_1 = \mu^0 C$ , where  $\mu^0$  denotes chemical potential of water molecules not interacting with the polymer network, and  $C$  stands for their concentration (number of molecules per unit volume in the initial state).

The specific energy of the polymer network (consisting of two parts with chemical and physical bonds) is given by  $\Psi_2 = \sum_{m=1}^2 W_m$ , where the specific mechanical energy stored in chains of the  $m$ th network  $W_m$  is given by Eq. (3).

The specific energy of mixing of water molecules with segments of polymer chains is accepted in the Flory-Huggins form

$$\phi_n \Psi_3 = \frac{k_B T_0}{v} (\phi_w \ln \phi_w + \chi \phi_w \phi_n), \quad (5)$$

where  $k_B$  is the Boltzmann constant,  $v$  is the characteristic volume of a water molecule,  $\chi$  is the effective Flory-Huggins parameter, and  $\phi_n, \phi_w$  are volume fractions of polymer and water molecules

$$\phi_n = \frac{1}{1 + C v}, \quad \phi_w = \frac{C v}{1 + C v}.$$

The coefficient  $\phi_n$  is introduced in the left-hand side of Eq. (5) because the right-hand side of this equation equals the specific energy of mixing per unit volume in the actual configuration.

The following expression is accepted for the effective Flory-Huggins parameter

$$\chi = \chi_0 + \chi_1 T \quad (T < T_c), \quad \chi = \chi_{max} \quad (T \geq T_c), \quad (6)$$

where  $T$  and  $T_c$  are measured in °C, and the material constants  $\chi_0, \chi_1, \chi_{max}$  obey the condition

$$\chi_{max} = \chi_0 + \chi_1 T_c. \quad (7)$$

Eq. (7) means that breakage of cages formed by water molecules around hydrophobic segments under heating of a gel induces an increase in  $\chi$  below  $T_c$ . When  $T$  exceeds the volume phase transition temperature  $T_c$ , further increase in  $\chi$  is prohibited by formation of aggregates of hydrophobic segments from which water molecules are expelled.

Under unconstrained equilibrium swelling of a TR gel, its degree of swelling  $Q = C v$  at an arbitrary temperature  $T$  obeys the nonlinear equation

$$\begin{aligned} \ln \frac{Q}{1+Q} + \frac{1}{1+Q} + \frac{\chi}{(1+Q)^2} + \frac{g_1}{1+Q} \left[ \left( \frac{1+Q}{1+Q_0} \right)^{\frac{2}{3}} - 1 \right] \\ + \frac{g_2}{1+Q} \left[ (1+Q)^{\frac{2}{3}} - 1 \right] = 0 \end{aligned} \quad (8)$$

where

$$g_m = \frac{G_m v}{k_B T_0} \quad (m = 1, 2)$$

are dimensionless elastic moduli. A detailed derivation of Eq. (8) is given in Supplementary Material.

Eq. (8) together with Eq. (6) for the effective Flory-Huggins parameter  $\chi$  and Eq. (4) for the elastic modulus  $g_2$  provide the governing equations for the equilibrium degree of swelling  $Q$ . These relations involve seven adjustable parameters: (i) coefficients  $\chi_0$  and  $\chi_1$  describe how hydrophilicity of chains is affected by temperature below the critical temperature  $T_c$ , (ii) parameter  $\chi_{max}$  characterizes their hydrophilicity above the volume phase transition temperature, (iii)  $g_1$  and  $Q_0$  stand for the dimensionless shear modulus of the covalently cross-linked network and its degree of swelling in the reference state, and (iv) coefficients  $\bar{g}_2$  and  $\beta$  describe an increase in the



dimensionless shear modulus of the network with physical bonds above  $T_c$ . The volume phase transition temperature  $T_c$  is calculated from Eq. (7).

### 3. Comparison with experimental data

To examine the ability of the model (4), (6) and (8) to describe experimental swelling diagrams, we focus on observations on poly(*N*-isopropylacrylamide) homopolymer and copolymer gels as these materials are widely used in biomedical applications [2].

In the conventional treatment of observations in swelling tests, the effective Flory-Huggins parameter  $\chi$  is thought of as an adjustable function of two variables  $T$  and  $\phi_n$ . Unlike this approach, we consider  $\chi$  as a material function of temperature  $T$  only. The dependence  $\chi(T)$  is found by fitting the equilibrium swelling diagram on a special gel prepared by  $\gamma$ -irradiation of an aqueous solution of PNIPA chains (this treatment excludes the effects of chemistry and concentration of cross-linker on the hydrophilicity of polymer chains). Afterwards, the "universal" coefficients  $\chi_0$  and  $\chi_1$  in Eq. (6) are fixed and used without changes for other hydrogels under investigation. This allows elastic moduli of the polymer networks with covalent and physical bonds to be determined with high accuracy.

For each set of observations, adjustable parameters are found by the nonlinear regression method to minimize the expression  $\sum(Q_{exp} - Q_{sim})^2$ , where summation is performed over all temperatures  $T$  under consideration,  $Q_{exp}$  stands for the degree of swelling measured in a test, and  $Q_{sim}$  is determined by Eq. (8), which is solved by means of the Newton-Raphson algorithm.

#### 3.1 The Flory-Huggins parameter

We begin with matching experimental data on PNIPA gel prepared by irradiation cross-linking of an aqueous solution of PNIPA chains with the irradiation dose  $I = 20$  kGy [53]. Observations in equilibrium water uptake tests are depicted in Fig. 2, where  $Q$  is plotted versus temperature  $T$ .

The swelling diagram in Fig. 2 is matched by means of a two-step procedure. At the first step, we approximate observations below  $T_c$  (where  $g_2 = 0$ ), set  $Q_0 = 12.81$  (which means that the reference state coincides with the as-prepared state [32]), determine  $\chi$  from Eq. (8), and fit the experimental dependence  $\chi(T)$  by means of Eq. (6), where  $\chi_0$  and  $\chi_1$  are calculated by the least-squares technique. The dimensionless elastic modulus  $g_1$  is found from the condition of the best-fit of the experimental function  $\chi(T)$  by linear Eq. (6). At the other step, the experimental data above  $T_c$  are matched with the help of two parameters,  $\beta$  and  $\bar{g}_2$  with  $\bar{g}_2 = \bar{G}_2 v / (k_B T_0)$ .



Fig. 2A demonstrates good agreement between the observations in equilibrium swelling tests and results of numerical simulation with the material constants collected in Tab. S2. Fig. 2B shows that the growth of  $\chi$  with temperature below  $T_c$  is described adequately by Eq. (6).

### 3.2 Copolymer gels

We approximate four sets of experimental data on PNIPA copolymer gels prepared with incorporation of hydrophobic and hydrophilic monomers.

We begin with the analysis of swelling diagrams on a homopolymer PNIPA gel and copolymer gels synthesized with addition of 4 mol.% of hydrophobic butyl methacrylate (BMA) and hydrophilic acrylamide (AAm) monomers [54]. The gels were prepared by cross-linking polymerization (18 h at 80 °C) of solutions of monomers in 1,4-dioxane (molar fraction  $m_{mon} = 0.884$  M) by using ethylene glycol dimethacrylate (EGDMA, molar fraction  $m_{cr} = 8.8$  mM) as a cross-linker.

First, we fit observations on homopolymer PNIPA gel (Fig. 3A) by using the coefficients  $\chi_0$  and  $\chi_1$  reported in Tab. S2, and find  $g_1$  and  $Q_0$  from the best-fit condition for the dependence  $\chi(T)$  below  $T_c$ . The coefficient  $\chi_{max}$  is determined from measurements of  $T_c$ , and the parameters  $\beta$  and  $\bar{g}_2$  are found by matching the experimental swelling diagram above  $T_c$ .

We proceed with fitting experimental data on PNIPA-BMA (Fig. 3B) and PNIPA-AAm (Fig. 3C) copolymer gels. As molar fractions of hydrophobic and hydrophilic comonomers are low, we disregard their influence on the degree of swelling in the reference state  $Q_0$  and the elastic modulus of the covalently cross-linked network  $g_1$ . For each set of observations, we calculate  $\chi_0$  and  $\chi_1$  by matching the dependence  $\chi(T)$  below  $T_c$  (using  $Q_0$  and  $g_1$  determined in fitting observations on the homopolymer gel), find  $\chi_{max}$  from measurement of  $T_c$ , and determine  $\beta$  and  $\bar{g}_2$  by matching the equilibrium swelling curve above  $T_c$ . The best-fit material constants are listed in Tab. S3.

We now approximate observations on double-network semi-interpenetrating PNIPA gels prepared in aqueous solutions of poly(*N*-vinylpyrrolidone) (PVP, molecular weight  $M_w = 1.3 \cdot 10^6$  g/mol) with various mass fractions of PVP chains  $\psi$  ranging from 0 to 3 wt.%. The hydrogels were prepared by cross-linking polymerization (24 h at 4 °C) of NIPA monomers (molar fraction  $m_{mon} = 0.885$  M) by using *N,N'*-methylenebisacrylamide (BIS,  $m_{cr} = 35.4$  mM) as a cross-linker [55]. Equilibrium swelling diagrams on gels with the lowest ( $\psi = 0$ ) and highest ( $\psi = 3$  wt.%) mass fractions of PVP chains are depicted in Figs. 4A and 4B together with results of numerical simulation, and those on gels with intermediate  $\psi$  values ( $\psi = 1$  and 2 wt.%) are presented in Figs. S1A and S1B.

Material parameters are determined by means of the same procedure that is used to fit observations in Fig. 3. We begin with the swelling diagram on homopolymer PNIPA gel, find  $g_1$  and  $Q_0$  by matching observations below  $T_c$  with the "universal" coefficients  $\chi_0$  and  $\chi_1$ , determine  $\chi_{max}$

from measurements of  $T_c$ , and calculate  $\beta$  and  $\bar{g}_2$  by fitting data above  $T_c$ . Afterwards, experimental data on the double-network hydrogels with various  $\psi$  are approximated by using the same algorithm with the fixed values of  $g_1$  and  $Q_0$ . Each set of observations is matched separately.

The coefficients  $g_1, Q_0, \chi_{max}$  and  $\beta$  are found to be independent of  $\psi$ . Their values are listed in Tab. S4. The remaining parameters,  $\chi_0, \chi_1$  and  $\bar{g}_2$ , are affected by mass fraction  $\psi$  of PVP chains in pre-gel solutions. Evolution of these quantities with  $\psi$  is illustrated in Fig. S1C, where the data are approximated by the relations

$$\chi_0 = \chi_0^0 - \psi \chi_0^1, \quad \chi_1 = \chi_1^0 + \psi \chi_1^1, \quad \log \bar{g}_2 = \log \bar{g}_2^0 - \psi \log \bar{g}_2^1 \quad (9)$$

with the coefficients calculated by the least-squares technique.

We proceed with fitting experimental data on PNIPA-*N,N'*-dimethyl aminoethyl methacrylate (DMAEMA) copolymer gels with mass fractions of DMAEMA monomers (with respect to NIPA)  $\psi = 0, 0.1$  and  $0.2$ . The hydrogels were synthesized by free-radical cross-linking polymerization (at  $80^\circ\text{C}$ ) of solutions of monomers in 1,4-dioxane (molar fraction of NIPA monomers  $m_{mon} = 2.68$  M) by using BIS as a cross-linker (molar fraction  $m_{cr} = 53.6$  mM) [56]. The experimental swelling diagrams on gels with the lowest ( $\psi = 0$ ) and highest ( $\psi = 0.2$ ) mass fractions of comonomers are depicted in Figs. 5A and 5B, and that on the gel with  $\psi = 0.1$  is presented in Fig. S2A. Each curve is matched separately by means of the same procedure that is used to fit experimental data in Figs. 3 and 4.

The best-fit coefficients  $g_1, Q_0, \chi_{max}$  and  $\beta$  are independent of  $\psi$ . Their values are listed in Tab. S5. The effect of  $\psi$  on parameters  $\chi_0, \chi_1$  and  $\bar{g}_2$  is illustrated in Fig. S2B, where the data are approximated by Eq. (9).

Finally, we match experimental data on PNIPA-acrylamide (AAM) graft copolymer gels with various mass fractions of AAM monomers (with respect to NIPA)  $\psi = 0, 0.2, 0.35$  and  $0.5$ . The gels were prepared by cross-linking polymerization (4 h at  $4^\circ\text{C}$ ) of aqueous solutions of NIPA (molar fraction  $m_{mon} = 0.74$  M) and AAM monomers by using BIS (molar fraction  $m_{cr} = 54$  mM) as a cross-linker [57]. Experimental data in equilibrium swelling tests on gels with the lowest ( $\psi = 0$ ) and highest ( $\psi = 0.5$ ) mass fractions of AAM monomers are presented in Figs. 6A and 6B. The other two sets of observations on gels with  $\psi = 0.2$  and  $0.35$  are reported in Figs. S3A and S3B. Each swelling diagram is fitted separately with the help of the same algorithm that is used to approximate observations in Figs. 3 to 5.

The best-fit material constants  $g_1, Q_0, \chi_{max}$  and  $\beta$  are collected in Tab. S6. Evolution of parameters  $\chi_0, \chi_1$  and  $\bar{g}_2$  with mass fraction of comonomers  $\psi$  is demonstrated in Fig. S3C, where the data are approximated by Eq. (9).

The following conclusions are drawn from Figs. 3 to 6:

(I) Incorporation of hydrophobic monomers induces a reduction in the volume phase transition temperature of copolymer gels, whereas addition of hydrophilic monomers into a pre-gel solution causes an increase in  $T_c$ .

(II) The shift of the critical temperature is explained by changes in hydrophilicity of polymer chains described by evolution of the coefficients  $\chi_0$  and  $\chi_1$  with molar fraction of comonomers  $\psi$ .

(III) When hydrophilic comonomers are added into a pre-gel solution, the coefficient  $\chi_0$  decreases strongly with  $\psi$ , while the coefficient  $\chi_1$  increases weakly. According to the thermodynamic theory of mixtures [17], these changes reflect the growth of the entropic and enthalpic components of the energy of interactions between water molecules and segments of chains.

(IV) Evolution of parameters  $\chi_0$  and  $\chi_1$  with  $\psi$  is accompanied by a reduction in the shear modulus  $\bar{g}_2$  of the polymer network with physical bonds. This decrease may be explained by a decay (caused by the presence of hydrophilic segments) in the number of hydrophobic aggregates served as physical junctions between chains above the volume phase transition temperature.

### 3.3 Homopolymer gels

Figs. 3 to 6 show that inclusion of hydrophilic and hydrophobic monomers under polymerization affects strongly equilibrium swelling diagrams of PNIPA gels (below and above  $T_c$ ) and leads to noticeable shifts of the volume phase transition temperature. Our aim now is to demonstrate that modification of the preparation conditions for homopolymer gels induces substantial changes in their equilibrium degree of swelling, but does not affect the critical temperature  $T_c$ . For this purpose, two sets of experimental data are analyzed.

First, observations in equilibrium swelling tests are fitted on PNIPA gels prepared in aqueous solutions of sucrose with various concentrations  $\psi$  ranging from 0 to 1.5 M. The hydrogels were synthesized by free radical cross-linking polymerization (24 h at 20 °C) of NIPA monomers (molar fraction  $m_{mon} = 0.59$  M) in aqueous solutions of sucrose by using BIS (molar fraction  $m_{cr} = 21.6$  mM) as a cross-linker [58]. Experimental swelling diagrams together with results of simulation are reported in Fig. 7.

Each set of data in Fig. 7 is matched separately by means of the following algorithm. Keeping in mind that polymer chains contain only NIPA monomers and molar fraction of cross-linker is low, we adopt the "universal" values of  $\chi_0$  and  $\chi_1$  found by fitting data in Fig. 2. Coefficients  $g_1$  and  $Q_0$  are calculated by matching experimental data below the volume phase transition temperature,  $T_c$  is measured in the swelling test, and parameters  $\bar{g}_2$  and  $\beta$  are determined by approximation of observations above  $T_c$ .

Material parameters  $\chi_0, \chi_1, \chi_{max}$  and  $\beta$  are independent of molar fraction of sucrose in aqueous solutions  $\psi$ . Their best-fit values are listed in Tab. S7. The effect of  $\psi$  on parameters  $g_1, \bar{g}_2$  and  $Q_0$  is illustrated in Fig. S4. The data are approximated by the phenomenological equations

$$\begin{aligned} \log g_1 &= \log g_1^0 + \psi \log g_1^1, & \log \bar{g}_2 &= \log \bar{g}_2^0 - \psi \log \bar{g}_2^1, \\ Q_0^{-1} &= q^0 - \psi q^1, \end{aligned} \quad (10)$$

where the coefficients are determined by the least-squares method.

We proceed with the analysis of equilibrium swelling diagrams on nanocomposite PNIPA cryogels with various mass fractions  $\psi$  of colloidal silica particles (Ludox AS-40, average diameter 20 nm) with  $\psi$  ranging from 0 to 0.35. The gels were prepared by cross-linking polymerization (24 h at 15 °C at the first stage and -18 °C at the other stage) of NIPA monomers (molar fraction  $m_{mon} = 0.97$  M) in aqueous dispersions of SiO<sub>2</sub> nanoparticles by using BIS (molar fraction  $m_{cr} = 15$  mM) as a cross-linker [59].

Observations in equilibrium swelling tests on the nanocomposite gels are reported in Fig. 8 together with results of simulation. Each swelling curve is matched separately by applying the same approach that is used to approximate experimental data in Fig. 7. The best-fit values of material parameters  $\chi_0, \chi_1, \chi_{max}$  and  $\beta$  are listed in Tab. S8. The effect of mass fraction  $\psi$  on silica nanoparticles on  $g_1, \bar{g}_2$  and  $Q_0$  is illustrated in Fig. S5, where the data are approximated by Eq. (10).

The following conclusions are drawn from Figs. 7 and 8:

- (i) Synthesis of PNIPA gels in aqueous solutions of sucrose and dispersions of colloidal particles does not induce changes in the volume phase transition temperature  $T_c$ , but affects strongly their mechanical properties, and, as a consequence, degree of swelling.
- (ii) Addition of sucrose to a pre-gel solution results in a pronounced reduction of the shear modulus  $g_1$  of the covalently cross-linked network, whereas insertion of nanoparticles induces a strong increase in  $g_1$ . The decay in  $g_1$  with  $\psi$  in sucrose solutions can be explained by collapse of PNIPA chains at high concentrations of sucrose [58] that leads to a decrease in the number of cross-links formed under preparation. The growth of  $g_1$  with  $\psi$  in silica dispersions reflects stiffening of nanocomposite hydrogels due to the presence of filler.
- (III) Dissolution of sucrose as well as dispersion of silica nanoparticles in a pre-gel solution induce a substantial decrease in the elastic modulus  $\bar{g}_2$  of the polymer network developed above the critical temperature  $T_c$ . This conclusion is explained by the growth of porosity of gels [58, 59] treated as an increase in the characteristic distance between segments of neighboring chains. The latter results in a reduction in concentration of aggregates formed by hydrophobic segments above the volume phase transition temperature, which, in turn, is proportional to  $\bar{g}_2$ .

(IV) The growth of  $\psi$  causes an increase in the degree of swelling  $Q_0$  in the reference (stress-free) state of the gels. This growth is strong for gels prepared in aqueous solutions of sucrose (due to the collapse of polymer chains) and becomes negligible for nanocomposite gels.

### 3.4 Discussion

Figs. 2 to 8 demonstrate good agreement between experimental data on homo- and copolymer hydrogels and results of numerical simulation. This confirms the ability of the model to describe observations in equilibrium swelling tests on thermo-responsive gels.

Unlike the conventional models that require very high values of the Flory-Huggins parameter  $\chi$  to ensure good quality of fitting, the coefficient  $\chi_{max}$  adopts reasonable values in the interval between 0.46 and 0.62 for all hydrogels under consideration, see Tabs. S2 to S8.

Figs. S2B, S3C, S4 and S5 show that adjustable parameters found by fitting experimental data change consistently with concentrations of comonomers and mass fractions of additives in pre-gel solutions. Their evolution with  $\psi$  is described adequately by phenomenological Eqs. (9) and (10). However, some scatter of the experimental data should be mentioned that may be ascribed to inaccuracies of measurements.

To assess how these inaccuracies affect the quality of prediction by the model, we calculate the volume phase transition of copolymer gels  $T_c$  as a function of concentration of hydrophilic monomers  $\psi$ . It follows from Eqs. (7) and (9) that

$$T_c = \frac{\chi_{max} - \chi_0^0 + \psi\chi_0^1}{\chi_1^0 + \psi\chi_1^1} . \quad (11)$$

We calculate  $T_c$  for PNIPA-PVP, PNIPA-DMAEMA and PNIPA-AAm copolymer gels by means of Eq. (11) (the coefficients in the right-hand side are taken from Figs. S1C, S2B and S3C) and plot the results together with experimental data in Figs. 4C, 5C and 6C, respectively. These figures show the ability of the model not only to describe experimental data in equilibrium swelling tests, but also to predict the effect of comonomers on the volume phase transition temperature.

### 4 Conclusions

A model is developed for the mechanical response and equilibrium swelling of thermo-responsive gels. Unlike conventional approaches grounded on the Flory-Rehner concept, our model accounts for a pronounced increase in the elastic modulus above the volume phase transition temperature observed in monotonic tensile tests and shear oscillatory tests. Its material parameters adopt

physically reasonable values (in particular, the Flory-Huggins parameter  $\chi$  does not exceed 0.62 for all hydrogels under investigation).

Polymer chains in a thermo-response gel are presumed to involve hydrophilic and hydrophobic segments. Below the volume phase transition temperature  $T_c$ , each hydrophobic segment is surrounded by a cage-like structure formed by water molecules bridged by hydrogen bonds. With an increase in temperature, thermal fluctuations induce breakage of these structures accompanied by aggregation of hydrophobic segments and formation of clusters from which water molecules are expelled. Above  $T_c$ , when most cage-like structures are broken, a gel consists of a number of deswollen hydrophobic aggregates bridged by hydrophilic segments and separated by nano-channels in which water molecules are located. With reference to this scenario, constitutive equations for an arbitrary three-dimensional deformation of a thermo-responsive hydrogel are derived by means of the free energy imbalance inequality.

The governing equations for equilibrium swelling of a hydrogel involve seven material parameters with transparent physical meaning: (i) coefficients  $\chi_0$  and  $\chi_1$  describe how hydrophilicity of chains is affected by temperature below  $T_c$ , (ii) parameter  $\chi_{max}$  characterizes their hydrophilicity at and above  $T_c$ , (iii)  $g_1$  and  $Q_0$  stand for the shear modulus of the covalently cross-linked network and its degree of swelling in the reference state, and (iv) coefficients  $\bar{g}_2$  and  $\beta$  characterize an increase in the shear modulus of polymer chains bridged by deswollen hydrophobic aggregates above  $T_c$ . These quantities are found by matching experimental swelling diagrams on homopolymer PNIPa gels cross-linked by  $\gamma$ -radiation, covalently cross-linked in water, 1,4-dioxane, aqueous sucrose solution and dispersion of silica colloidal particles, as well as on copolymer PNIPa-BMA, PNIPa-PVP, PNIPa-DMAEMA and PNIPa-AAm gels. Figs. 2 to 8 demonstrate good agreement between the experimental data and results of numerical simulation.

An analytical formula, Eq. (11), is derived for the volume phase transition temperature of copolymer gels. Figs. 4C, 5C and 6C confirms the ability of the model to predict the effect of concentration of monomers on  $T_c$ .

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### List of figures

Figure 1: The ratio of storage moduli  $R = G'(T)/G'(T_0)$  with  $T_0 = 22\text{ }^{\circ}\text{C}$  versus temperature  $T$ . Circles: experimental data on PNIPA gels in shear oscillatory tests. Solid lines: results of simulation. A – [36], B – [40].

Figure 2: A - Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [53] on PNIPA gel prepared by irradiation of polymer solution. Solid line: results of simulation. B - Parameter  $\chi$  versus temperature  $T$ . Circles: treatment of observations. Solid line: approximation of the data by Eq. (6).

Figure 3: Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [54]. Solid lines: results of simulation. A - PNIPA gel, B - PNIPA-BMA gel, C - PNIPA-AAm gel.

Figure 4: A, B - Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [55] on interpenetrating PNIPA-PVP gels with various mass fractions  $\psi$  of PVP (A -  $\psi = 0$ , B -  $\psi = 3$  wt.%). Solid lines: results of simulation. C - Volume phase transition temperature  $T_c$  versus mass fraction  $\psi$  of PVP. Circles: treatment of observations. Solid line: prediction of the model.

Figure 5: A, B - Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [56] on PNIPA-DMAEMA gels with various mass fractions  $\psi$  of DMAEMA monomers (A -  $\psi = 0$ , B -  $\psi = 0.2$ ). Solid lines: results of simulation. C - Volume phase transition temperature  $T_c$  versus mass fractions  $\psi$  of DMAEMA monomers. Circles: treatment of observations. Solid line: prediction of the model.

Figure 6: A, B - Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [57] on PNIPA-AAm gels with various molar fractions  $\psi$  of AAm monomers. (A -  $\psi = 0$ , B -  $\psi = 0.5$ ). Solid lines: results of simulation. C - Volume phase transition temperature  $T_c$  versus molar fraction  $\psi$  of AAm monomers. Circles: treatment of observations. Solid line: prediction of the model.

Figure 7: Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [58] on PNIPA gels prepared in aqueous solutions of sucrose with various concentrations  $\psi$  (A -  $\psi = 0$ , B -  $\psi = 0.5$ , C -  $\psi = 1.0$ , D -  $\psi = 1.5$  M). Solid lines: results of simulation.

Figure 8: Degree of swelling  $Q$  versus temperature  $T$ . Circles: experimental data [59] on PNIPA gels reinforced with various mass fractions  $\psi$  of silica nanoparticles (A -  $\psi = 0$ , B -  $\psi = 5$ , C -  $\psi = 21$ , D -  $\psi = 35$  wt.%). Solid lines: results of simulation.

















