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Moesgaard, Mette; Yue, Yuanzheng

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# GLASS FORMING ABILITY OF CALCIUM **ALUMINOSILICATE MELTS**

# M. Moesgaard, Y. Yue

Section for Chemistry, Aalborg University, Sohngaardsholmsvej 57 DK-9000 Aalborg, Denmark e-mail: min@bio.aau.dk

described in terms of glass stability, i.e. the ability of a glass to resist crystallization during heating. In addition, the fragility index (m) is derived by fitting the viscosity data with the of compositions. The eutectic composition of anorthite-wollastonite-tridymite is found to However, this proportionality is only valid for comparison of the glasses in the same series stability for the two series of melts, implying that m is an indirect measure of GFA Avramov-Milchev equation. The results show that m is inversely proportional to the glass line parallel to the joining line on the alumina rich side. In the present work, GFA is eutectic compositions as end members. The second series consists of five compositions on a wollastonite-tridymite and that of anorthite-wollastonite-gehlenite. The series includes the consists of five compositions on the joining line between the cutectic point of anorthite studied by measuring their viscous behavior and crystallization tendency. The first series exhibit the highest GFA of the melts under investigation. The glass forming ability (GFA) of two series of calcium aluminosilicate melts is

Keywords: Calcium aluminosilicates, viscosity, fragility, glass stability, glass forming

of special interest for glass scientists to seek alternative methods for determining determination of the critical cooling rate is not always an easy task. Therefore it is crystallization. The critical cooling rate is the minimum rate required to vitrify a melt. This rate can be considered as a direct measure of GFA [1,2]. However, melt can be made glassy if the quenching process is sufficiently fast to avoid the glass forming ability (GFA) of a given melt. From a kinetic point of view, any predominant way for producing inorganic glasses is still the melt-quench process vapor deposition, solid-state reactions and sol-gel methods. However, the To optimize this process for producing high quality glasses, it is essential to know Nowadays inorganic glasses can be made in many ways, e.g. by chemical

upon reheating. This stability refers to the ability of a glass to bypass crystallization aluminosilicate (CAS) melts by determining the stability of the formed glasses The objectives of this work are to define and quantify GFA of ten calcium

> melting temperature. upon nearing, in this work the Hruby parameter ( $x_{\rm H}$ ) obtained from calorimetric data is used as a measure of glass stability (Eq. 1) [3]. In Eq. 1  $T_{\rm g}$  is the glass transition temperature,  $T_e$  the onset temperature of crystallization, and  $T_m$  the

$$K_{II} = \frac{T_c - T_g}{T_m - T_c} \tag{1}$$

used as a measure of GFA of a melt upon cooling [3-5]. inverse linear relation is found between  $K_H$  and the critical cooling rate,  $K_H$  may be The larger the parameter  $K_{Ib}$  the higher is the glass stability. Since an

and described by the Avramov-Milchev (AM) equation: The temperature (T) dependences of viscosity  $(\eta)$  are measured using viscometry

$$\log \eta = \log \eta_{\infty} + \left(12 - \log \eta_{\infty}\right) \left(\frac{T_{g}}{T}\right)^{r} \tag{2}$$

where  $\eta_x$  is the viscosity at infinite high temperature, and F is the fragility index

definition of m, F can be linked to m in the following manner [15]: slope of the fragility plot, i.e. the logy versus  $T_g/T$  plot, at  $T_g$ . From Eq. (2) and the and co-workers [13,14] have proposed another fragility index (m) defined as the In addition to the fragility parameter F derived from the AM equation, Angell

$$m = (12 - \log \eta_{\infty})F. \tag{3}$$

anorthite-wollastonite-gehlenite with the two cutectic compositions being the end work. The eutectic series (CAS1 to -5) is positioned on the joining line connecting alternative measure of GFA for those systems. Now the question is whether this is increasing values of NBO/T. An inverse correlation between fragility and GFA has the two eutectic compositions of anorthite-wollastonite-tridymite (An-Wo-Tri) and the Hrüby parameter and the fragility of two series of CAS glass compositions. the case for the CAS system. In this work we clarify this question by determining been found for various metallic glasses [7-9], and hence, fragility can be used as an consideration. In general  $\log p_{\omega}$  is for the ten melts observed to decrease with Iwo series of five compositions each were synthesized and investigated in this It is noticed that for determining m the parameter  $\log \eta_{\infty}$  is taken into

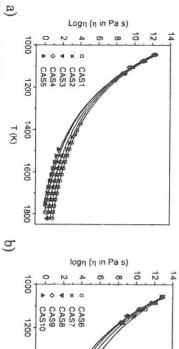
members. The non-eutectic series (CAS6 to -10) is positioned parallel to the

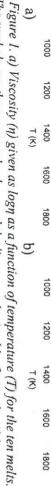
eutectic series at larger alumina concentrations. The chemical compositions are seen in Table 1. The table also states the number of non-bridging oxygen per tetrahedron (NBO/T) for each glass.

Table. 1: The compositions (in mol%) of the 10 CAS melts found by means of wet chemistry.

		SiO2	Al <sub>2</sub> O <sub>3</sub>	CaO	NBO/T
	CASI	64.9	9.3	25.8	0.40
Entactic	CAS2	59.9	10.0	30.1	0.50
ceries	CAS3	54.7	10.9	34.4	0.62
301103	CAS4	49.6	11.7	38.7	0.74
	CAS5	44.4	12.5	43.1	0.88
	CAS6	61.6	14.9	23.4	0.17
Non-	CAS7	57.8	15.8	26.3	0.23
eutectic	CAS8	51.9	16.8	31.3	0.30
series	CAS9	48.1	18.9	33.0	0.37
	CAS10	42.7	19.3	38.0	0.44

In the low viscosity range (approx.  $10^{\circ}$ - $10^{3}$  Pa s) the viscosity was measured using concentric cylinder viscometry, and in the high viscosity range (approx.  $10^{8}$ - $10^{13}$  Pa s) the viscosity was measured by means of micro penetration viscometry using a vertical dilatometer.  $T_{\rm g}$  and  $T_{\rm c}$  were measured using differential scanning calorimetry (DSC) by heating the samples up to 1723 K at a heating rate of 20 K/min. The heat capacity curves were obtained using the evaluation method described in [10,11]. Further details about the experimental work including the production process of the ten glasses can be found in [12].





The symbols are the measured values and the lines are obtained by fitting the AM equation

to the viscosity data.

Figs. 1a and b show the obtained viscosity data as well as the fit of the equation (Eq. (2)) to the data. From the figure it is observed that the AM exprovides a rather good description of the data ( $R^2 > 0.999$ ). Figure obtained from the AM fit and m is found using Eq. 3 (Table 2). As expect silicate melts the fragility increases with increasing NBO/T within each segmentation of the melt composition.

Table 2. Properties of the 10 CAS melts. F is obtained from fits of the AM equiviscosity data, m is found from Eq. 3.  $T_g$  and  $T_c$  are found from DSC using a heating 20 K/min.  $T_m$  is found using the model proposed by [16] and  $K_H$  is the Hrubÿ padefined in Eq. 1.

	series CAS9	eutectic CAS8	Non- CAS7	CAS6	CAS5	series CAS4	c CAS3	Eutecti CAS2	CASI	
$3.4 \pm 0.2$	$3.69 \pm 0.09$	$3.6 \pm 0.3$	$3.2 \pm 0.1$	$2.9 \pm 0.2$	$3.8 \pm 0.2$	$3.8 \pm 0.1$	$3.7 \pm 0.1$	$3.7 \pm 0.1$	$3.74 \pm 0.05$	F(-)
$49 \pm 3$	$51 \pm 1$	48 ± 4	44 ± 1	40 ± 3	53 ± 3	52 ± 1	50 ± 1	48±1	$47.5 \pm 0.6$	m (-)
1095	1096	1080	1091	1106	1068	1064	1063	1062	1070	$T_g$ '(K)
1347	1332	1320	1330	1379	1341	1336	1344			$T_c(K)$
1702	1693	1682	1666	1646	1538	1562	1554	1543	1443	$T_m(K)$

Figs. 2a and b depict the temperature dependence of isobaric heat  $c_p$  obtained for the glasses in the eutectic and non-eutectic series, respective seen that no crystallization is observed for CAS1 and -2.

 $T_{\rm g}$  and  $T_{\rm c}$  are found from the calorimetric measurements (Table 2) estimated based on the model proposed in [16]. This model assumes that close to the temperature at which the first crystal forms during cooling of From these characteristic temperatures  $K_{\rm H}$  is calculated using Eq. 1 (see Table 2).

As DSC is a dynamic method, the characteristic temperatures of the transitions are dependent on the heating rate employed during the measur. Thus, the values obtained for  $K_{\rm H}$  depend on the heating rate. This dependence rise to difficulties in obtaining  $K_{\rm H}$  of stable glasses having a low tende crystallize. This is due to the fact that crystallization can be bypassed when glasses are heated at a normal rate of e.g. 20 K/min. Therefore,  $T_{\rm c}$  is not determined thence  $K_{\rm H}$  can not be determined. This behavior is observed for CAS1 and

Thus,  $K_{\rm H}$  may only be used for quantifying the GFA of glasses with a relative high tendency to crystallize.

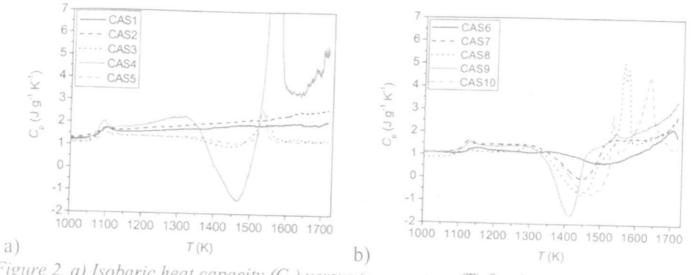


Figure 2. a) Isobaric heat capacity  $(C_p)$  versus temperature (T) for the ten glasses. All DSC measurements were carried out in atmospheric air at a heating rate of 20K/min.

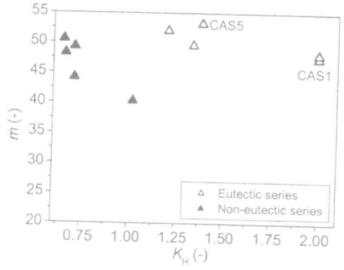


Figure 3. The fragility index (m) as a function of the Hrubÿ parameter  $(K_H)$  for the ten compositions.

To test whether the inverse correlation between fragility and  $K_{\rm H}$  exists for the CAS melts examined in this work the values of m and  $K_{\rm H}$  are compared in Fig 3. Within each series, m is observed to decrease with  $K_{\rm H}$ . This trend is most obvious for the non-eutectic series. For CAS1 and -2,  $K_{\rm H}$  is set to be 2 to reflect the highest stability of these two glasses upon reheating [3]. Therefore it can be stated that an inverse correlation between fragility and GFA exists within a series of CAS melts with systematic compositional variations.

## Conclusions

In summary, GFA of ten CAS melts has been quantified by the glass stability, while the fragility of these melts has been determined by fitting the AM

the five eutectic compositions exhibit higher GFA than the five non-eutectic ones. variations. In detail, the stronger the glass melt, the higher is its GFA. In overall, equation to viscosity data. An inverse correlation between fragility and GFA is found for the same series of peralkaline CAS melts with systematic compositional CAS1 possesses the highest GFA of the ten melts.

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