

Separation of Long-Crested Nonlinear Bichromatic Waves into Incident and Reflected Components

Andersen, Thomas Lykke; Eldrup, Mads Røge; Clavero, Maria

Published in:
Journal of Marine Science and Engineering

DOI (link to publication from Publisher):
[10.3390/jmse7020039](https://doi.org/10.3390/jmse7020039)

Creative Commons License
CC BY 4.0

Publication date:
2019

Document Version
Publisher's PDF, also known as Version of record

[Link to publication from Aalborg University](#)

Citation for published version (APA):
Andersen, T. L., Eldrup, M. R., & Clavero, M. (2019). Separation of Long-Crested Nonlinear Bichromatic Waves into Incident and Reflected Components. *Journal of Marine Science and Engineering*, 7(2), Article 39.
<https://doi.org/10.3390/jmse7020039>

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal -

Take down policy

If you believe that this document breaches copyright please contact us at vbn@aub.aau.dk providing details, and we will remove access to the work immediately and investigate your claim.

Separation of Long-Crested Nonlinear Bichromatic Waves into Incident and Reflected Components

Thomas Lykke Andersen^{1,*}, Mads R. Eldrup¹ and Maria Clavero²

¹ Department of Civil Engineering, Aalborg University, 9220 Aalborg Ø, Denmark; mre@civil.aau.dk

² Instituto Interuniversitario de Investigación del Sistema Tierra (IISTA), Universidad de Granada, Avda. del Mediterráneo s/n, 18006 Granada, Spain, mclavero@ugr.es

* Correspondence: tla@civil.aau.dk; Tel.: +45-9940-8486

Received: 11 December 2018; Accepted: 31 January 2019; Published: 7 February 2019

Abstract: Methods for the separation of long-crested linear waves into incident and reflected waves have existed for more than 40 years. The present paper presents a new method for the separation of nonlinear bichromatic long-crested waves into incident and reflected components, as well as into free and bound components. The new method is an extension of a recently proposed method for the separation of nonlinear regular waves. The new methods include both bound and free higher harmonics, which is important for nonlinear waves. The applied separation method covers interactions to the third order, but can easily be extended to a higher orders. Synthetic tests, as well as physical model tests, showed that the method accurately predict the bound amplitudes and incident and reflected surface elevations of nonlinear bichromatic waves. The new method is important in order to be able to describe the detailed characteristics of nonlinear bichromatic waves and their reflection.

Keywords: bichromatic waves; reflection separation; bound waves; nonlinear waves

1. Introduction

In physical model tests, it is very important to know in detail the wave conditions that are present in the facility. Incident waves hit passive or active absorbers or structures and are partly absorbed and partly reflected. Thereafter, the wave system includes both incident and reflected components. Nonlinear waves might at a given frequency include both bound and free components, making the separation into incident and reflected components more complicated. In regular or bichromatic waves, free incident higher harmonics are usually unwanted, as they mainly exist if the bound components were not correctly generated by the wave maker. Moreover, in regular and bichromatic waves, the bound harmonics at a given frequency usually stem from only one interaction. In irregular waves, this is not the case, and moreover, for wider spectra the primary energy overlaps with the sub- and superharmonics. If the wave height decreases, for example due to wave-breaking or waves propagating into deeper waters, the generation of free harmonics might also occur.

The present paper presents a detailed analysis of two-dimensional model tests with unidirectional bichromatic waves. Bichromatic waves are commonly used for detailed studies on the effect of bound sub- and superharmonics on, for example, the response of beaches and structures. Therefore, being able to accurately separate these waves into incident and reflected as well as bound and free components is of high interest.

Historically, waves have been separated into incident and reflected components based on methods assuming linear waves, cf. Goda and Suzuki [1], Mansard, and Funke [2], and Zelt and Skjelbreia [3]. Today, these methods are standard tools used in most hydraulic laboratories, but these methods do not consider any bound components to be present and also disregard amplitude

dispersion. The few existing methods for nonlinear waves use questionable assumptions, e.g., the Lin and Huang [4] method, which applies to regular waves but disregards amplitude dispersion and thus is only applicable to mildly nonlinear regular waves. The nonlinear LASA methods (Local Approximation using Simulated Annealing) by Figueres et al. [5] and Figueres and Medina [6] are based on local time domain solutions fitted to theoretical wave profiles, making application of their method to cases where free energy exists questionable. Even when no free energy exists and even for linear waves, Lykke Andersen et al. [7] and Eldrup and Lykke Andersen [8] found that the LASA V method was not accurate, and as the method at the same time is computationally very expensive, it is not practical for real applications.

Recently, a nonlinear frequency domain method to separate regular waves into incident and reflected components was developed, cf. Lykke Andersen et al. [7]. This method is an extension of the Lin and Huang [4] method, but includes amplitude dispersion based on stream function wave theory (Fenton and Rienecker [9]). This nonlinear separation method was further extended by Eldrup and Lykke Andersen [8] to irregular waves by utilizing a narrow-band assumption for the primary spectrum. They showed that even for typical single-peaked primary spectra (JONSWAP with $\gamma = 3.3$), this assumption was leading to accurate estimated incident and reflected waves even for highly nonlinear waves. The reason for this was that the main contribution to the bound superharmonics stems from the interaction of components near the peak frequency of the primary spectrum.

The narrow-band assumption applied by Eldrup and Lykke Andersen [8] for the separation of irregular waves is not necessarily valid for nonlinear bichromatic waves if the frequency interval between the two primary components is not small enough. However, as the bound waves in bichromatic waves normally stem mainly from only one interaction, a more accurate method could be developed. Such a method is presented in the present paper, and the new method is evaluated on new model tests performed in a wave flume at the Atmosphere-Ocean Interaction Flume in Granada, Spain.

2. Third-Order Wave Theory for Bichromatic Waves

Bichromatic waves refer to waves with two primary incident components at cyclic frequencies ω_n and ω_m . The surface elevation of such incident waves can, with first-order theory, be expressed as

$$\begin{aligned}\eta^{(1)}(x, t) &= a_{n,I}^{(1)} \cos(k_n x - \omega_n t + \varphi_{n,I}^{(1)}) + a_{m,I}^{(1)} \cos(k_m x - \omega_m t + \varphi_{m,I}^{(1)}) \\ &= A_{n,I}^{(1)} \cos(k_n x - \omega_n t) + B_{n,I}^{(1)} \sin(k_n x - \omega_n t) + \\ &\quad A_{m,I}^{(1)} \cos(k_m x - \omega_m t) + B_{m,I}^{(1)} \sin(k_m x - \omega_m t).\end{aligned}\quad (1)$$

Second-order theory for a bichromatic group gives additionally three bound superharmonic components (sum-interactions) at the cyclic frequencies $2\omega_n$, $2\omega_m$, and $\omega_n + \omega_m$, and one subharmonic component (difference-interactions) at cyclic frequency $\omega_m - \omega_n$ (assuming $\omega_m > \omega_n$). Complete expressions, including second-order transfer functions (G), are given in, for example, Sharma and Dean [10], Schäffer [11], and Madsen and Fuhrman [12;13]. The second-order contribution due to the interaction of component n and m can be written as:

$$\begin{aligned}\eta_{n\pm m}^{(2)}(x, t) &= G_{nm}^{\pm}(A_{n,I}^{(1)}A_{m,I}^{(1)} \mp B_{n,I}^{(1)}B_{m,I}^{(1)}) \cos((k_n \pm k_m)x - (\omega_n \pm \omega_m)t) + \\ &\quad G_{nm}^{\pm}(A_{m,I}^{(1)}B_{n,I}^{(1)} \pm A_{n,I}^{(1)}B_{m,I}^{(1)}) \sin((k_n \pm k_m)x - (\omega_n \pm \omega_m)t) \\ &= a_{n\pm m} \cos((k_n \pm k_m)x - (\omega_n \pm \omega_m)t + \varphi_{n\pm m,I}).\end{aligned}\quad (2)$$

This gives one subharmonic contribution (η_{n-m}) and three superharmonic contributions (η_{2n} , η_{2m} , η_{n+m}). The period of the subharmonic component ($T = 2\pi / (\omega_m - \omega_n)$) also corresponds to the duration of the formed wave group. A correction to the linear dispersion equation appears first at third order, and thus in second order theory the linear dispersion equation is valid for the primary components.

The wave numbers of the bound superharmonics are calculated as the sum of the wave numbers of the interacting components and the difference for the subharmonics. Thus, the celerity of the bound components due to interaction of component n and m can be calculated as $c_{n-m} = (\omega_m - \omega_n)/(k_m - k_n)$ for the subharmonic and $c_{n+m} = (\omega_m + \omega_n)/(k_m + k_n)$ for the superharmonic component.

Recently, third-order solutions for bichromatic waves as well as for irregular waves were developed, cf. Madsen and Fuhrman [12;13]. Applying that theory to unidirectional bichromatic waves yields additionally four bound superharmonic components at the cyclic frequencies $3\omega_n$, $3\omega_m$, $\omega_m + 2\omega_n$, $\omega_n + 2\omega_m$ and two additional bound subharmonics at the cyclic frequencies $|\omega_n - 2\omega_m|$ and $|\omega_m - 2\omega_n|$. The computational cost of that method for irregular waves is very high, but for bichromatic waves the computational cost is very small. The wave numbers of the bound waves at the above given angular frequencies are found simply by summation and differences of the wave numbers for the primary frequencies (as in the second-order components given in Equation 2). Thus, for example, the wave number of the bound component at frequency $\omega_m + 2\omega_n$ is given by $k_m + 2k_n$. The celerity of the bound components can afterwards be calculated using the same principle as for the second-order components. However, the celerity of the primary components is different from the first-order values due to amplitude dispersion. The dispersion equation was derived to third order by Madsen and Fuhrman [12;13]. Here, it was shown that the celerity of each of the two primary components depend on the amplitude and frequency of both components.

3. Nonlinear Reflection Separation Method for Bichromatic Waves

Lykke Andersen et al. [7] showed that for regular waves the celerity of the bound superharmonics is higher than a free component at the same frequency, and this makes it possible to separate the bound and free waves. The same applies to bichromatic waves, and thus for bichromatic waves it is also possible to separate the bound and free superharmonic components due to their different celerities. The bound subharmonic component has a lower celerity than a free one at the same frequency. Thus, it is also possible to separate these components based on their differences in celerity. However, for shallow water waves, the celerities of the bound and the free waves are almost identical, and thus separation of the two is not possible.

The mathematical model used for the separation of nonlinear bichromatic waves is chosen as a third-order surface for the incident as well as for the reflected waves. Moreover, free incident and reflected components are included in all of the sub- and superharmonic frequencies. Finally, a noise term (Ω) is included. In the following, it is assumed that at the frequencies of the two primary components, only primary incident and reflected waves exist. In special cases, it might occur for bichromatic waves that the frequency of one or more of the sub- or superharmonic components is coincident with either a primary component or another higher harmonic. This is a special case that for the moment is not covered by the present method. For irregular waves, this occurs to a large extent, and Eldrup and Lykke Andersen [8] used a narrow band assumption for the primary spectrum to overcome this issue.

In order to separate the bichromatic waves, a mathematical model for the surface is needed at every frequency present in the signal. The surface is expressed at each of the wave gauges (x_j) in the frequency domain (Fourier space). The signal include both incident and reflected waves, and due to amplitude dispersion, the wave numbers are different for the incident waves ($k_{n,I}$, $k_{m,I}$) and the reflected ($k_{n,R}$, $k_{m,R}$) primary components. Based on Equation (1) the following mathematical model is obtained at the two primary frequencies (where index i can take the values n and m and thus represent frequencies ω_n and ω_m):

$$\begin{aligned}\hat{\eta}^{(1)}(x_j) &= C_I^{(1)} X_I^{(1)} + C_R^{(1)} X_R^{(1)} + \Omega_{i,j}^{(1)} \\ X_I^{(1)} &= a_{i,I}^{(1)} \exp[-i(k_{i,I} x_1 + \varphi_{i,I}^{(1)})] \\ X_R^{(1)} &= a_{i,R}^{(1)} \exp[i(k_{i,R} x_1 + \varphi_{i,R}^{(1)})] \\ C_I^{(1)} &= \exp(-ik_{i,I} \Delta x_j) \\ C_R^{(1)} &= \exp(ik_{i,R} \Delta x_j),\end{aligned}\tag{3}$$

where $\Delta x_j = x_j - x_1$ is the distance between wave gauge number j and wave gauge number 1, i is the imaginary unit ($i^2 = -1$), and $\Omega_{i,j}$ is the noise at frequency ω_i at gauge j . Later, an iterative procedure to estimate the wave numbers will be presented. The amplitudes are then calculated by a least-squares approach identical to that used by Lykke Andersen et al. [7] for regular waves.

Seven superharmonic frequencies ($2\omega_n$, $2\omega_m$, $\omega_m + \omega_n$, $3\omega_n$, $3\omega_m$, $\omega_m + 2\omega_n$, $\omega_n + 2\omega_m$) and three subharmonic frequencies ($\omega_m - \omega_n$, $|\omega_n - 2\omega_m|$ and $|\omega_m - 2\omega_n|$) are analyzed. These corresponded to the second- and third-order interaction frequencies given in Section 2. In the following, these frequencies are termed ω_i , where index i can take the values $2n$, $2m$, $m + n$, $3n$, $3m$, $m + 2n$, $m - n$, $n - 2m$, and $m - 2n$. The related wave numbers of the bound wave are termed k_i : For example, $i = m+2n$ corresponds to the cyclic frequency $\omega_m + 2\omega_n$, and the wave number of the bound wave is $k_i = k_{m+2n} = k_m + 2k_n$. These wave numbers are different for the incident and the reflected waves due to different primary wave numbers due to amplitude dispersion ($k_{n,I}$, $k_{m,I}$ for incident and $k_{n,R}$, $k_{m,R}$ for reflected). For these ten frequencies, the mathematical model consists of both free and bound components in the incident and reflected wave direction. The mathematical model can be written in frequency domain as

$$\begin{aligned}\hat{\eta}_i(x_j) &= C_{i,I,B}X_{i,I,B} + C_{i,R,B}X_{i,R,B} + C_{i,I,F}X_{i,I,F} + C_{R,F}X_{R,F} + \Omega_{i,j} \\ X_{i,I,B} &= a_{i,I,B} \exp[-i(k_{i,I}x_1 + \phi_{i,I,B})] \\ X_{i,R,B} &= a_{i,R,B} \exp[i(k_{i,R}x_1 + \phi_{i,R,B})] \\ X_{I,F} &= a_{i,I,F} \exp[-i(k_f x_1 + \phi_{i,I,F})] \\ X_{R,F} &= a_{i,R,F} \exp[i(k_f x_1 + \phi_{i,R,F})] \\ C_{i,I,B}^{(n)} &= \exp(-ik_{i,I} \Delta x_j) \\ C_{i,R,B}^{(n)} &= \exp(ik_{i,R} \Delta x_j) \\ C_{I,F} &= \exp(-ik_f \Delta x_j) \\ C_{R,F} &= \exp(ik_f \Delta x_j),\end{aligned}\quad (4)$$

where k_f is the wave number of the free waves at the cyclic frequency ω_i and is calculated by the linear dispersion equation. The amplitudes of the bound harmonics can also be calculated by a least-square method when the wave numbers are known (see solution in Lykke Andersen et al. [7]).

Including terms up to the third order is reasonable for the tests considered in the present paper. Nevertheless, it is straightforward to extend the method to a higher order by applying Equation (4) at these frequencies. However, it is important to stress that it is assumed that only one (significant) bound interaction must occur at each frequency. This becomes more difficult to fulfill the higher order the waves are.

The wave numbers of the two primary components determine the wave numbers of each of the bound sub- and superharmonics analyzed with Equation (4). Thus, a critical part of being able to separate accurately the bound and the free harmonics is to have an accurate estimate of the wave number (or the celerity) of the two incident and reflected primary components that the bichromatic waves consist of. In principle, these four wave numbers could be unknown parameters in the mathematical model to be calculated, which, however, would result in nonlinear equations. Alternatively, they might be estimated by a wave theory, which was the procedure chosen by Lykke Andersen et al. [7] and Eldrup and Lykke Andersen [8] and which was also chosen for the present paper. In the present case, the wave numbers of the free sub- and superharmonic components (k_f) were calculated with the linear dispersion equation. The wave numbers for the primary may be calculated with the third-order theory of Madsen and Fuhrman [12;13], which is valid for all of the present cases except one test (see Chapter 5). Initial tests showed that the presence of a second primary component did not influence significantly the celerity of the other component. Therefore, another possibility is to calculate the celerity of each primary component based on the stream function theory for regular waves by Fenton and Rienecker [9], with the parameters of each of the primary waves. This might increase the range of applicability to more shallow water waves. For the present test cases, the results were almost identical for the two methods, and thus more nonlinear waves in shallow water are needed to clarify this. The iterative procedure used is as follows:

1. Calculate the wave number for each primary frequency (n, m) based on linear dispersion, i.e., for infinitesimally small amplitudes of the primary components. Use this estimate as a starting guess for the incident and reflected wave numbers ($k_{n,I}$, $k_{m,I}$, $k_{n,R}$, and $k_{m,R}$);
2. Calculate first- to third-order incident and reflected components by applying the Lykke Andersen et al. [7] method on Equation (3) for the two primary frequencies and Equation (4) for the frequencies of the ten bound second and third harmonics. For bound components, use the latest estimated incident and reflected wave numbers ($k_{n,I}$, $k_{m,I}$, $k_{n,R}$, and $k_{m,R}$) calculated in either step 1 for the first iteration or step 3 for the following iterations. Free components are normally of much smaller height, and linear assumption is assumed valid for those;
3. Calculate updated values of $k_{n,I}$, $k_{m,I}$, $k_{n,R}$, and $k_{m,R}$ either based on either a) third-order wave theory using the found amplitudes of the primary components, or b) ignoring the interaction of the two primary components (n and m), and thus a method for highly nonlinear regular waves can be applied for each component (e.g., stream function theory from Fenton and Rienecker (1980));
4. Repeat steps 2 and 3 until convergence is obtained for the incident and reflected wave numbers.

In principle, the calculations of the wave numbers should take into account the generated return currents from the incident and reflected waves. The third-order dispersion equation given by Madsen and Fuhrman [12,13] makes it possible to calculate the influence of the return currents on the celerities. This was done by calculating the celerities when no return currents were considered ($U = 0$) and when a closed basin was considered and thus a return current from the incident waves existed ($q = 0$). As the reflected waves generate a return current in the opposite direction, these calculations show the maximum influence of the return currents. For the test cases considered in the present paper, the difference on the celerities between using $U = 0$ and $q = 0$ was found to be from 0.2% to 0.9%, and thus the return current was not very important to include for the present tests. Therefore, it was decided to use $U = 0$ in the calculations, which was in line with what was used by Lykke Andersen et al. [7] for regular waves.

Moreover, the interaction of the incident and reflected waves was ignored, which from second-order wave theory is known to be a reasonable approximation (Eldrup and Lykke Andersen [8]). When both free and bound waves are present at a given frequency, this causes a modulation of the amplitude of the other components. This effect is mainly relevant when the bound and the free waves are high and have amplitudes of the same order of magnitude. This effect was not included in the mathematical model by Lykke Andersen et al. [7] and Eldrup and Lykke Andersen [8], and it was also ignored in the present paper.

Equations (3) and (4) are of similar form to the equations provided by Lykke Andersen et al. [7] for regular waves. Their solution can thus be applied also to bichromatic waves. Cases where the celerity of the free and the bound waves are almost identical can also be handled in a similar way to that presented in that paper. In bichromatic waves, the two primary frequencies in the signal would normally be known from the input to the wave maker. If this is not the case, a frequency domain analysis can be carried out to identify the frequency of the two highest peaks.

4. Validation on Synthetic Data

In order to validate the method and its implementation, bichromatic synthetic data were generated using the third-order theory of Madsen and Fuhrman [12;13]. The test case corresponds to “Test No. 2” in the later presented physical model tests (see Section 5). The data does not include any reflection or free harmonics. The wave gauge array used is also identical to that used in the physical model tests. The chosen phases of the two primary components are zero at $x = 0$.

Table 1 presents the actual amplitudes and the estimated ones. Note that there is almost full agreement, and errors on the amplitudes are typically less than 1%. Moreover, the estimated reflected free and bound components as well as the incident free components are close to zero, as used in the synthetic data. Minor errors are present mainly in the second-order components and are expected to be caused by small errors on the estimated celerities of the bound waves due to using third-order

theory with $q = 0$ in the synthetic data and using stream function theory with $U = 0$ for each primary wave in the analysis method.

Table 1. Actual and calculated amplitudes in millimeters for the synthetic test case.

Component	Actual Incident Bound	Estimated Incident Bound	Estimated Reflected Bound	Estimated Incident Free	Estimated Reflected Free
a_n	50.0	50.1	0.2	-	-
a_m	50.0	49.9	0.2	-	-
a_{2n}	5.8	5.8	0.0	0.0	0.0
a_{2m}	4.7	4.7	0.0	0.1	0.1
a_{n+m}	10.5	10.5	0.0	0.2	0.1
a_{m-n}	7.4	7.6	0.1	0.3	0.1
a_{3n}	0.7	0.7	0.0	0.0	0.0
a_{3m}	0.5	0.5	0.0	0.0	0.0
a_{n+2m}	1.6	1.6	0.0	0.0	0.0
a_{2n+m}	1.8	1.8	0.0	0.0	0.0
a_{n-2m}	7.7	7.7	0.0	0.0	0.0
a_{m-2n}	3.4	3.2	0.0	0.2	0.0

Additionally, the time series are plotted in Figure 1, which demonstrates that phases are also correctly calculated. Moreover, the figure gives an overall impression of the accuracy, as the estimated incident time series including only bound higher harmonics is almost identical to the target. Moreover, the estimated incident free higher harmonics, as well as the reflected components, are insignificant. Therefore, the implemented method was validated for data, fulfilling the assumptions of the method.

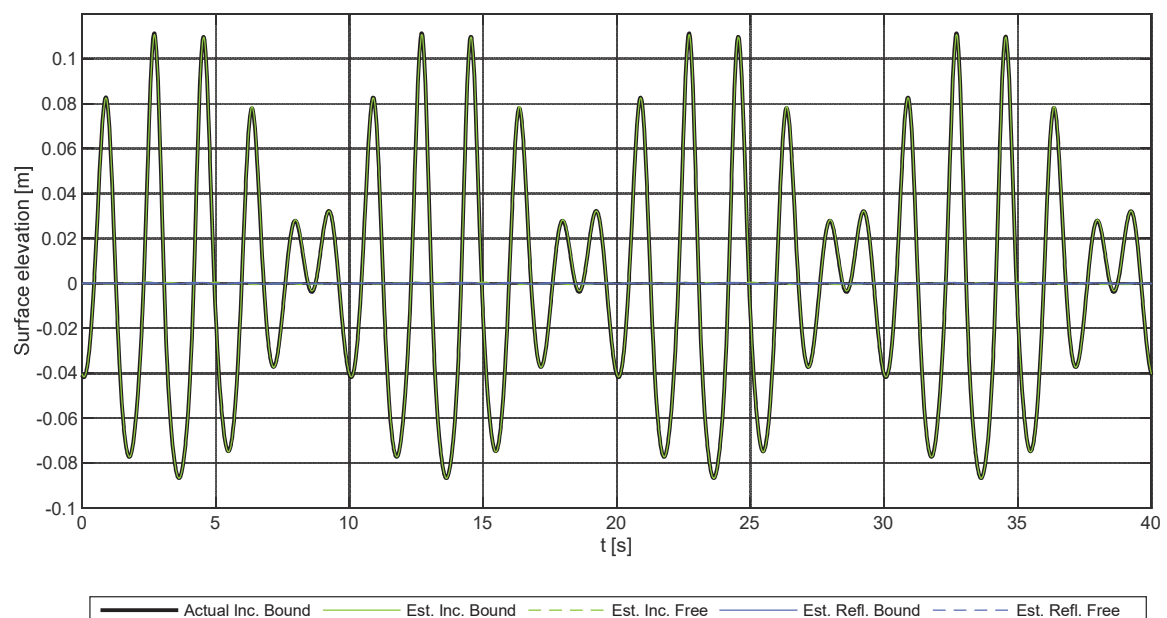


Figure 1. Comparison of measured total and predicted incident and reflected time series at WG1 for the synthetic test case.

5. Physical Model Test Setup and Methodology

In order to evaluate the method, 2-D model tests were performed in a wave flume at the Atmosphere-Ocean Interaction Flume in Granada, Spain. The flume has a piston wave maker in each end, where one wave maker (WM1) is generating and absorbing waves, and the other wave maker (WM2) is only absorbing. The active absorption method used was the one presented by Lykke

Andersen et al. [14], and the model test setup was also identical. An array of eight wave gauges (WG1–WG8) were used to test the above given reflection separation method. The method uses data from all gauges to calculate incident and reflected wave train components (amplitudes and phases). Based on the calculated components, the incident and reflected wave trains can be calculated at any point, but any errors in the mathematical model (for example, celerities) will amplify with distance from the central part of the wave gauge array. In the present paper, the time series will only be presented for $x = 5.95$ m (at the location of WG1). The water depth was constant throughout the length of the flume and equal to 0.65 m in all tests. The model test setup is shown in Figure 2.

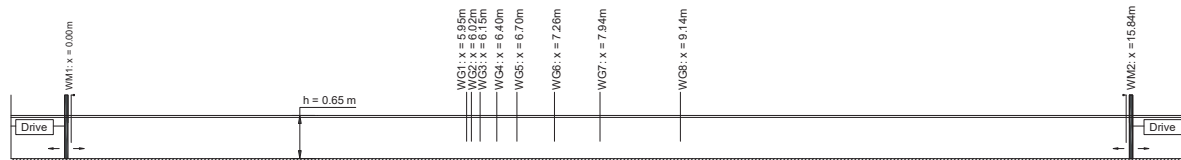


Figure 2. Model test setup.

Bichromatic waves were generated using the second-order wave maker theory of Schäffer [11], which correctly generates the bound sub- and superharmonics to second-order and thus minimizes free second-order incident energy. The test was performed for 240 s with a 10-s ramp up and down in each end. The analyzed part of the tests was from 40 s to 230 s. Table 2 presents the test conditions. With the chosen test conditions, the assumption in the mathematical model of all the primary and the interaction terms occurring at independent frequencies up to the third order was fulfilled. After Test Nos. 3, 8, and 9, some minor cross-modes were observed.

Table 2. Target test conditions.

Test No.	f_n [Hz]	f_m [Hz]	a_n [mm]	a_m [mm]
1	0.30	0.40	50	50
2	0.50	0.60	50	50
3	0.60	0.70	50	50
4	0.60	0.80	50	50
5	0.50	0.55	50	50
6	0.50	0.52	50	50
7	0.30	0.40	25	25
8	0.50	0.60	25	25
9	0.60	0.70	25	25
10	0.60	0.80	25	25
11	0.50	0.55	25	25
12	0.50	0.52	25	25

Figure 3 presents the test conditions in a Le Méhauté [15] diagram, where the data are plotted with the highest period of the two primary components and with the sum of their wave heights. In that way, the diagram should be slightly on the safe side with respect to the valid theory. It appears that third-order theory should be valid for all cases except for Test No. 1.

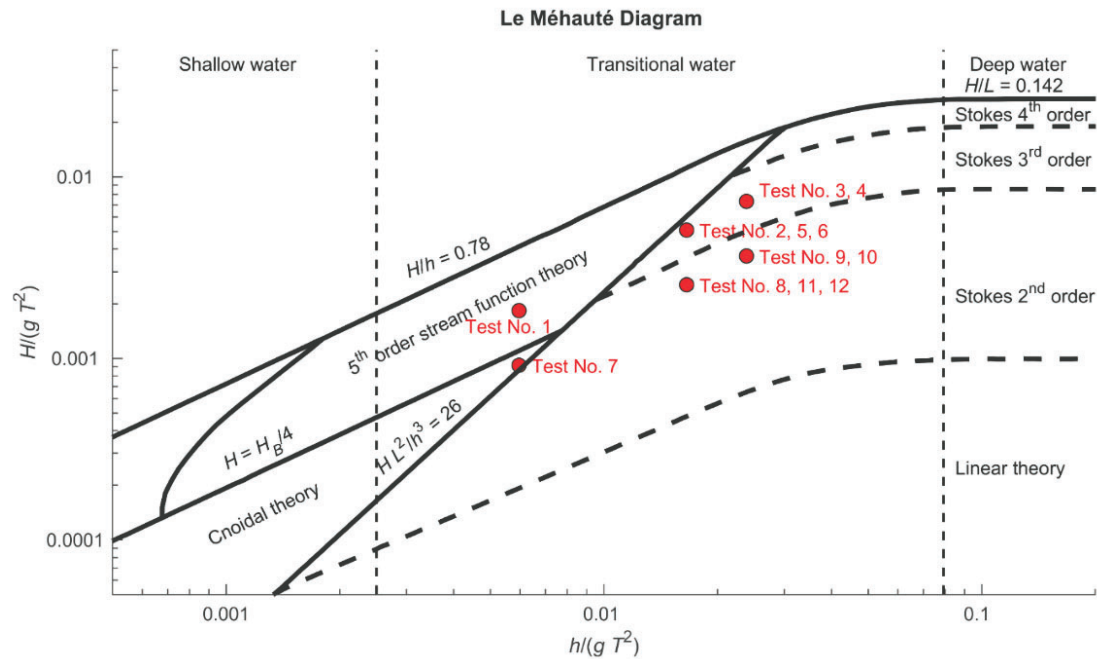


Figure 3. Applicability of different wave theories for the test conditions.

6. Physical Model Test Results

Figures 4 and 5 show the incident and reflected time series for Test Nos. 2 and 5, respectively. The time series for the bound waves also include the two primary components. It appears that reflection is limited and in both cases at the order of 5%–10% of the incident wave. In the following, the focus is on analyzing the incident waves. An in-depth analysis of the reflection of the bound and free waves and a comparison to the linear absorption curve given by the Lykke Andersen et al. [14] method, is covered in detail by Lykke Andersen et al. [16].

Incident free waves of small amplitude are present, indicating that the bound harmonics were not generated accurately. This was maybe expected, as second-order generation was used while third-order theory was needed, according to Figure 3.

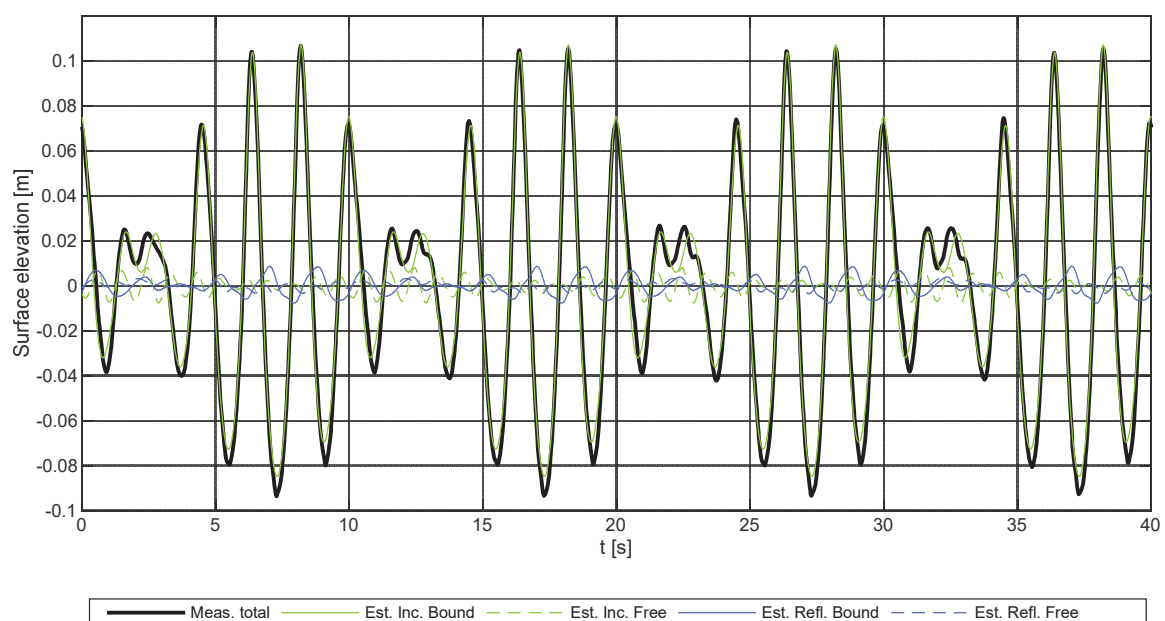


Figure 4. Comparison of measured total and predicted incident and reflected time series at WG1 ($x = 5.95$ m) for Test No. 2.

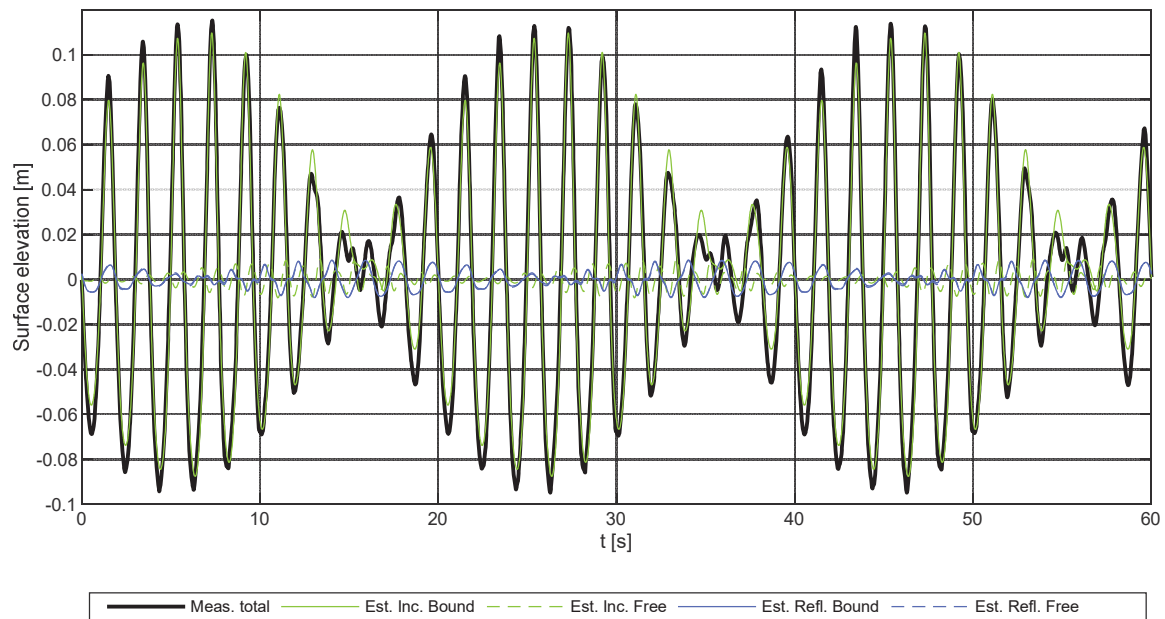


Figure 5. Comparison of measured total and predicted incident and reflected time series at WG1 ($x = 5.95$ m) for Test No. 5.

Table 3 presents the measured components for all the test cases using the present method. It appears that the two primary amplitudes are usually slightly lower than the target. This might be partly caused by energy needed to be stolen for the third-order components that were not generated and partly due to other issues such as leakage around the paddle.

Table 3. Estimated amplitudes in millimeters of all the incident bound components.

Test	a_n	a_m	a_{2n}	a_{2m}	a_{n+m}	a_{m-n}	a_{3n}	a_{3m}	a_{n+2m}	a_{2n+m}	a_{n-2m}	a_{m-2n}
1	47.0	44.3	12.2	5.7	16.2	13.7	1.7	0.8	3.8	5.5	3.9	1.3
2	47.5	46.8	5.4	4.2	9.8	7.2	0.7	0.6	1.5	1.4	2.9	1.6
3	46.4	47.6	4.6	4.0	8.2	4.9	0.8	0.5	0.9	1.5	0.6	1.4
4	45.8	46.5	4.7	5.2	7.9	2.1	1.2	0.9	2.3	2.5	2.7	1.1
5	50.5	44.5	6.3	4.2	9.6	9.3	0.9	0.5	1.1	1.2	5.5	4.4
6	52.7	40.7	7.1	2.4	9.2	5.4	1.3	0.1	0.8	1.6	6.5	6.0
7	24.2	23.7	3.2	1.7	4.4	4.6	0.2	0.1	0.4	0.5	0.8	0.2
8	23.6	23.9	1.2	1.0	2.3	1.8	0.1	0.0	0.1	0.2	0.4	0.3
9	23.6	24.3	1.0	1.0	1.9	1.3	0.1	0.1	0.2	0.3	0.0	0.4
10	23.6	24.2	1.0	1.1	2.1	0.7	0.1	0.1	0.2	0.2	0.3	0.1
11	24.2	23.4	1.3	1.1	2.3	2.1	0.1	0.0	0.1	0.1	0.8	0.7
12	24.5	23.1	1.4	1.0	2.4	1.3	0.0	0.0	0.1	0.1	0.7	0.9

In Figure 6, the measured amplitudes from Table 3 are compared to theoretical predictions based on third-order wave theory (Madsen and Fuhrman [12;13]) using the two estimated primary amplitudes. The estimated amplitudes of the bound second-order superharmonics by the present method match accurately the ones predicted by the third-order theory. The same is the case for the subharmonic component, but more scatter is observed.

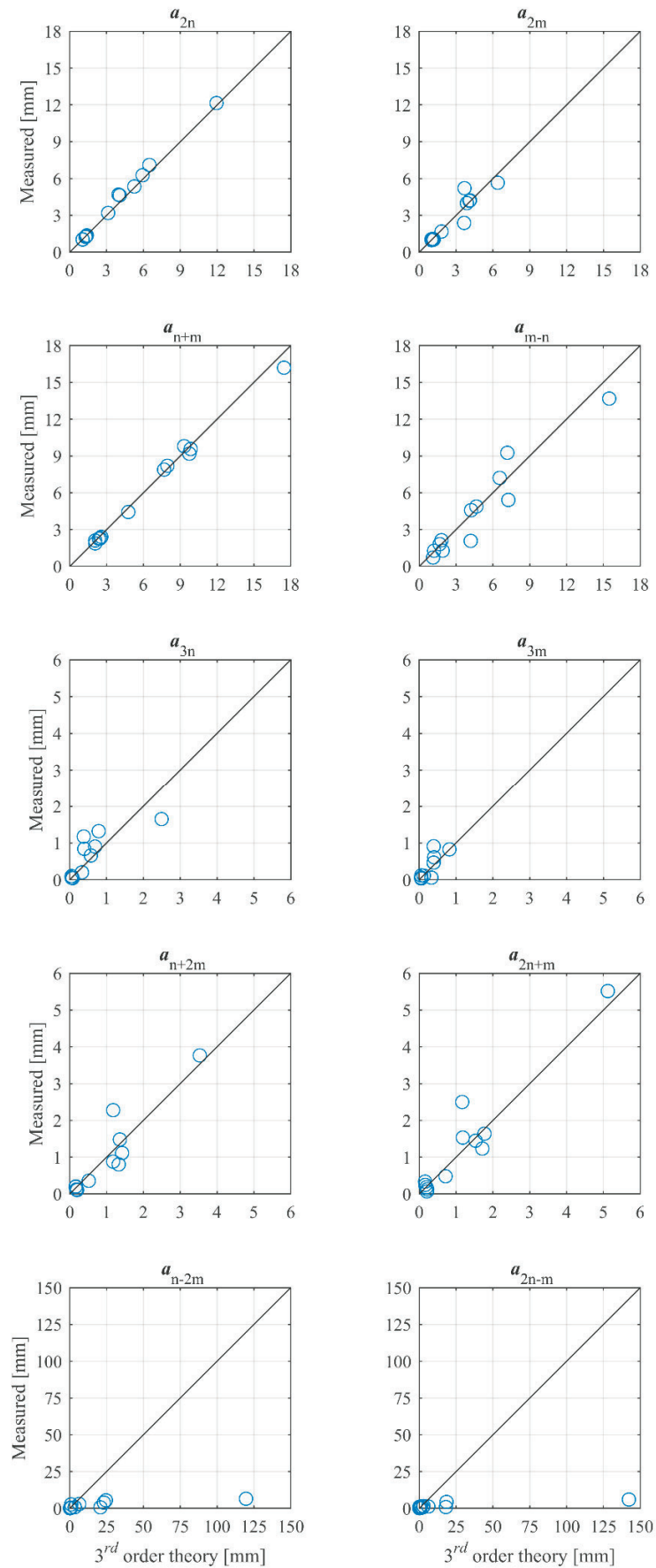


Figure 6. Measured amplitudes of bound second- and third-order components compared to Madsen and Fuhrman [12,13].

With respect to the third-order components, the agreement with third-order wave theory is fair except for the subharmonics, which presented strong deviations. The predicted amplitudes are significantly larger than the second-order components, which is not physically correct and is due to singularities in the transfer functions, as also found by Madsen and Fuhrman [13].

7. Discussion

In the present paper, a new method to separate nonlinear bichromatic waves into incident and reflected surface elevation time series was presented. Most existing methods only consider free energy to be present, and their range of applicability is thus limited to linear waves. The new method includes both free and bound higher harmonics, which is necessary in order to separate nonlinear waves accurately. The method is an extension of the method for nonlinear regular waves presented recently by Lykke Andersen et al. [7]. That method was extended by Eldrup and Lykke Andersen [8] to fully irregular waves by utilizing a narrow band approximation for the primary spectrum. The new method for bichromatic waves includes all interactions correctly to the third order. As expected, the results showed that the new method accurately predicted the incident and reflected waves in synthetically generated third-order bichromatic waves.

Moreover, the method was tested on physical model tests performed in a wave flume with wave makers in both ends. The new method seems to predict accurately the incident and reflected wave trains, and the estimated amplitudes of the second- and third-order bound components matched reasonably with third-order wave theory for irregular waves. For third-order subharmonics, a significant deviation from third-order wave theory was, however, found in some tests, but this could be attributed to singularities in the transfer functions provided by Madsen and Fuhrman [12;13], and thus their method was not valid for these cases.

Author Contributions: T.L.A. and M.R.E. defined the new analysis method, and M.R.E. prepared the synthetic and numerical model data. M.C. provided access to the wave flume and prepared the test setup for the physical model tests. T.L.A. prepared the test methodology and performed the model tests and the analysis. T.L.A. wrote the paper. All authors have read and approved the final manuscript.

Funding: This research received no external funding.

Conflicts of Interest: The authors declare no conflicts of interest.

References

1. Goda, Y.; Suzuki, Y. Estimation of incident and reflected waves in random wave experiments. In Proceedings of the 15th International Conference on Coastal Engineering, Honolulu, HI, USA, 11–17 July 1976; pp. 828–845, doi:10.9753/icce.v15.%25p.
2. Mansard, E.P.D.; Funke, E.R. The measurement of incident and reflected spectra using a least squares method. In Proceedings of the 17th International Conference on Coastal Engineering, Sydney, Australia, 23–29 March 1980; pp. 154–172, doi:10.1061/9780872622647.008.
3. Zelt, J.A.; Skjelbreia, J.E. Estimating incident and reflected wave fields using an arbitrary number of wave gauges. In Proceedings of the 23rd International Conference on Coastal Engineering, Venice, Italy, 4–9 October 1992; pp. 777–788, doi:10.9753/icce.v23.%25p.
4. Lin, C.-Y.; Huang, C.-J. Decomposition of incident and reflected higher harmonic waves using four wave gauges. *Coast. Eng.* **2004**, *51*, 395–406, doi:10.1016/j.coastaleng.2004.04.004.
5. Figueres, M.; Garrido, J.M.; Medina, J.R. *Cristalización Simulada para el Análisis de Oleaje Incidente y Reflejado con un Modelo de Onda Stokes-V*; VII Jornadas de Puertos y Costas: Almeria, Spain, 2003.
6. Figueres, M.; Medina, J.R. Estimating incident and reflected waves using a fully nonlinear wave model. In Proceedings of the 29th International Conference on Coastal Engineering, Lisbon, Portugal, 19–24 September 2004; pp. 594–603, doi:10.1142/9789812701916_0047.
7. Lykke Andersen, T.; Eldrup, M.R.; Frigaard, P. Estimation of Incident and Reflected Components in Highly Nonlinear Regular Waves. *Coast. Eng.* **2017**, *119*, 51–64, doi:10.1016/j.coastaleng.2016.08.013.
8. Eldrup, M.R.; Lykke Andersen, T. Estimation of Incident and Reflected Wave Trains in Highly Nonlinear Two-Dimensional Irregular Waves. *J. Waterw. PortCoast. Ocean Eng.* **2019**, *145*, doi:10.1061/(ASCE)WW.1943-5460.0000497.

9. Fenton, J.D.; Rienecker, M.M. Accurate numerical solution for nonlinear waves. In Proceedings of the 17th Conference of Coastal Engineering, Sydney, Australia, 23–29 March 1980; Volume 1, pp. 50–69, doi:10.9753/icce.v17.%25p.
10. Sharma, J.; Dean, R. Second-order directional seas and associated wave forces. *Soc. Pet. Eng. J.* **1981**, *21*, 129–140, doi:10.2118/8584-PA.
11. Schäffer, H.A. Laboratory Wave Generation Correct to Second Order. In Proceedings of the Conference Wave Kinematics and Environmental Forces, London, UK, 24–25 March 1993; Soc Underwater Tech; Volume 29, pp. 115–139.
12. Madsen, P.A.; Fuhrman, D.R. Third-order theory for bichromatic bi-directional water waves. *J. Fluid Mech.* **2006**, *557*, 369–397, doi:10.1017/S0022112006009815.
13. Madsen, P.A.; Fuhrman, D.R. Third-order theory for multi-directional irregular waves. *J. Fluid Mech.* **2012**, *698*, 304–334, doi:10.1017/jfm.2012.87.
14. Lykke Andersen, T.; Clavero, M.; Frigaard, P.; Losada, M.; Puyol, J.I. A new active absorption system and its performance to linear and non-linear waves. *Coast. Eng.* **2016**, *114*, 47–60, doi:10.1016/j.coastaleng.2016.04.010.
15. Le Mehauté, B. *An Introduction to Hydrodynamics and Water Waves*; Springer: Berlin/Heidelberg, Germany, 1976. doi:10.1007/978-3-642-85567-2.
16. Lykke Andersen, T.; Clavero, M.; Eldrup, M.R.; Frigaard, P.; Losada, M. Active Absorption of Nonlinear Irregular Wave. In Proceedings of the 36th International Conference on Coastal Engineering, Baltimore, MD, USA, 30 July–3 August 2018. submitted.



© 2019 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).